

Information about the exam

Exam

Course code and name	Date	Time	Hall
First option: ELEC-E8427 Power Transmission Systems	19.4.2024	13:00-16:00	TU5 - 1194-1195, Maarintie 8
Another option: ELEC-E8427 Power Transmission Systems	13.5.2024	16:30-19:30	Informed later

- **Exam materials: Material is all “theory” lectures (given by Janne Seppänen) + calculation exercises. No guest lectures, no materials labelled as “extra”.**
- **Exam will be a normal lecture hall exam (not remote)**
- **The most complicated equations (such as ABCD constants of long transmission lines, swing equation, symmetrical components) will be given in the exam material, if they are needed**
- **Calculator is needed and allowed in the exam**
- **Use of materials/books/computer and internet are not allowed**

Grading

- **Home calculations (non mandatory): max 6 extra points in total**
- **Exam: max 30 points**
- **Total maximum points if all home calculations have been done: $30 + 6 = 36$**
- **Grade limits:**
 - 27 or higher -> 5
 - 24-26 -> 4
 - 21-23 -> 3
 - 18-20 -> 2
 - 15-17 -> 1
 - 0-14 -> 0

Exam, core topics

- **Power flow**
- **Transmission lines (natural power, behavior of line in different loading conditions etc)**
- **Faults: three phase short circuit and one phase ground fault**
- **Voltage stability & angle stability, stability of generators after a fault**
- **Transfer capacity**

Example of given equations

- These equations (at least) will be given in the exam
- This is a standard set of equations given in the exams of the previous versions of the Power Transmission Systems course, and these equations cannot and should not be used to determine which types of questions will be included in the exam.

Equations (this is a standard set of equations given at every exam):

$$\cosh(\alpha + j\beta) = \frac{1}{2}(e^{\alpha+j\beta} + e^{-\alpha-j\beta}) = \frac{1}{2}(e^{\alpha} \cdot e^{j\beta} + e^{-\alpha} \cdot e^{-j\beta}) = \frac{e^{\alpha}}{2} \angle \beta + \frac{e^{-\alpha}}{2} \angle -\beta$$

$$\sinh(\alpha + j\beta) = \frac{1}{2}(e^{\alpha+j\beta} - e^{-\alpha-j\beta}) = \frac{1}{2}(e^{\alpha} \cdot e^{j\beta} - e^{-\alpha} \cdot e^{-j\beta}) = \frac{e^{\alpha}}{2} \angle \beta - \frac{e^{-\alpha}}{2} \angle -\beta$$

$$\underline{A} = \cosh \underline{\gamma} s \quad \underline{B} = \underline{Z}_0 \sinh \underline{\gamma} s \quad \underline{C} = \frac{\sinh \underline{\gamma} s}{\underline{Z}_0}$$

Swing equation as pu values:

$$\frac{2H}{\omega_s} \omega_{pu}(t) \frac{d^2 \delta}{dt^2} = p_m(t) - p_e(t)$$

Reactive power consumed by a line:

$$Q_1 + Q_2 = \frac{U_1^2}{X} + \frac{U_2^2}{X} - 2 \frac{U_1 U_2}{X} \cos \delta - \frac{B U_1^2}{2} - \frac{B U_2^2}{2} \approx 2 \frac{U^2}{X} (1 - \cos \delta) - B U^2$$

Line receiving end voltage u when the sending end voltage is $e = 1$ pu

$$u = \sqrt{\frac{(1 - 2xp \tan \phi) \pm \sqrt{1 - 4xp \tan \phi - 4x^2 p^2}}{2}}$$

Symmetrical components:

$$\begin{bmatrix} \underline{U}_A \\ \underline{U}_B \\ \underline{U}_C \end{bmatrix} = \begin{bmatrix} 1 & 1 & 1 \\ 1 & \underline{a}^2 & \underline{a} \\ 1 & \underline{a} & \underline{a}^2 \end{bmatrix} \begin{bmatrix} \underline{U}_{A0} \\ \underline{U}_{A1} \\ \underline{U}_{A2} \end{bmatrix} \quad (\text{similar equation also applies for currents})$$

$$\begin{bmatrix} \underline{U}_{A0} \\ \underline{U}_{A1} \\ \underline{U}_{A2} \end{bmatrix} = \frac{1}{3} \begin{bmatrix} 1 & 1 & 1 \\ 1 & \underline{a} & \underline{a}^2 \\ 1 & \underline{a}^2 & \underline{a} \end{bmatrix} \begin{bmatrix} \underline{U}_A \\ \underline{U}_B \\ \underline{U}_C \end{bmatrix} \quad (\text{similar equation also applies for currents})$$

$$\underline{U}_{A1} = \underline{E}_A - \underline{Z}_1 \underline{I}_{A1}$$

$$\underline{U}_{2A} = -\underline{Z}_2 \underline{I}_{A2}$$

$$\underline{U}_{0A} = -\underline{Z}_0 \underline{I}_{A0}$$