

**CHEM-E1150**  
**BIOMASS PRETREATMENT AND FRACTIONATION**  
Theme 1: Kraft pulping, Module 2  
**Prehydrolysis**

*Herbert Sixta, 2019*

## Outline Theme 1

**Module 1: Raw materials and mechanical pretreatment**

**Module 2: Prehydrolysis**

**Module 3: Kraft cooking**

**Module 4. Screening, washing, bleaching and drying**

**Module 5: Pulp properties and uses**

## Module 2

### 1. Introduction

### 2. Chemistry

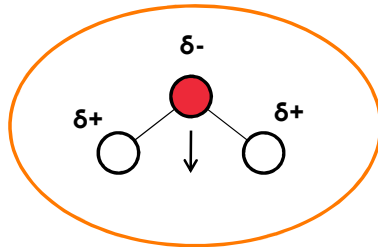
### 3. Kinetics

### 4. Technology

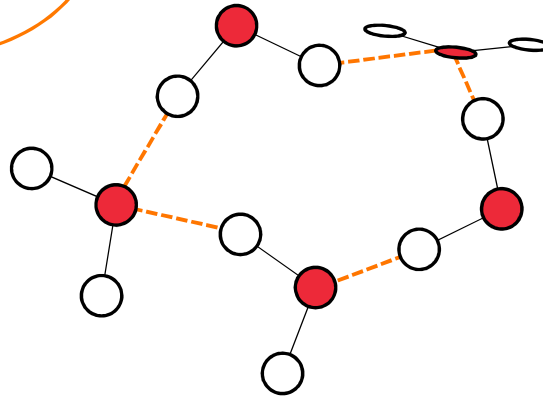
## Some introductory words...History

|      |                  |                               |                                                                                                                                           |
|------|------------------|-------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------|
| 1819 | Braconnot        | HCl conc                      | Ind.Eng.Chem. 1945,37,5-8                                                                                                                 |
| 1923 | Schöller         | Percolation, 0.5 wt% SA, 170C | Ind.Eng.Chem. 1945,37,9-11                                                                                                                |
| 1929 | Mason            | Steam explosion               | U.S. Patent No. 1,655,618, 1929.                                                                                                          |
| 1932 | Babcock          | Steam explosion               | U.S. Patent No. 1,825,464, 1932                                                                                                           |
| 1937 | Bergius          | Batch, 40 wt% HCl at 25C      | Ind.Eng.Chem. 1937, 29, 247-253                                                                                                           |
| 1940 | Königsberg       | Prehydrolysis (Soda)          | Rydholm 1966                                                                                                                              |
| 1945 | Madison          | Percolation, 0.5 wt% SA, 180C | report no. R1617 1946                                                                                                                     |
| 1968 | Bobleter         | Hydrothermolysis              | AT No. 263661, 25.7.1968                                                                                                                  |
| 1978 | Lora and Wayman  | Autohydrolysis                | TAPPI J. 1978, 61, 47.                                                                                                                    |
| 1987 | Overend, Chornet | Hydrothermal treatment        | Phil. Trans. R. Soc. Lond., 1987, 321, 523.                                                                                               |
| 1994 | Antal            | Aquasolv                      | Advances in Thermochemical<br>Biomass Conversion; Bridgewater,<br>A.V., Ed.; Blackie Academic and<br>Professional: London, 1994; p. 1572. |

## Water

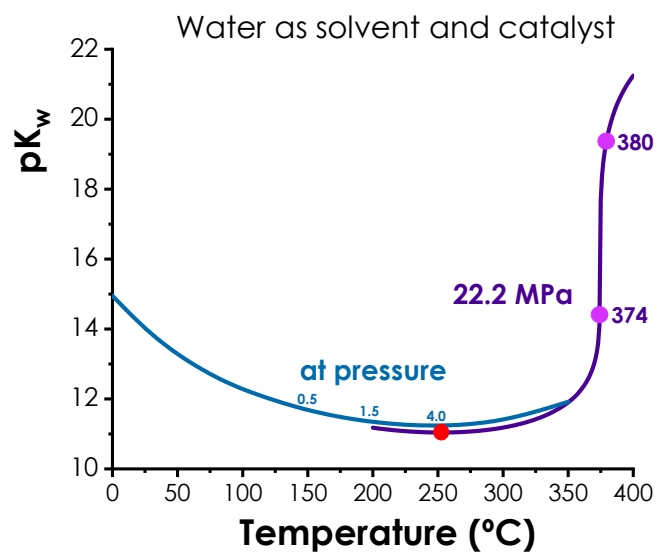
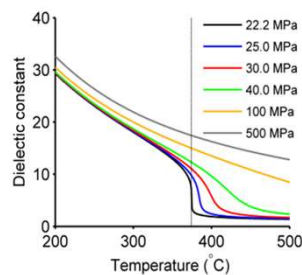
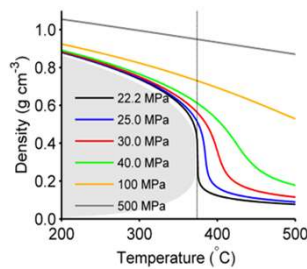


- Permanent dipole moment
- Hydrogen bonding ability
- Self-dissociation:  $2 \text{H}_2\text{O} \rightarrow \text{H}_3\text{O}^+ + \text{OH}^-$   
by proton jumping (Grotthuss mechanism)



<https://upload.wikimedia.org/wikipedia/commons/d/d8/Autoionizacion-agua.gif>

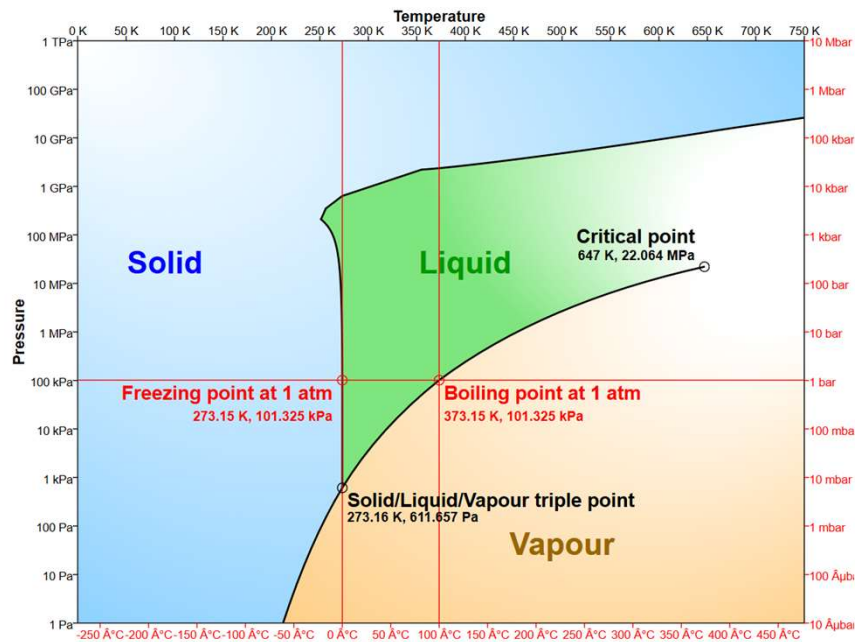
## Physical properties of water



Ion product calculated according to (Marshall, Franck 1981).

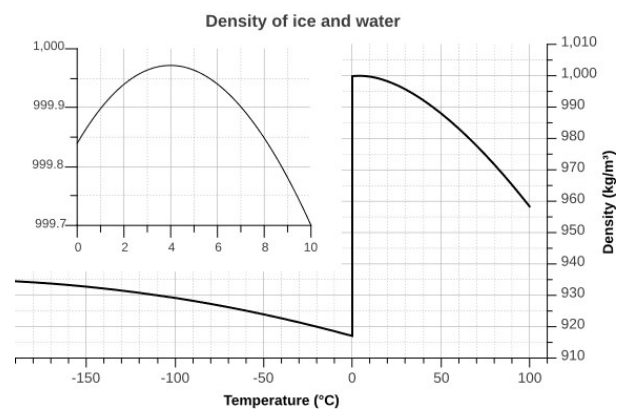
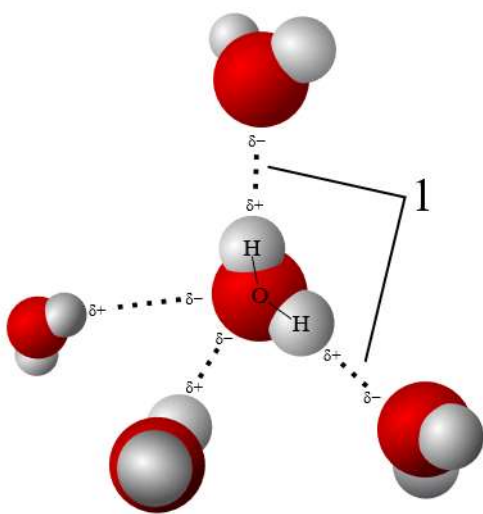
Lasse Tolonen: PhD thesis 2016

## Phase diagram of water

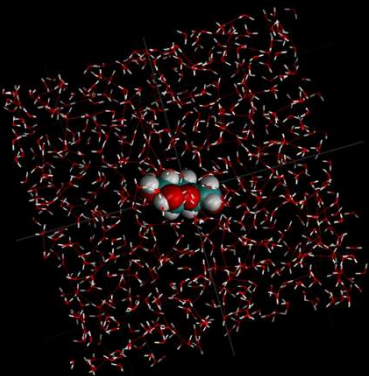


Wikipedia

## Phase diagram of water

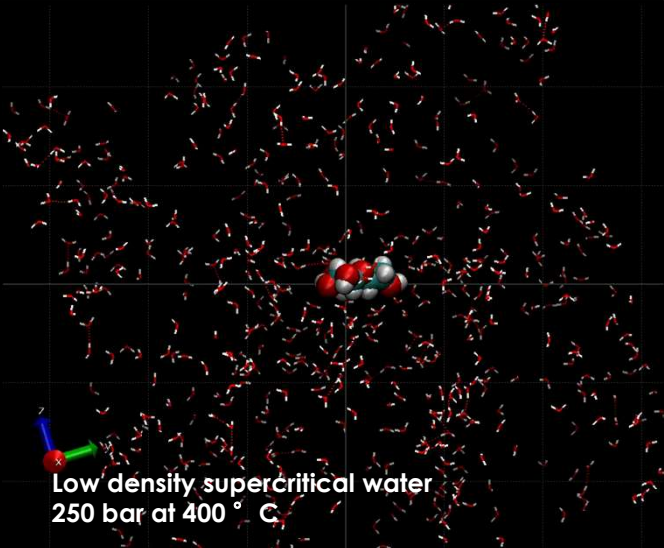


Wikipedia



**Ambient water**

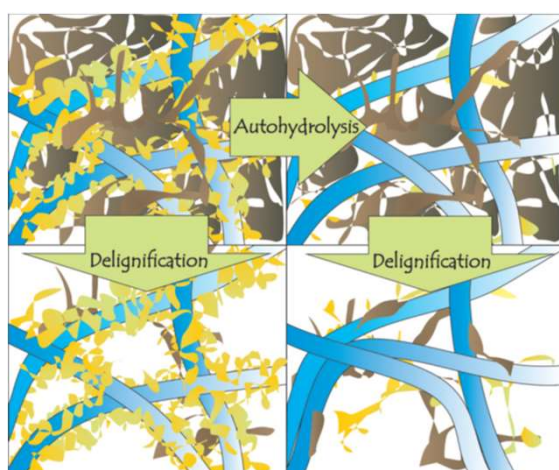
- Extensive H-bonding
- High dielectric constant
- Miscible with polar solvents
- Dissolves salts
- Does not dissolve cellulose



**Low density supercritical water  
250 bar at 400 ° C**

- Less H-bonds; compressible
- Low dielectric constant
- Miscible with non-polar solvents
- Cellulose solubility starts near the critical point; more favorable at higher pressure

## Prehydrolysis

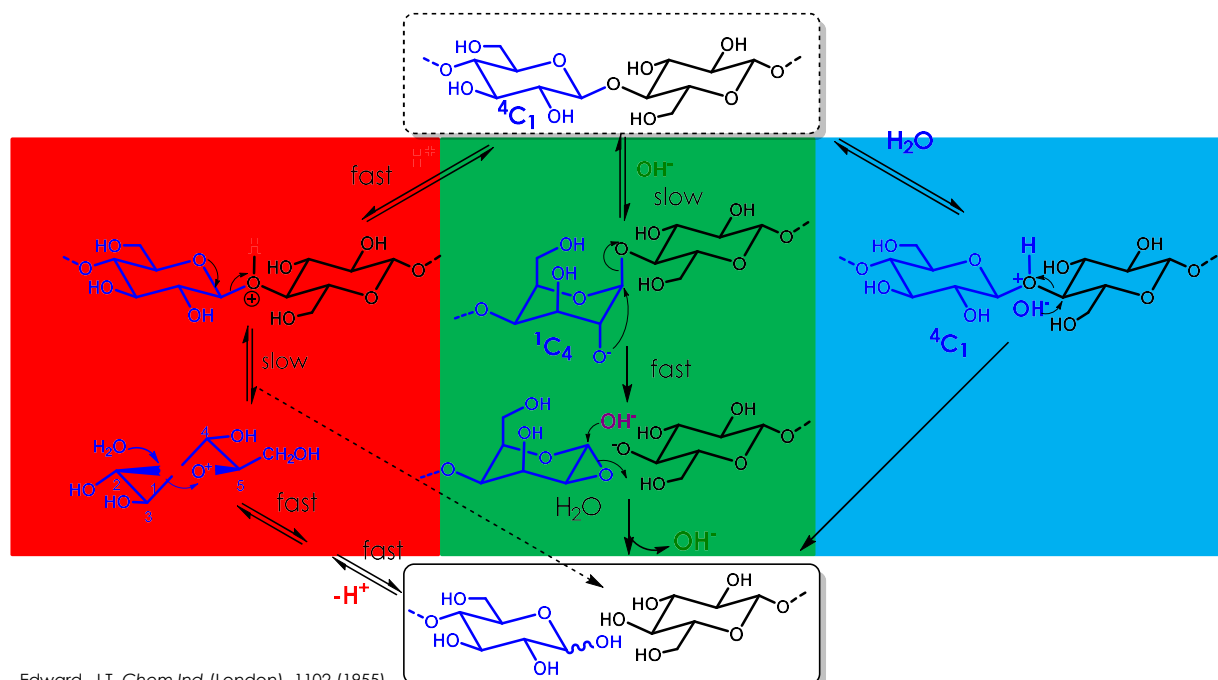


- Autohydrolysis effectively increases the cellulose surface area by hemicellulose dissolution
- The removal of lignin leads to a more accessible pore structure.
- Delignification increases the hydrophilicity of the remaining lignin, which also increases hydrolyzability

## Module 2

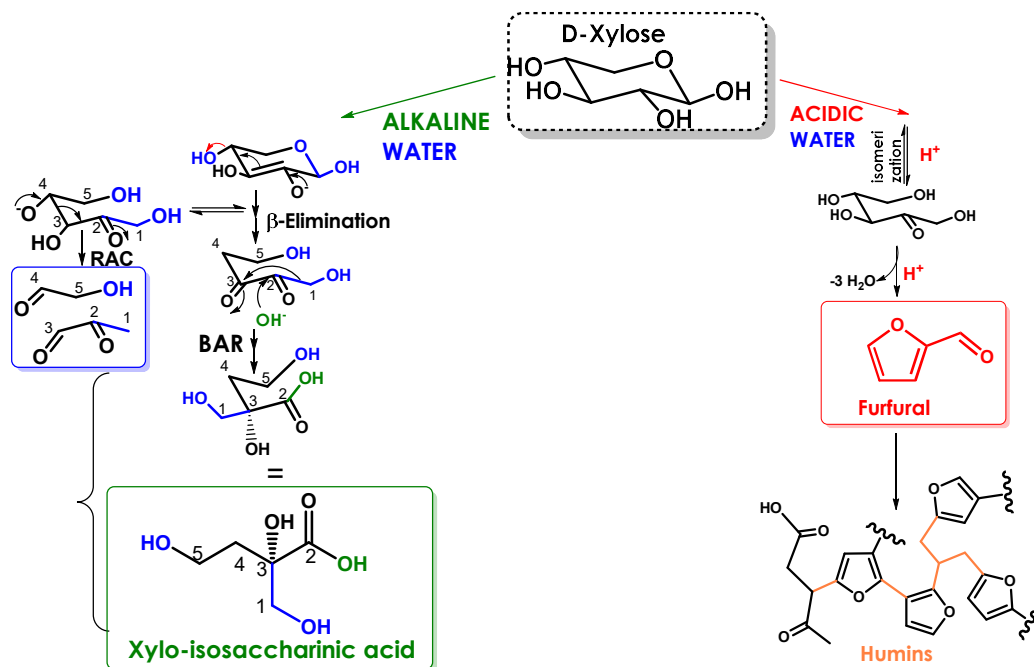
1. Introduction
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## Chemistry of glycosidic bond cleavage



Edward, J.T. *Chem. Ind. (London)*, 1102 (1955)

## Chemistry of xylose degradation in water



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## Prehydrolysis of Wood

- **Comparative evaluation of birch and pine**
- Selectivity of xylan removal
- Bound and free acetic acid in the hydrolysate
- Effect of liquor-to-wood-ratio
- Effect of wood particle size
- Batch- vs. percolation reactor
- Acid-catalyzed hydrolysis

## Intensity of Prehydrolysis

P-factor used in PHK<sup>1</sup>

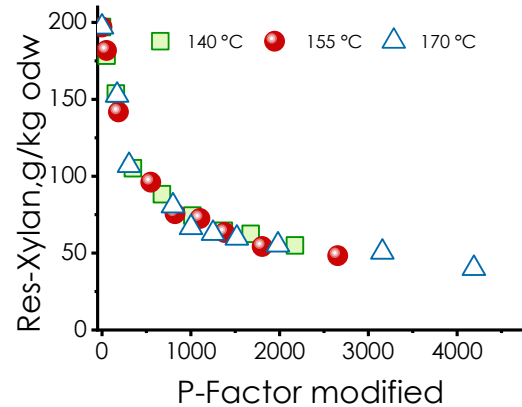
$$P = \int_{t_0}^t \frac{k_X}{k_{100^\circ\text{C}}} dt = \int_{t_0}^t \text{Exp} \left( 40.48 - \frac{15106}{T} \right) dt$$

$$P_{\text{mod}} = \int_{t_0}^t \frac{k_X}{k_{100^\circ\text{C}}} dt = \int_{t_0}^t \text{Exp} \left( 58.02 - \frac{21649}{T} \right) dt$$

Severity Factor<sup>2,3</sup>

$$\log(R_0) = \log \left[ t \cdot \exp \left( \frac{T - 100}{14.75} \right) \right]$$

$$\log(R_0^*) = \log(R_0) + |pH - 7|$$



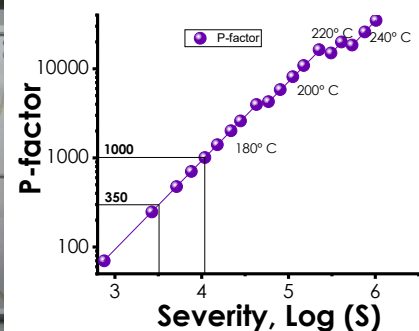
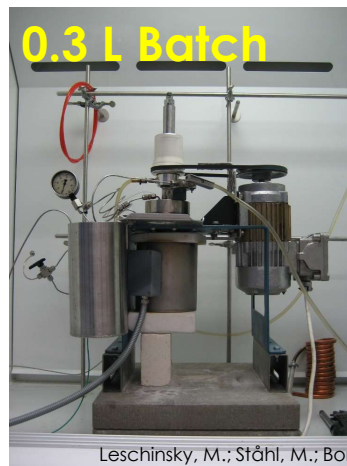
<sup>1</sup> Sixta, H. (2006) and (2011)

<sup>2</sup> Abatzoglou, N.J.; Chornet, E.; Belkacemi, K.; Overend, R.P. (1992), Chem. Eng Sci, 47, 1109-1122.

<sup>3</sup> Chum, H.L., D.K. Black, S.K.; Overend, R.P. (1990). Appl. Biochemistry and Biotechnology, 24/25, 1-14

## Birch vs Pine Prehydrolysis - Experimental

- Wood ground to particles < 1mm
- Liquor-to-wood ratio = 40:1 (m:m)
- Heating-up time converted to time at reaction temperature ( $t_{\text{corr}}$ )



Leschinsky, M.; Ståhl, M.; Borrega, M.; Testova, L.; Guetsch, J. Sixta, H.

## Wood composition

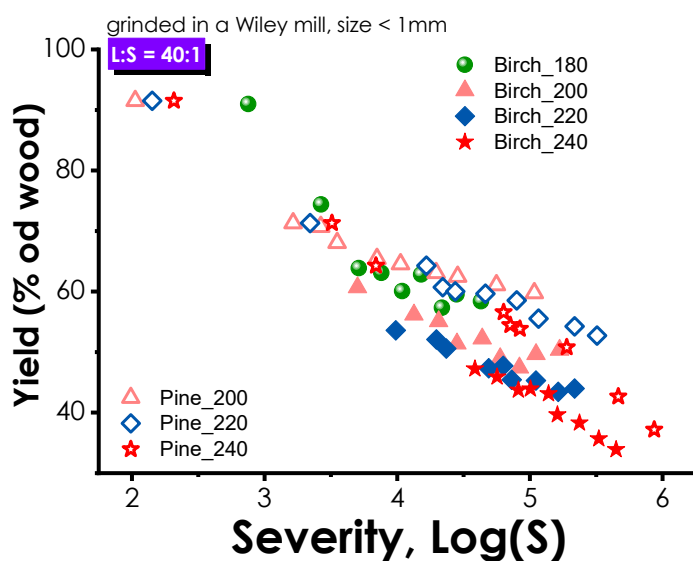
| Constituent                | % od birch   |
|----------------------------|--------------|
| Acetone-Extractives        | 2,0          |
| Klason Lignin              | 21,4         |
| Acid soluble lignin        | 4,4          |
| <b>Total Lignin</b>        | <b>25,8</b>  |
| <b>Xylose</b>              | <b>26,1</b>  |
| Arabinose                  | 0,3          |
| <b>Glucose</b>             | <b>38,3</b>  |
| Galactose                  | 0,7          |
| Mannose                    | 1,8          |
| 4OMeGlcA                   | 3,1          |
| Acetyl                     | 4,8          |
| <b>Total carbohydrates</b> | <b>75,1</b>  |
| <b>Total</b>               | <b>102,9</b> |

| Constituent                     | % od pine    |
|---------------------------------|--------------|
| <b>Acetone-Extractives</b>      | <b>3,0</b>   |
| Klason Lignin                   | 27,1         |
| Acid soluble lignin             | 0,6          |
| <b>Total Lignin</b>             | <b>27,6</b>  |
| <b>Arabinoxylan (AX)</b>        | <b>9,1</b>   |
| <b>Galactoglucomannan (GGM)</b> | <b>15,8</b>  |
| Other carbohydrates             | 2,4          |
| Uronic acids                    | 2,1          |
| <b>Cellulose</b>                | <b>40,9</b>  |
| <b>Total carbohydrates</b>      | <b>70,3</b>  |
| <b>Total</b>                    | <b>100,9</b> |

Testova, L. et al.: Holzforschung, Vol. 65, pp. 535–542, 2011

Markus Paananen et al. : Holzforschung 2015; 69(9): 1049–1058  
Ståhl, M. et al. Biomass and Bioenergy 109 (2018) 100–113

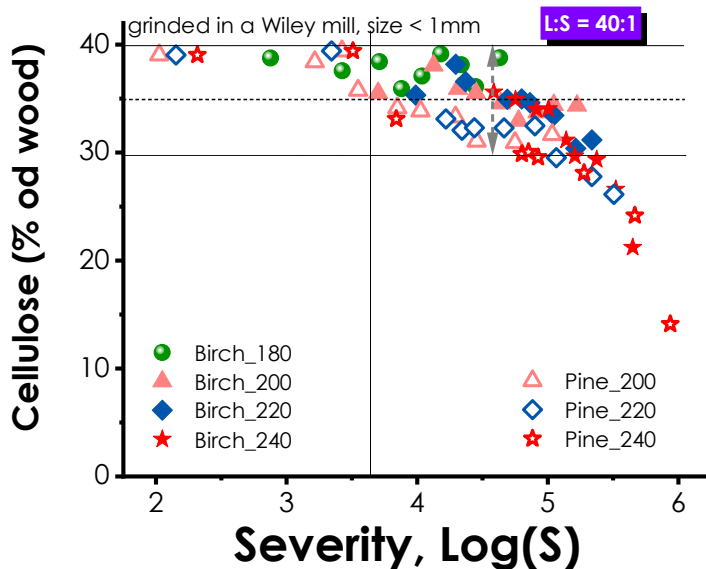
## Severity vs Yield



- $\text{Log}(S) \leq 3.5$ : pine ~ birch
- $\text{Log}(S) > 3.5$ :  $Y_{\text{pine}} > Y_{\text{birch}}$

Leschinsky, M.; Ståhl, M.; Borrega, M.; Testova, L.; Guetsch, J. Sixta, H.

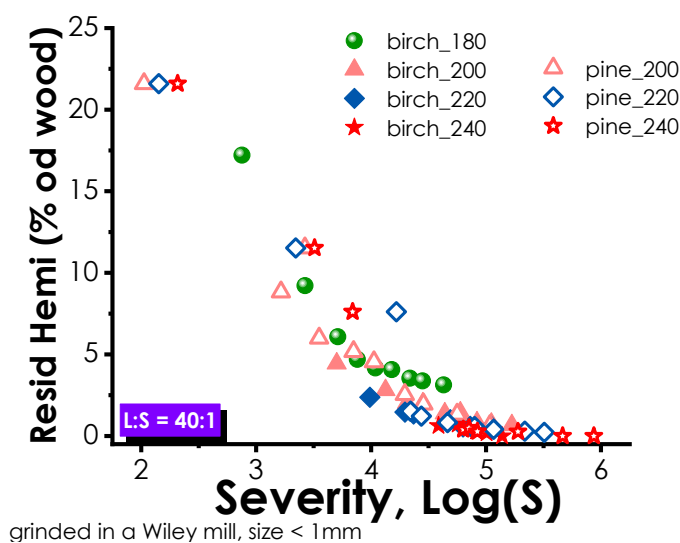
## Severity vs Cellulose yield in residue



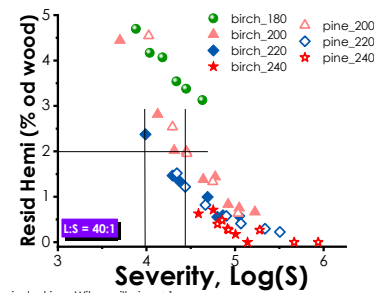
- $\text{Log}(S) \leq 3.5$ : pine ~ birch
- $3.5 < \text{Log}(S) < 5.1$ :  
 $Y_{\text{pine}} < Y_{\text{birch}}$
- $5.1 \leq \text{Log}(S)$ :  $Y_{\text{pine}} \sim Y_{\text{birch}}$

Leschinsky, M.; Stöhl, M.; Borrega, M.; Testova, L.; Guetsch, J. **Sixta, H.**

## Severity vs Hemi in residue



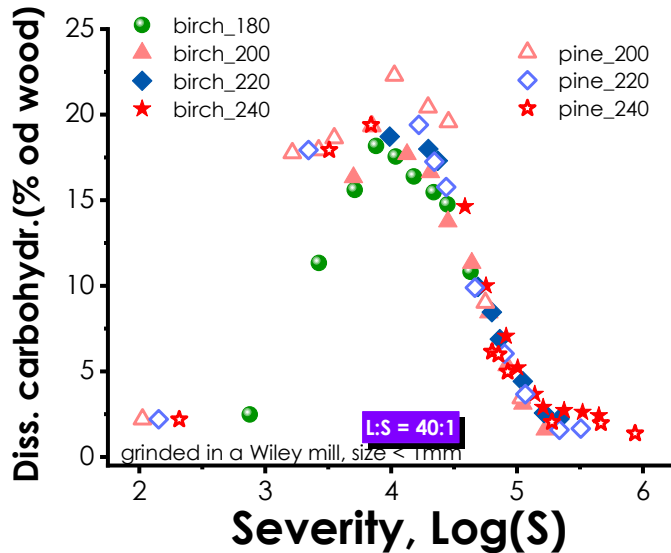
Despite the fact that pine and birch consist of different types of hemicelluloses, the removal kinetics of the sum of the hemicelluloses **seems to be quite comparable.**



Leschinsky, M.; Stöhl, M.; Borrega, M.; Testova, L.; Guetsch, J. **Sixta, H.**

grinded in a Wiley mill, size < 1 mm

## Severity vs Hemi in hydrolysate



Log(S) ~ 4.0:

highest amount of intact carbohydrates dissolved (pine and birch)

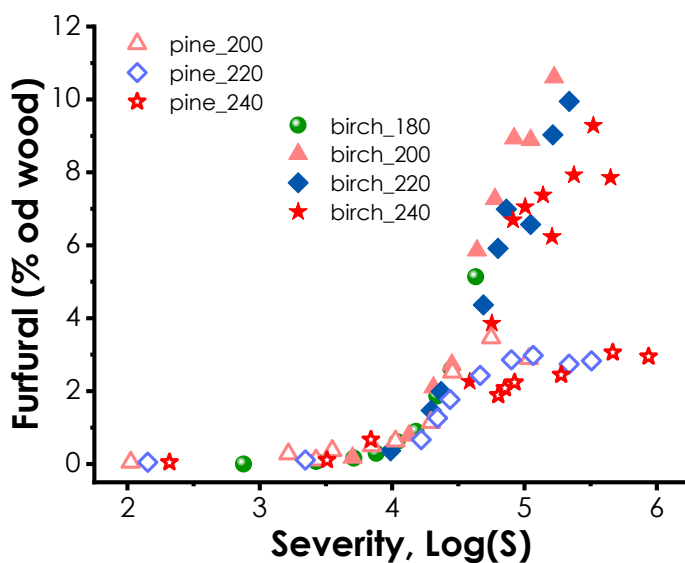
$3.2 < \text{Log}(S) < 4.5$ :

More carbohydrates dissolved from pine wood

\* Side chains: 4OMeGlcA and Acetyl groups not included

Leschinsky, M.; Ståhl, M.; Borrega, M.; Testova, L.; Guetsch, J. **Sixta, H.**

## Severity vs Furfural in hydrolysate

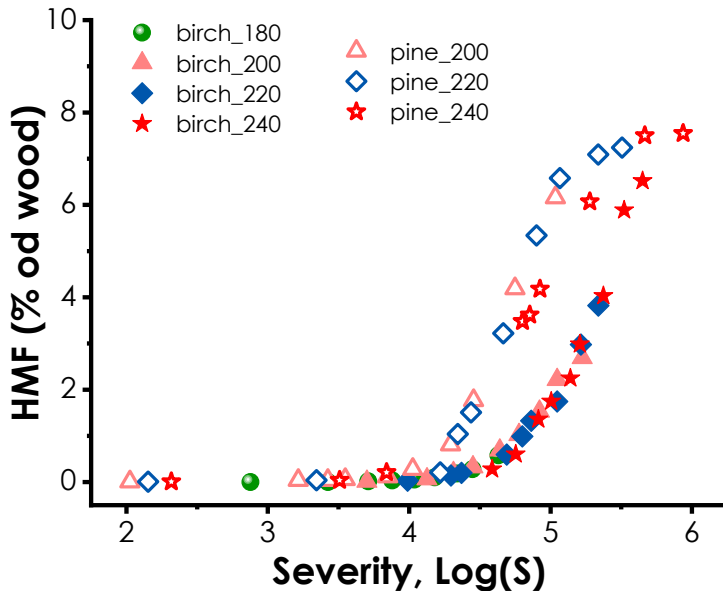


$4.2 < \text{Log}(S)$  :  
pine ~ birch

$4.2 \geq \text{Log}(S)$  :  
birch >> pine

Leschinsky, M.; Ståhl, M.; Borrega, M.; Testova, L.; Guetsch, J. **Sixta, H.**

## Severity vs HMF in hydrolysate



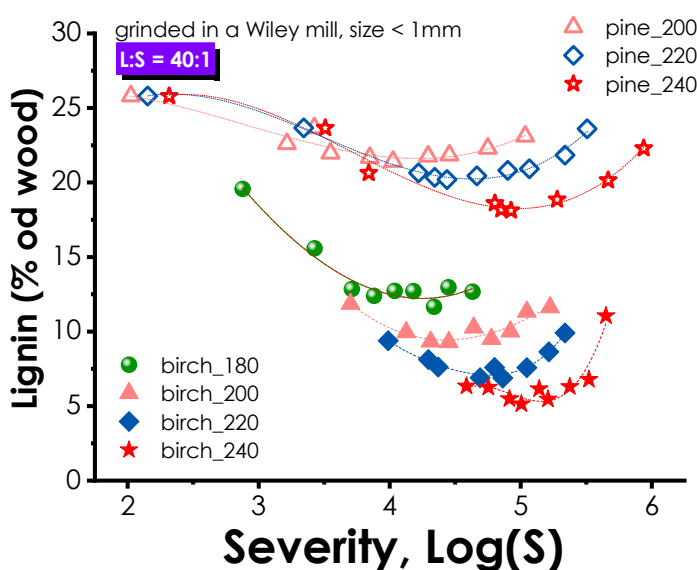
$4.2 < \text{Log}(S)$  :  
pine ~ birch

$4.2 \geq \text{Log}(S)$  :  
pine >> birch

$5.7 < \text{Log}(S)$ :  
pine ~ birch

Leschinsky, M.; Ståhl, M.; Borrega, M.; Testova, L.; Guetsch, J. **Sixta, H.**

## Severity vs Lignin in residue

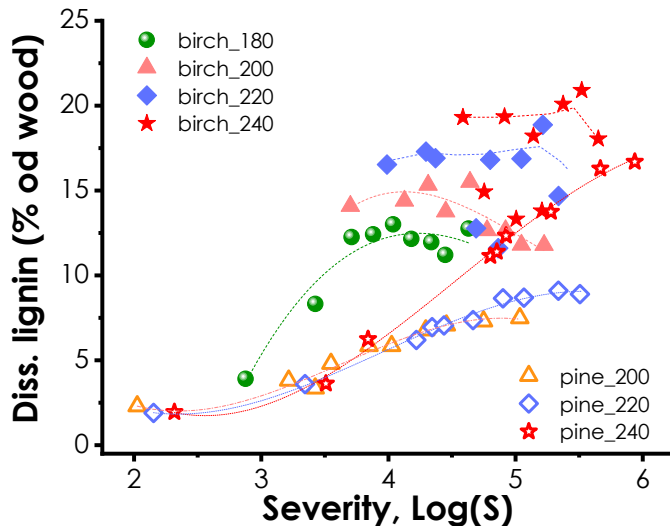


- lignin removal goes through a maximum, specific for each temperature, after which it decreased mainly triggered by progressive lignin condensation and re-precipitation

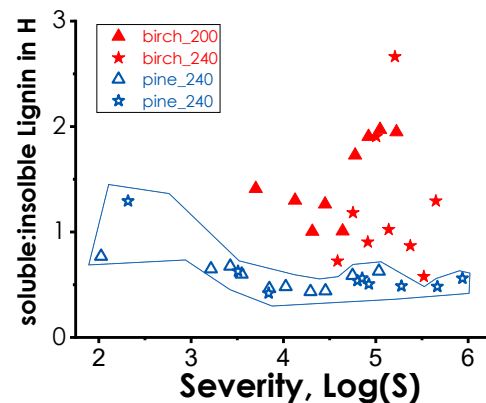
- Lignin removal:**  
**Birch Lignin >> Pine Lignin**

Leschinsky, M.; Ståhl, M.; Borrega, M.; Testova, L.; Guetsch, J. **Sixta, H.**

## Severity vs Lignin in hydrolysate



- Mirror image results in hydrolysate
- **Lignin removal:**  
**Birch Lignin >> Pine Lignin**
- **Pine: higher fraction of insoluble lignin in hydrolysate**



Leschinsky, M.; Ståhl, M.; Borrega, M.; Testova, L.; Guetsch, J. Sixta, H.

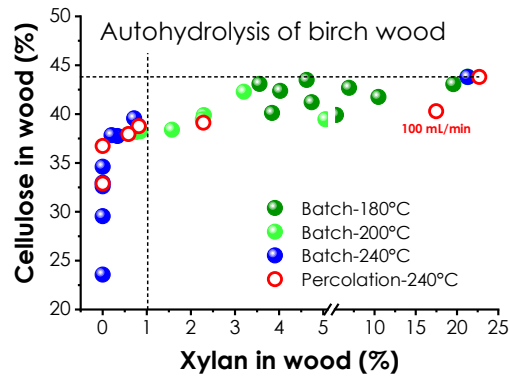
## Prehydrolysis of Wood

- Comparative evaluation of birch and pine
- **Selectivity of xylan removal**
- Bound and free acetic acid in the hydrolysate
- Effect on residual lignin
- Effect of liquor-to-wood-ratio
- Effect of wood particle size
- Batch- vs. percolation reactor
- Acid-catalyzed hydrolysis

## Prehydrolysis of birch wood

### Selectivity of Xylan Removal

Batch-L:W=40:1. Percolation-100 mL/min



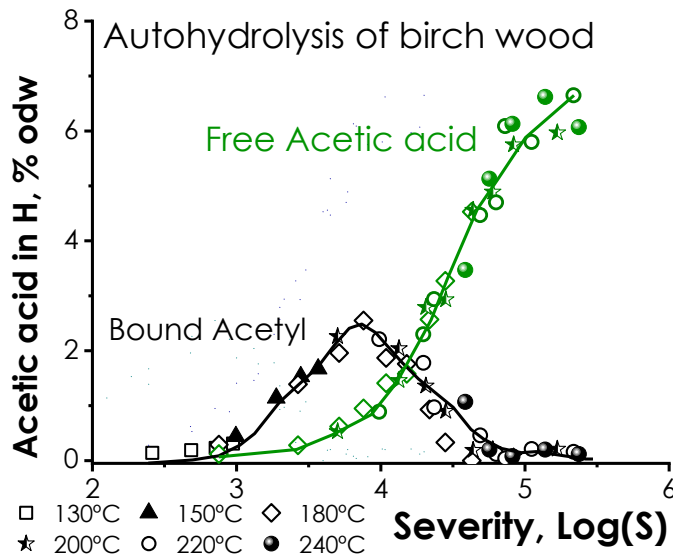
**Xyl > 3%** moderate cellulose loss  
**Xyl < 0.5%** severe cellulose loss

M.Borrega, K.Nieminen, H.Sixta. *Bioresource Technology* (2011) 102 (2011) 10724–10732

## Prehydrolysis of Wood

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## Bound and free acetic acid in Birch Hydrolysate



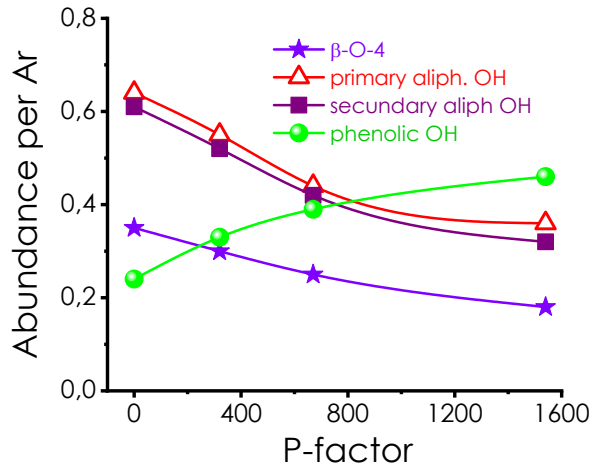
Testova, L. et al. *Holzforschung*, 2011, 65, pp. 535–542.  
M.Borrega, K.Nieminen, H.Sixta, *Bioresource Technology* (2011) 102 (2011) 10724–10732  
Guetsch, J.G.; Nousiainen, T.; Sixta, H: *Bioresource Technology* 109 (2012) 77–85

\* batch autoclave, V = 0.3 L, L:S = 40:1

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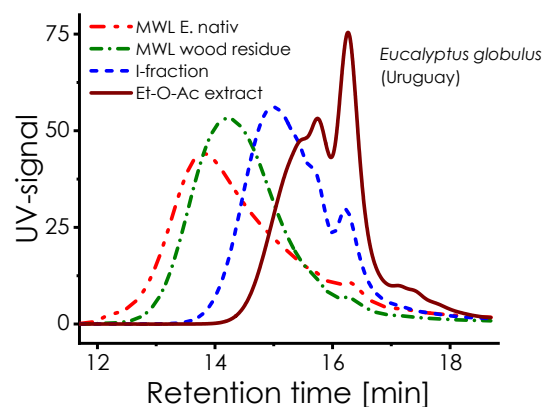
## Effect on Residual Lignin of *E. globulus*



| Residual Lignin (MWL) |                              |         |                               |
|-----------------------|------------------------------|---------|-------------------------------|
| P-factor              | S/G                          | PhenOH  | COOH                          |
|                       | <sup>13</sup> C & Q-DEPT NMR | mol/mol | <sup>31</sup> P NMR<br>mmol/g |
| 0                     | 1,98                         | 0,22    | 0,18                          |
| 200                   | 1,68                         | 0,33    | 0,18                          |
| 750                   | 1,57                         | 0,37    | 0,23                          |

Leschinsky, M., et al., *Holzforschung*, **2008**, *62*(6) 645-652  
 Leschinsky, M., et al., *Holzforschung*, **2008**, *62*(6) 653-658

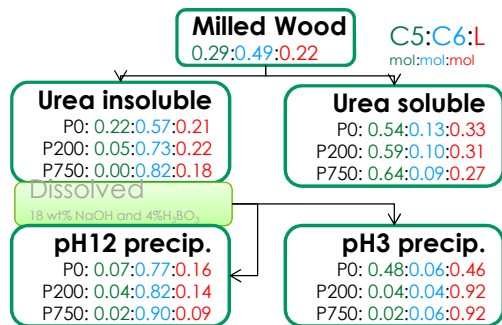
## Effect on Residual Lignin of *E. globulus*



Leschinsky, Moritz: Doctoral Dissertation, Faculty of Mathematics, Informatics and Natural Sciences, University of Hamburg, **2009**

## Effect on residual lignin of birch

### Fractionation of Lignin-Carbohydrate Complexes (LCCs)



As the intensity of the prehydrolysis increases, the proportion of the LCC fraction in the residual lignin of the birch decreases.

### Conclusions:

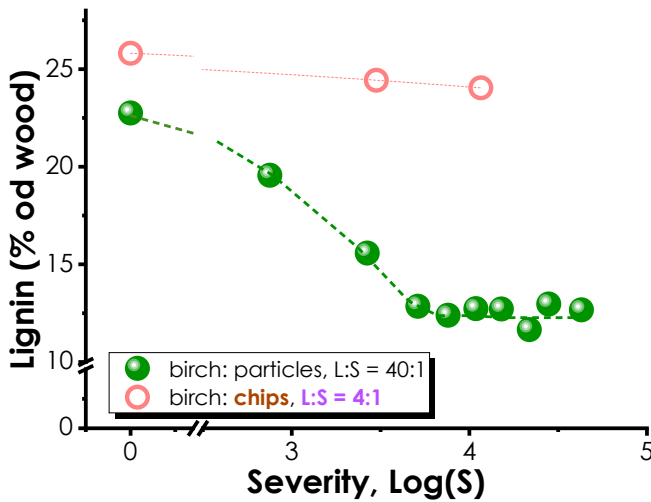
Prehydrolysis leads to a cleavage of the LCC bonds

Rauhala, T. et al. *NPPRJ*, **2011**, 26(4), 386-391  
Guetsch, J., H. Sixta. *Holzforschung*, **2011**, **65**, 511-518

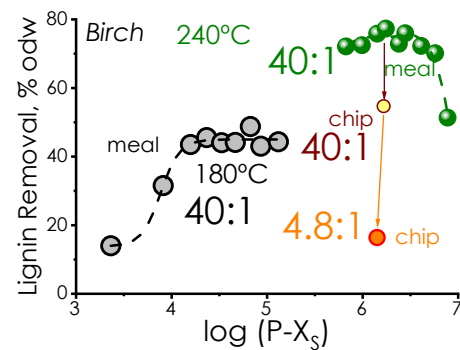
## Prehydrolysis of Wood

- Comparative evaluation of birch and pine
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## Effect of Liquor-to-wood ratio



Decrease of L:S leads to a significantly reduced delignification



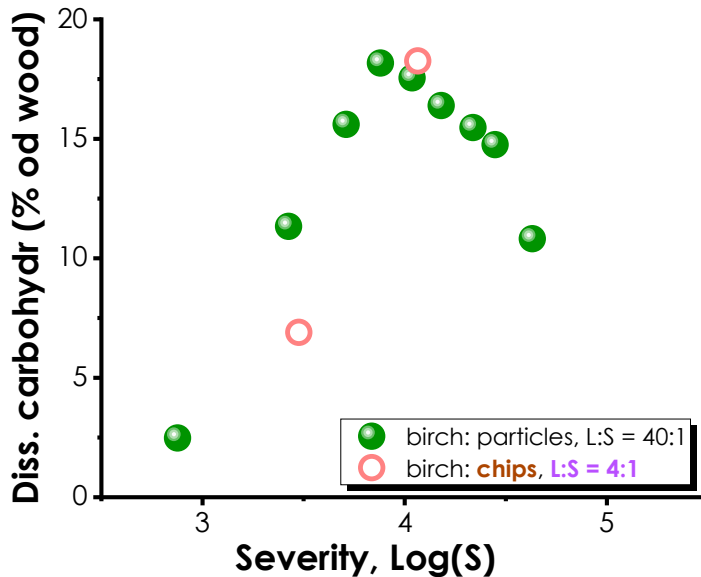
Borrega, M. et al. BioResources, 6(2), (2011) 1890-1903  
 Ståhl, M. et al. Biomass and Bioenergy, 109 (2018), 100-113

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## Prehydrolysis of Wood

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## Particle size, L:S on carbohydrate yield

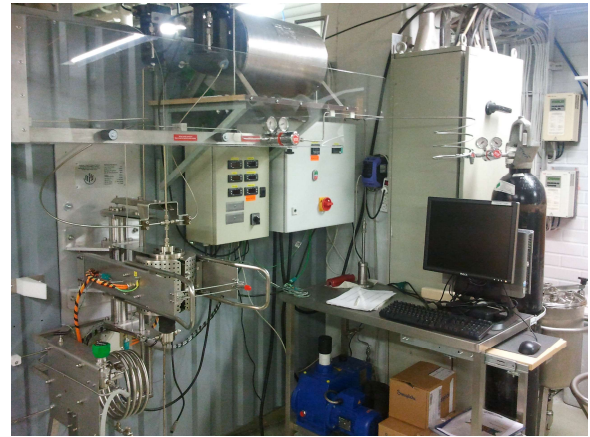
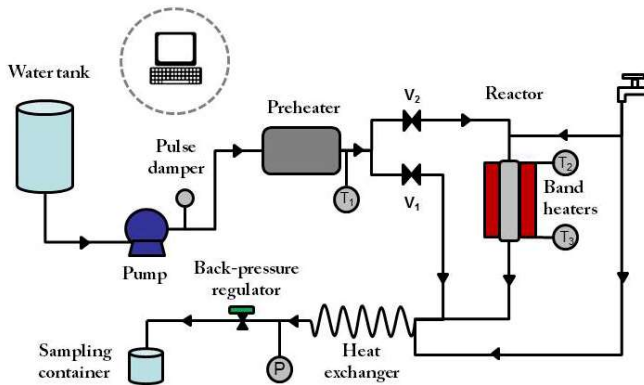


Effect of combined L:S and particle size on carbohydrate removal low

## Prehydrolysis of Wood

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- **Batch- vs. percolation reactor**
- Acid-catalyzed hydrolysis

## Percolation-type of reactor

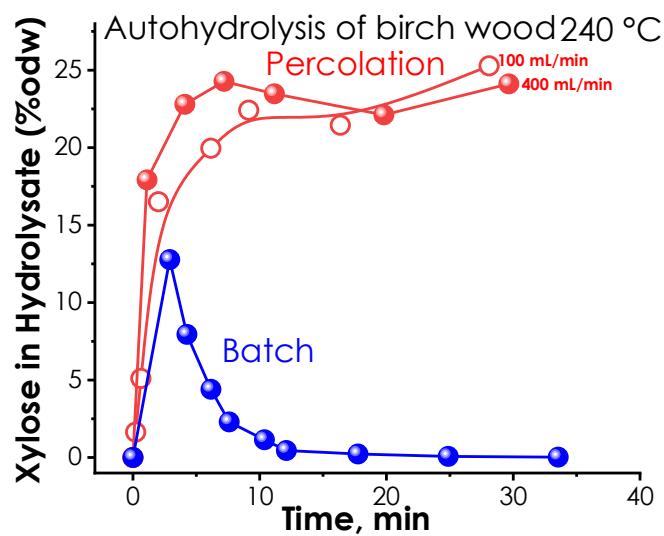


$$V_{\text{reactor}} = 190 \text{ mL}$$

Marc Borrega, PhD

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## Batch vs Percolation-type of reactors



**Batch:** Maximum xylose yield 15 - 17% odw

**Percolation:** Theoretical xylose yield of 25% odw

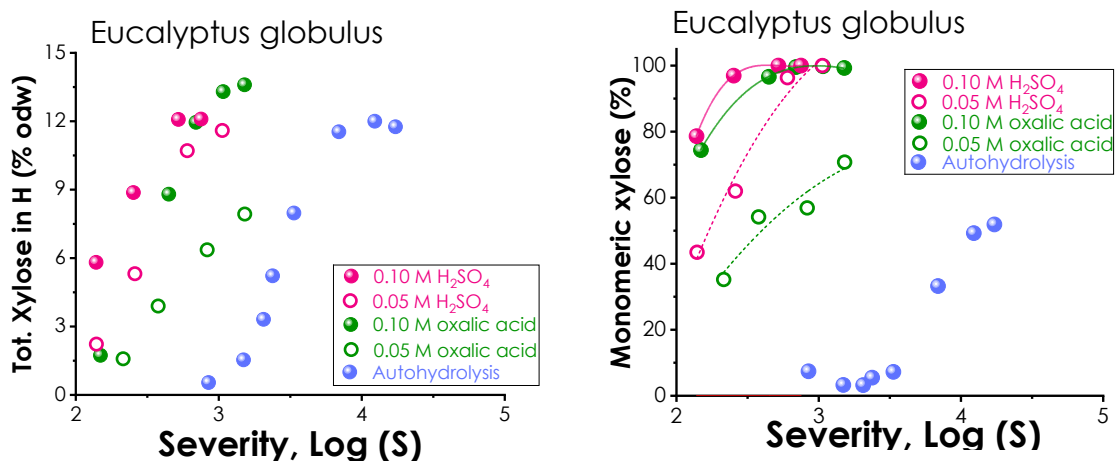
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## Prehydrolysis of Wood

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- Effect of wood particle size
- Batch- vs. percolation reactor
- **Acid-catalyzed hydrolysis**

## Acid catalyzed hydrothermal treatment

Acidity can be compensated by temperature, and vice versa!



Maximum xylose yield: 12-13 wt% odw

Realistic xylose yield: 8 – 9 wt% odw

because the xylose remaining in the void fraction of the chips,  $V_V = \frac{1}{\rho_{dw}} - \frac{1}{1.53}$ , cannot be recovered.

## Module 2

1. Introduction
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## Kinetic Modeling of Prehydrolysis

$$-\frac{dX}{dt} = z_X \cdot k_{f,X} \cdot X_f + (1 - z_X) \cdot k_{s,X} \cdot X_s \quad (1)$$

$$z_X = \frac{(X - X_s)}{X} = \frac{X_f}{X} \quad (2)$$

$X$ : fraction of original xylan remaining in the solid  
 $X_f$ : fraction of the fast – reacting xylan remaining in the solid  
 $X_s$ : fraction of the slowly – reacting xylan remaining in the solid  
 $z_X$ : fraction of the readily reacting xylan  
 $k_{f,X}, k_{s,X}$ : rate constants

Non-linear regression (least squares) analysis is applied to determine the best values for the coefficients in the integrated form of equ 1.

$$X = z_X \cdot \text{Exp}(-k_{f,X} \cdot t) + (1 - z_X) \cdot \text{Exp}(-k_{s,X} \cdot t) \quad (3)$$

## Heating-up time correction

$$t_{T_0} = \int_{t_{T_t}}^{t_{T_0}} \text{Exp} \left( \frac{E_A}{R} \cdot \left[ \frac{1}{T_{T_t}} - \frac{1}{T_0} \right] \right)$$

|            |        |
|------------|--------|
| Ea, kJ/mol | 120,0  |
| Ea/R       | 14433  |
| T [°C]     | 150    |
| T [K]      | 423,15 |

$T_t$ : temperature during heating – up

$T_0$ : target temperature

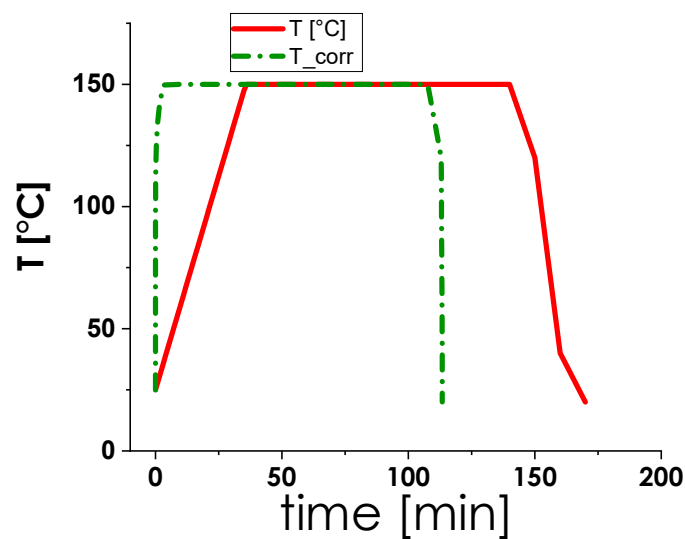
$E_A$ : factivation temperature

| time [min] | t_corr [min] | T [°C] | T [K] | exp(-Ea/R*(1/Te-1/Tf)) | delta |
|------------|--------------|--------|-------|------------------------|-------|
| 0          | 0,0          | 25     | 298,2 | 0,000                  | 0,000 |
| 1          | 0,0          | 29     | 301,7 | 0,000                  | 0,000 |
| 4          | 0,0          | 39     | 312,2 | 0,000                  | 0,000 |
| 7          | 0,0          | 50     | 322,7 | 0,000                  | 0,000 |
| 10         | 0,0          | 60     | 333,2 | 0,000                  | 0,000 |
| 13         | 0,0          | 71     | 343,7 | 0,000                  | 0,000 |
| 16         | 0,0          | 81     | 354,2 | 0,001                  | 0,002 |
| 19         | 0,0          | 92     | 364,7 | 0,004                  | 0,005 |
| 22         | 0,0          | 102    | 375,2 | 0,013                  | 0,015 |
| 25         | 0,1          | 113    | 385,7 | 0,036                  | 0,044 |
| 28         | 0,3          | 123    | 396,2 | 0,098                  | 0,116 |
| 31         | 0,8          | 134    | 406,7 | 0,251                  | 0,295 |
| 34         | 2,0          | 144    | 417,2 | 0,612                  | 0,714 |
| 37         | 4,6          | 150    | 423,2 | 1,000                  | 1,000 |
| 38         | 5,6          | 150    | 423,2 | 1,000                  | 1,000 |
| 39         | 6,6          | 150    | 423,2 | 1,000                  | 1,000 |

$$t_{corr} = (t_t - t_{t-1}) \cdot (t_{t,T_0} + t_{t+1,T_0})/2 + t_{corr-1}$$

Sixta, H. Handbook of Pulp (2006)

## Heating-up time correction



Sixta, H. Handbook of Pulp (2006)

## P-factor concept

$$P = \int_{t_0}^t k_{rel} \cdot dt \quad (5)$$

$$\ln(k_{X(T)}) = \ln(A) - \frac{E_{A,X}}{R} \cdot \frac{1}{T} \quad (6)$$

$$\ln(k_{X,100^\circ C}) = \ln(A) - \frac{E_{A,X}}{R} \cdot \frac{1}{373.15} \quad (7)$$

$$\ln\left(\frac{k_{X(T)}}{k_{X,100^\circ C}}\right) = \frac{E_{A,X}}{R \cdot 373.15} - \frac{E_{A,X}}{R \cdot T} \quad (8)$$

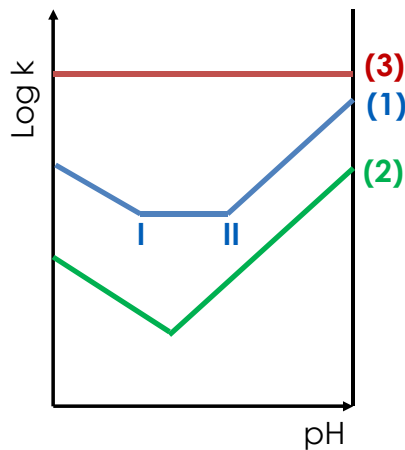
$$k_{rel} = \frac{k_{X(T)}}{k_{X,100^\circ C}} = \exp \cdot \left(40.48 - \frac{15106}{T}\right) \quad (9)$$

$$P = \int_{t_0}^t \frac{k_{X(T)}}{k_{X,100^\circ C}} \cdot dt = \int_{t_0}^t \exp \cdot \left(40.48 - \frac{15106}{T}\right) \cdot dt \quad (10)$$

Sixta, H. Handbook of Pulp (2006)

| <b>E<sub>a</sub>=</b>                                                                |                   | <b>125,6</b> [kJ/mol]          |                                          |                  |                |                                   |                 |
|--------------------------------------------------------------------------------------|-------------------|--------------------------------|------------------------------------------|------------------|----------------|-----------------------------------|-----------------|
| $k_r=\text{EXP}(((1000\cdot E_a/373\cdot 8,31)-(1000\cdot E_a/(8,31\cdot (273+T))))$ |                   |                                |                                          | <b>[T = °C]</b>  |                |                                   |                 |
| <b>Input Data</b>                                                                    |                   | Only in the yellow shaded area |                                          |                  |                |                                   |                 |
| <b>Result</b>                                                                        |                   | green shaded area              |                                          |                  |                |                                   |                 |
| <b>Zeit</b><br>min                                                                   | <b>1143</b><br>°C | <b>k<sub>r</sub></b>           | <b>(k<sub>r</sub>+k<sub>r-1</sub>)/2</b> | <b>dt</b><br>min | <b>dt</b><br>h | <b>P-F1</b><br>bei t <sub>n</sub> | <b>P factor</b> |
| <b>0</b>                                                                             | <b>80,0</b>       | 0,1                            |                                          | 0                |                | 0                                 | <b>0</b>        |
| <b>4</b>                                                                             | <b>85,0</b>       | 0,2                            | 0,1                                      | 4                | 0,07           | 0                                 | <b>0</b>        |
| <b>6</b>                                                                             | <b>90,0</b>       | 0,3                            | 0,3                                      | 2                | 0,03           | 0                                 | <b>0</b>        |
| <b>8</b>                                                                             | <b>95,0</b>       | 0,6                            | 0,5                                      | 2                | 0,03           | 0                                 | <b>0</b>        |
| <b>10</b>                                                                            | <b>100,0</b>      | 1,0                            | 0,8                                      | 2                | 0,03           | 0                                 | <b>0</b>        |
| <b>18</b>                                                                            | <b>120,0</b>      | 7,9                            | 6,3                                      | 2                | 0,03           | 0                                 | <b>0</b>        |
| <b>26</b>                                                                            | <b>140,0</b>      | 50,6                           | 41,5                                     | 2                | 0,03           | 1                                 | <b>4</b>        |
| <b>28</b>                                                                            | <b>145,0</b>      | 78,4                           | 64,5                                     | 2                | 0,03           | 2                                 | <b>6</b>        |
| <b>30</b>                                                                            | <b>150,0</b>      | 120,3                          | 99,4                                     | 2                | 0,03           | 3                                 | <b>9</b>        |
| <b>34</b>                                                                            | <b>160,0</b>      | 274,5                          | 228,5                                    | 2                | 0,03           | 8                                 | <b>22</b>       |
| <b>38</b>                                                                            | <b>170,0</b>      | 603,6                          | 506,2                                    | 2                | 0,03           | 17                                | <b>50</b>       |
| <b>40</b>                                                                            | <b>170,0</b>      | 603,6                          | 603,6                                    | 2                | 0,03           | 20                                | <b>70</b>       |
| <b>50</b>                                                                            | <b>170,0</b>      | 603,6                          | 603,6                                    | 2                | 0,03           | 20                                | <b>171</b>      |
| <b>60</b>                                                                            | <b>170,0</b>      | 603,6                          | 603,6                                    | 2                | 0,03           | 20                                | <b>271</b>      |
| <b>70</b>                                                                            | <b>170,0</b>      | 603,6                          | 603,6                                    | 2                | 0,03           | 20                                | <b>372</b>      |
| <b>72</b>                                                                            | <b>170,0</b>      | 603,6                          | 603,6                                    | 2                | 0,03           | 20                                | <b>392</b>      |
| <b>74</b>                                                                            | <b>170,0</b>      | 603,6                          | 603,6                                    | 2                | 0,03           | 20                                | <b>412</b>      |

## General kinetics of hydrolysis reactions



$$k = k_w + k_a[H^+] + k_b[OH^-]$$

The minimum reaction rate constant  
(by differentiation of  $k$  according to  $[H^+]$ )

$$k_0 = k_w + 2\sqrt{k_a k_b [H^+][OH^-]}$$

### 3 Cases

1.  $pH < I$ :  $k_a[H^+] \uparrow$
- $I < pH < II$ :  $k_w \uparrow$
- $pH > II$ :  $k_b[OH^-] \uparrow$

e.g. Saponification of lactic acid ester

$$2. k_w \ll 2\sqrt{k_a k_b [H^+][OH^-]}$$

e.g. Hydrolysis of acid amides

$$3. k_w > 2\sqrt{k_a k_b [H^+][OH^-]}$$

e.g. Carbon dioxide cleavage of carboxylic acids

Skrabal, A. Ueber ein sehr allgemeines Zeitgesetz der chem. Kinetik und seine Deutung. Die Hydrolyse Geschwindigkeit der Organooxyde. *Z. Elektrochem.* 1927, 33, 322.

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## Simplified kinetics of cellulose hydrolysis



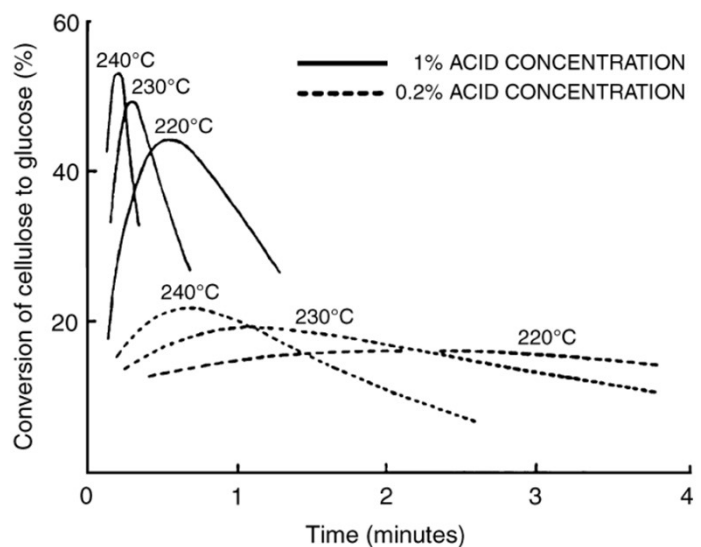
$$\frac{d[C]}{dt} = (k_w + k_a[H^+] + k_b[OH^-]) \cdot [C]$$

$$\frac{d[C]}{dt} = (k_w + k_a[H^+] + k_b[OH^-]) \cdot [C] = k_1[C]$$

$$[Glu] = [C]_0 \frac{k_1}{k_2 - k_1} (e^{-k_1 t} - e^{-k_2 t})$$

High glucose formation can only be reached when  $k_1 \gg k_2$ .

Acid hydrolysis at 1 wt%  $[H^+]$  leads to 50% **Glu** at 230-240°C

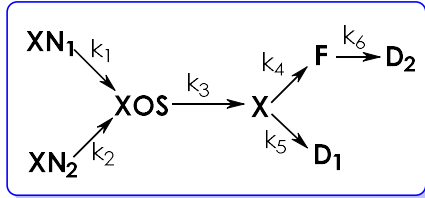


Bobleter, O. Polysaccharides (2nd edition) 2005, 893-936

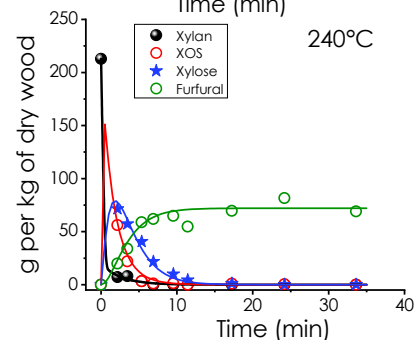
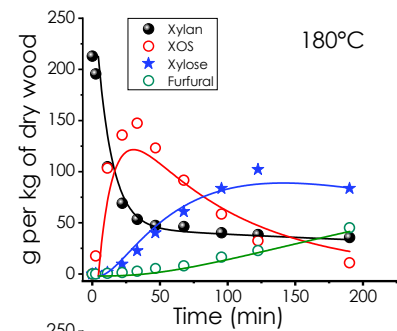
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# Kinetics of xylan degradation in wood

## Birch Wood



$$\begin{aligned}
 \frac{d[\text{XN}_1]}{dt} &= -k_1[\text{XN}_1] \\
 \frac{d[\text{XN}_2]}{dt} &= -k_2[\text{XN}_2] \\
 \frac{d[\text{XOS}]}{dt} &= k_1[\text{XN}_1] + k_2[\text{XN}_2] - k_3[\text{XOS}] \\
 \frac{d[\text{X}]}{dt} &= k_3[\text{XOS}] - (k_4 + k_5)[\text{X}] \\
 \frac{d[\text{F}]}{dt} &= k_4[\text{X}] - k_6[\text{F}]
 \end{aligned}$$



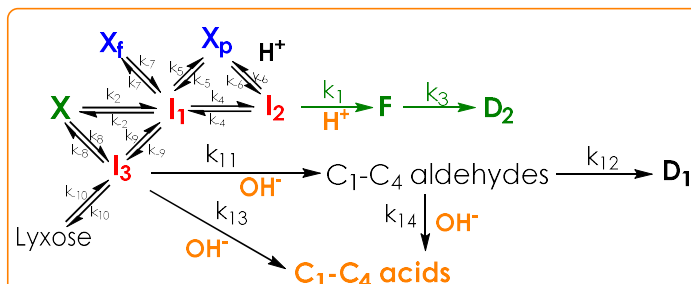
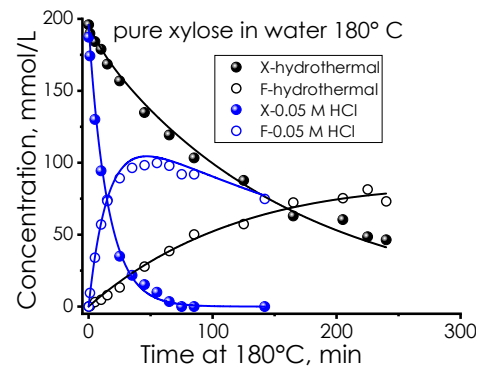
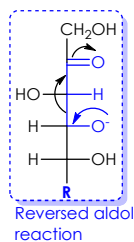
M.Borrega, K.Nieminen, H.Sixta. *Bioresource Technology* (2011) 102 (2011) 10724–10732

5 g extractive-free wood meal, L:S=40:1,  $V_{\text{batch}}=0.3$  L

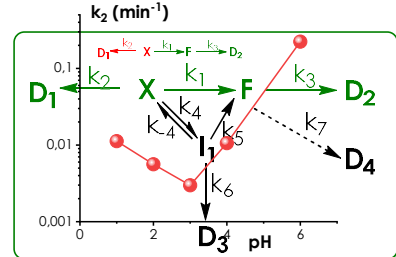
# Hydrothermolysis kinetics of xylose

| Parameter, g/kg od w  | Treatments |             |
|-----------------------|------------|-------------|
| <b>P-factor</b>       | <b>766</b> | <b>8166</b> |
| Temperature, °C       | 180        | 220         |
| Time, min             | 30         | 25          |
| L:W                   | 3          | 3           |
| Sugars                | 98         | 8           |
| Furans (F+HMF)        | 12         | 59          |
| Acetic/formic acid    | 19         | 71          |
| C2-C4 aliphatic acids | 2          | 9           |
| <b>TOTAL</b>          | <b>131</b> | <b>147</b>  |
| <b>YIELD LOSS</b>     | <b>191</b> | <b>407</b>  |

Borrega, M.; Niemela K.; Sixta, H. *Holzforschung* **2013**; 67(8): 871–879



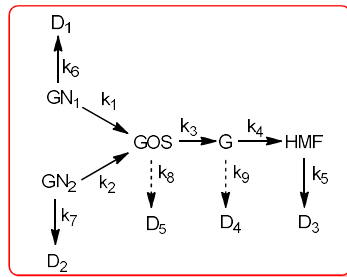
Monatshette fuer Chemie 123, 547-556 (1992)



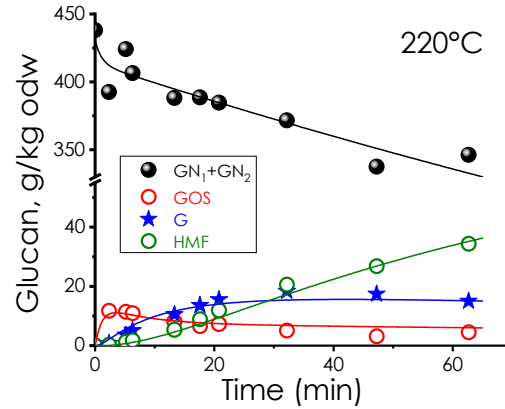
Ershova, O.; Nieminen, K.; Sixta, H. *ChemCatChem* **2017**, 9, 3031 – 3040  
Sixta, H. unpublished results (2009)

# Kinetics of cellulose degradation in wood

## Birch Wood



$$\begin{aligned}\frac{d[GN_1]}{dt} &= -(k_1 + k_6)GN_1 \\ \frac{d[GN_2]}{dt} &= -(k_1 + k_7)GN_2 \\ \frac{d[GOS]}{dt} &= k_1GN_1 + k_2GN_2 - (k_3 + k_8)GOS \\ \frac{d[G]}{dt} &= k_3GOS - (k_4 + k_9)G \\ \frac{d[HMF]}{dt} &= k_4G - k_5HMF\end{aligned}$$



M.Borrega, K.Nieminen, H.Sixta, *Bioresource Technology* (2011) 102 (2011) 10724–10732

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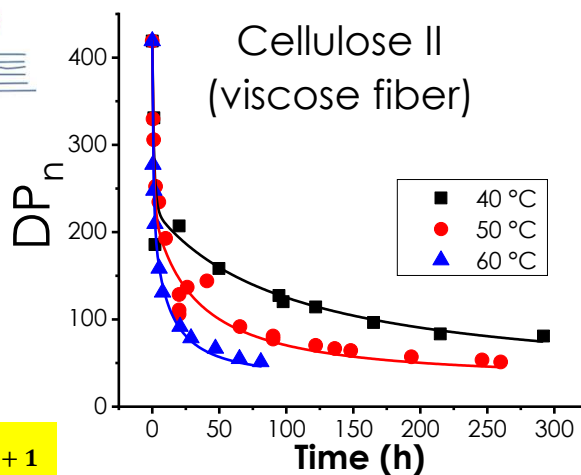
# Cellulose Depolymerization Model

$$\begin{cases} \frac{dM}{dt} = -k_1M \\ \frac{dH_1}{dt} = k_1M \\ \frac{dW}{dt} = -k_2W \\ \frac{dH_2}{dt} = k_2W \end{cases} \quad \begin{cases} M = M_0 e^{-k_1 t} \\ H_1 = M_0 (1 - e^{-k_1 t}) \\ W = W_0 e^{-k_2 t} \\ H_2 = W_0 (1 - e^{-k_2 t}) \end{cases}$$

$$DP = \frac{DP_0}{H_1 + H_2 + 1}$$

$$\frac{DP_0}{DP} - 1 = CS = M_0(1 - e^{-k_1 t}) + W_0(1 - e^{-k_2 t}) + 1$$

$M$  – number of amorphous segments with normal degradation rate  
 $W$  – number of amorphous segments containing weakly linked glycosidic bonds  
 $H_1$  – number of chain breaks in normal amorphous segments  
 $H_2$  – number of chain breaks in weakly linked subcategories  
 $k_1$  – normal rate constant  
 $k_2$  – fast rate constant (cleavage of weakly linked elements)

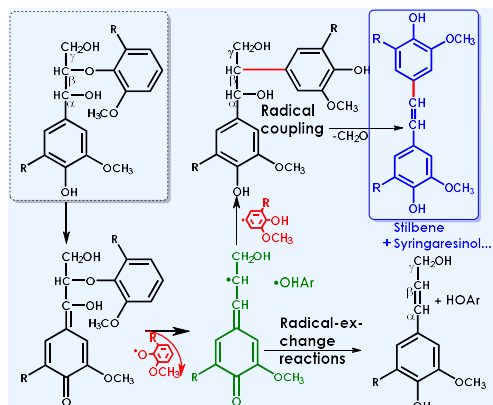


Cellulose (2016) 23:213–229  
 K. Nieminen, Sixta, H. (2015)

## Delignification mechanisms

### Mildly acidic conditions

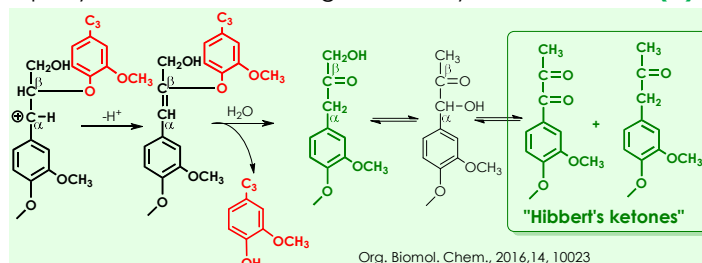
Homolytic cleavage of the  $\beta$ -aryl ether (C)



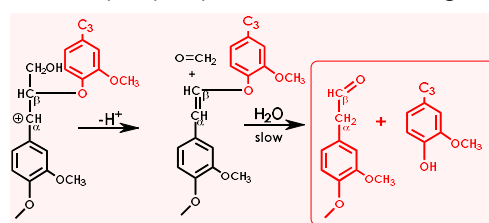
Li, S.; Lundquist, K. NPPRJ, 2000, 15, 292

### More strongly acidic conditions

$\beta$ -aryl ether bond cleavage via benzylic carbo cation (A)



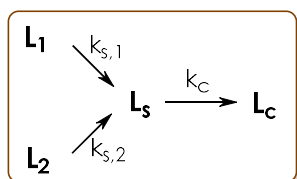
Acidolytic  $\beta$ -aryl ether bond cleavage (B)



(Meshgini, M., Sarkanen, K.V. (1989))

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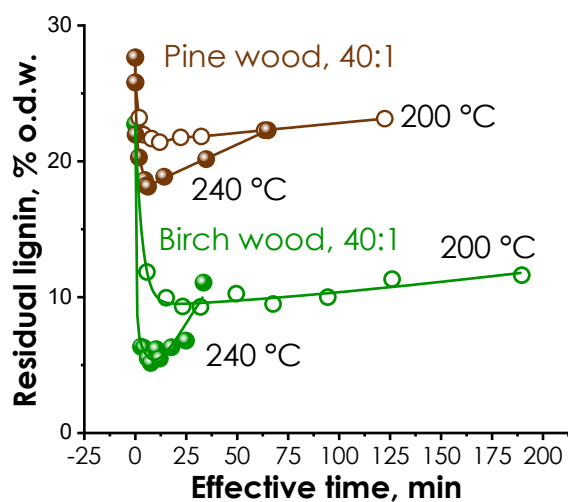
## Delignification kinetics



$$\begin{aligned} \frac{dL_1}{dt} &= -k_{s,1}L_1 \\ \frac{dL_2}{dt} &= -k_{s,2}L_2 \\ \frac{dL_s}{dt} &= k_{s,1}L_1 + k_{s,2}L_2 - k_cL_s \\ \frac{dL_c}{dt} &= k_cL_s \end{aligned}$$

| Species | Temp, °C | Portions, % |      | Reaction rates, min <sup>-1</sup> |                |                |
|---------|----------|-------------|------|-----------------------------------|----------------|----------------|
|         |          | Fast        | Slow | k <sub>1</sub>                    | k <sub>2</sub> | k <sub>c</sub> |
| Birch   | 200      | 58          | 42   | 0,294                             | 0,004          | 0,003          |
| Pine    | 200      | 22          | 78   | 0,786                             |                | 0,003          |
| Birch   | 220      | 61          | 39   | 0,858                             | 0,036          | 0,010          |
| Pine    | 220      | 29          | 71   | 10,060                            | 0,240          | 0,007          |
| Birch   | 240      | 63          | 37   | 2,538                             | 0,128          | 0,019          |
| Pine    | 240      | 38          | 63   | 27,740                            | 0,370          | 0,010          |

Borrega, M. et al. BioResources, 6(2), (2011) 1890-1903  
Ståhl, M. et al. Biomass and Bioenergy, 109 (2018), 100-113



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## Module 2

1. Introduction
2. Chemistry
3. Kinetics
4. Technology → Module 3