

MEC-E5003

FLUID POWER BASICS

Study Year 2018 - 2019

Fluid conditioning

- Filters
- Heat exchangers
- Extra:
 - The reservoir
 - Piping components



Main themes

- Contamination control
- Temperature control

Lecture themes

Does the cleanliness of the fluid matter, i.e., should the "trash" be removed from the system?

Warmth is nice, but how about the temperature?

(Reservoir, a storage for fluid, or is it also something else?)

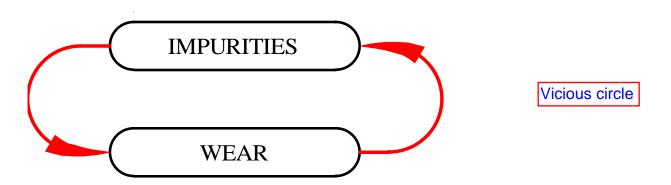
(How to conduct fluid from pumps to valves and actuators?)



Filters

Maintain the cleanliness of fluid

! Impurities cause ~70–80 % of all malfunctions of hydraulic systems





Impacts of the impurities

- weaken the properties of fluid
- shorten the useful life of fluid
- speed up the wear of the system
- impact on the behaviour and the reliability of the system

Impurity sources

- -initial impurities of the system
- impurities of the environment
- impurities originating from the system itself



Impurity types

- solid particles
- liquids (either dissolved in base fluid or as separate agent)
- gases (either dissolved in base fluid or as separate agent)

- * 50 55% of malfunctions are due to solid impurities
- * 20 25% of malfunctions are due to water and air



Solid impurities

Effects on the system depends on

- material
- hardness
- size
- shape
- quantity

Effects

- sudden damages or malfunctions (large particles)
- slow wear (size of particles $\sim \leq$ clearance size)



Liquid impurities

Most noteworthy of these is water

- ill effects are minor if water is dissolved in to base fluid
- when not dissolved, water has significant ill effects
 - reacts with base fluid
 - wear of the system speeds up (reduced lubricity)
 - danger of corrosion and rust



Gaseous impurities

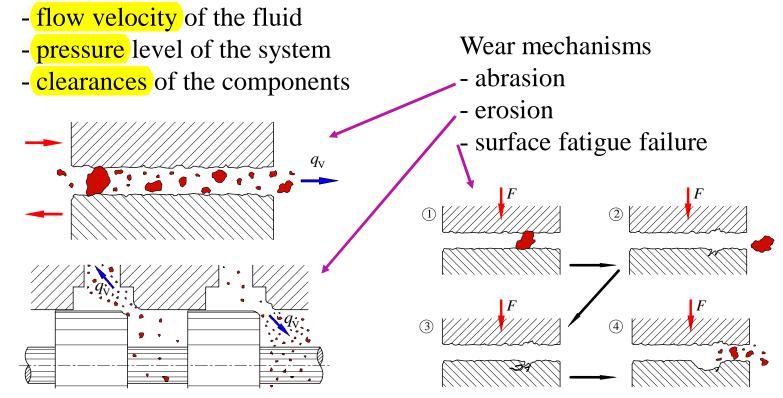
Most noteworthy of these is air

- ill effects are minor if air is dissolved in to base fluid
- when not dissolved, air has significant ill effects
 - reacts with base fluid (oxidation, ageing)
 - compressibility of the fluid increases
 - danger of cavitation



Wear caused by solid impurities

System parameters contributing to the ill effects of solid impurities





Wear is caused by particles with sizes of approximately the same magnitude as, or smaller than, the clearances. Lager particles cause jamming (of, e.g., spools) or blocking (of small flow channels).

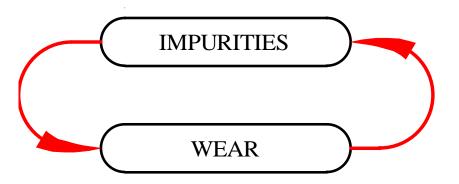
Harmful particle sizes

Component/gap	Clearance [mn]
Gear pump/motor	
tip of tooth – chamber wall	0,5-5
end of gear – side plate	0,5-5
Vane pump/motor	
tip of vane – chamber wall	0,5-5
side of vane – side plate	5- 25
Piston pump/motor	
piston – cylinder wall	5-40
valve plate – cylinder block	0,5- 10
Spool valve	
spool – valve housing	5- 25
Servo valve	
spool – valve housing	2-8
nozzle – flapper	20-70
nozzle (diameter)	100-400
Hydrostatic bearing	1- 30



Effects of wear

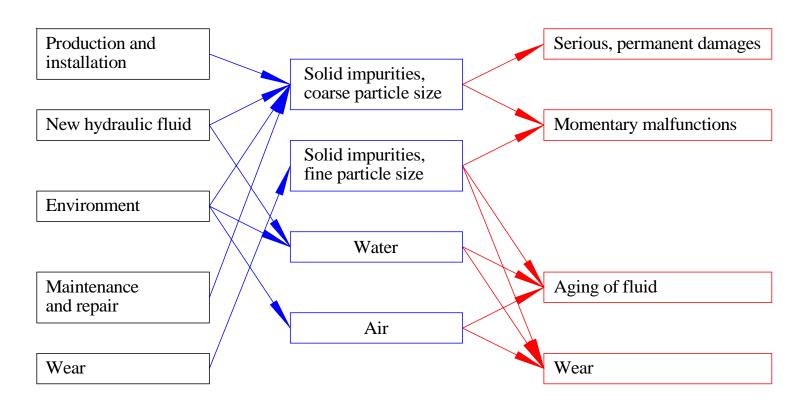
- → increase of clearance sizes
 - → increase of friction, leak and power loss in components
- → increase of quantity of impurities
 - → wear speed increases





Summary

Sources, types and effects of impurities





Ok, so what amounts and sizes of solid impurities (particles) can be allowed?

Before giving recommendations, we need a standardized way to express this => the cleanliness class

Cleanliness class

Denotes quantity and size distribution of solid impurities. Describes

- what is allowed for a component or a system, or
- what has been measured from the system (by sampling the fluid)

Standards

- ISO 4406
- SAE AS 4059 (Society of Automotive Engineers, Aerospace Standard)
- NAS 1638 (National Aerospace Standard)





Cleanlineag	Maximum Contamination Count (particles / 100 ml)					
Cleanliness class	5- 15	15- 25	25-50	50-100	>100	
Class	m m	mm	m m	mn	m m	
00	125	22	4	1	0	
0	250	44	8	2	0	
1	500	89	16	3	1	
2	1000	178	32	6	1	
3	2000	356	63	11	2	
4	4000	712	126	22	4	
5	8000	1425	253	45	8	
6	16 000	2850	506	90	16	
7	32 000	5700	1012	180	32	
8	64 000	11 400	2025	360	64	
9	128 000	22 800	4050	720	128	
10	256 000	45 600	8100	1440	256	
11	512 000	91 200	16 200	2880	512	
12	1 024 000	182 400	32 400	5760	1024	

Determination in five size classes, but system class number is determinated according to the class giving poorest result (usually the class 5–15 mm)

The result for all five size classes is lumped into one cleanliness number. (compare to ISO 4406 => one cleanliness number for each size class (of which there are three), p. 19.



Compare to ISO 4406

SAE AS 4059

Count type	Particle size [mm]						
I	> 1	> 5	> 15	> 25	> 50	> 100	
II	> 4	> 6	> 14	> 21	> 38	> 70	
Cleanliness	Size code and maximum contamination count (particles / 100 ml)						
class	A	В	С	D	Е	F	
000	195	76	14	3	1	0	
00	390	152	27	5	1	0	
0	780	304	54	10	2	0	
1	1560	609	109	20	4	1	
2	3120	1217	217	39	7	1	
3	6250	2432	432	76	13	2	
4	$1,25 \times 10^4$	4864	864	152	26	4	
5	$2,50>10^4$	9731	1731	306	53	8	
6	5,00×10 ⁴	1,95×10 ⁴	3462	612	106	16	
7	$10,0>10^4$	$3,89>10^4$	6924	1224	212	32	
8	$20,0>10^4$	$7,79>10^4$	$1,39>10^4$	2449	424	64	
9	40.0×10^{4}	15,6×10 ⁴	$2,77 \times 10^4$	4898	848	128	
10	$80,0>10^4$	$31,1>10^4$	$5,54>10^4$	9796	1696	256	
11	$1,60>10^6$	62,3>10 ⁴	$11,1>10^4$	1,96>104	3392	512	
12	3,20×10 ⁶	1,25×10 ⁶	22,2×10 ⁴	3,92×10 ⁴	6784	1024	

Determination in one or more size classes (the particle sizes vary according to measuring equipment and the standard used in calibration of the equipment)

Several ways to report the result, e.g.

6B (one particle size class)
7B/6C/5D (three size classes)

Replaces the outdated NAS 1638



SAE AS 4059

Counting the number of particles, two main methods

Type I: Calculation either by

- automatic particle counter (calibrated along ISO 4402)
- microscope (particle size is determinated as the maximum measure of the particle)

Type II: Calculation either by

- automatic particle counter (calibrated along ISO 11171)
- -electron microscope

 (particle size is determinated as the diameter of a circle whose area corresponds to the plane projected area of the particle)



Cleanliness class		amination count es / 1 ml)				
	Lower limit	Upper limit	=2 x lower limit	ISO 4406		
< 1	0,00	0,01		130 4400		
1	0,01	0,02				
2	0,02	0,04				•
3	0,04	0,08		Determination by auto	omatic partic	cle counter electrical counter e
4	0,08	0,16			P	
5	0,16	0,32	-	(three size classes)		
6	0,32	0,64		(unico sizo ciasses)		
8	0,64 1,3	1,3 2,5		> 4 m m		
9	2,5	5				
10	5	10		> 6 m m		Each size class gets its own
11	10	20	=	<u> </u>		
12	20	40		> 14 m m		cleanliness class number.
13	40	80		<u>~ 17 11111</u>		
14	80	160		→ three part class cod	10 0 0 21/2	1/15
15	160	320	-	- unce part class coe	10, 0.g., 24/2	11/13
16	320	640				
17	640	1300				
18	1300	2500		Determination by mic	roscone	
19 20	2500 5000	5000 10^4		Determination by mic	roscope	
21	10 ⁴	2×10 ⁴	=	(two size classes)		
22	2×10 ⁴	4×10 ⁴		(two size classes)		
23	4×10 ⁴	8×10 ⁴		> 5 m m		
24	8>10 ⁴	1,6>105		<u> </u>		
25	1,6>10 ⁵	3,2>10 ⁵		> 15 m m		
26	3,2>105	6,4>105		∠ 13 IIIII		
27	6,4>105	1,3>106		thron port along and	$\frac{1}{2}$	/15
28	1,3>106	2,5>106		→ three part class coo	ıe, e.g., <mark>-/</mark> ∠1.	/ 1 <i>J</i>
> 28	2,5>106			_	humb	on -> counted 'by microscope'
					nypn	en => counted 'by microscope'



Examples of cleanliness recommendations/requirements

Cleanliness class requirements of components

Component	Recommendation for Cleanliness class		anliness class	for pressure level 160 - 200 bar
	ISO 4406	NAS 1638	SAE AS 4059*	* Calculation either by
Directional control valve	21/18/15	10	11A/9B/9C	- automatic particle
Flow valve	21/18/15	10	11A/9B/9C	- automatic particle
Pressure valve, controlling	21/18/15	10	11A/9B/9C	counter
Cylinder	21/18/15	10	11A/9B/9C	(calibr. ISO 11171)
Gear pump / motor	21/18/15	10	11A/9B/9C	,
Piston pump / motor	20/18/15	9	10A/9B/9C	 electron microscope
Vane pump / motor	20/17/14	9	10A/8B/8C	
Proportional valve	20/16/13	9	10A/7B/7C	
Servoproportional valve	18/16/13	8	8A/7B/7C	
Servo valve	17/14/11	7	7A/5B/5C	Check with component manufacturers
Servo cylinder	17/14/11	7	7A/5B/5C	for actual values!

Sensitive components (small clearances) require cleaner fluid



Effect of system pressure level on the required cleanliness class (in relation to the table on previous slide)

Level of operating pressure	Change in Cleanliness class
0- 100 bar	3 classes weaker
100- 160 bar	1 class weaker
160-210 bar	No change
210- 250 bar	1 class stronger
250- 315 bar	2 classes stronger
315-420 bar	3 classes stronger
420- 500 bar	4 classes stronger
500- 630 bar	5 classes stronger



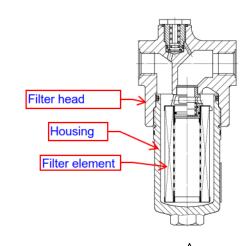
Cleanliness class requirements of systems

System type	Recommendation for Cleanliness class				
	ISO 4406	NAS 1638	SAE AS 4059*		
Low pressure systems with conventional valves	24/17/14	9® 11	-/8B/7C		
High pressure systems with conventional valves	21/16/13	7® 9	11A/11B/7C		
Proportional valve systems	20/15/12	6® 7	10A/6B/6C		
Servoproportional valve systems	18/14/11	5® 6	8A/5B/5C		
Servo valve systems	18/13/10	4® 5	8A/4B/4C		
Highly sensitive high power systems	16/11/9	3® 4	6A/2B/3C		

- * Calculation either by
 - automatic particle counter (calibr. ISO 11171)
 - electron microscope

Realizing a certain cleanliness class requires filtration on a certain level





Filter

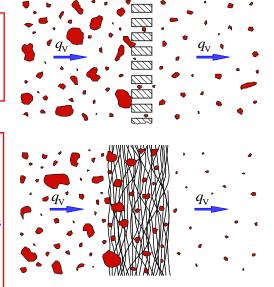
Operating principles of filter elements

Surface filtering

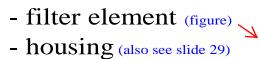
- Thin sheets (folded)
- Celulose or wowen fibers (plastic or steel)
- 'Constant' pore size

Depth filtering

- Thick fiber mat or compacted/sintered metal granulates
- Cellulose, glass fibres, metal fibres or granulates
- Passages of non-constant size
- Clogging takes longer than with surface filters



Parts



- accessories

Protection mesh

Protection fabric

Fiberglass fabric

i.e. actual filter material

Protection mesh

Support mesh

Perforated support tube



How to characterize the performance of the filter

=> 50 % of particles > size x are removed $\beta_x = 20 = 95 \%$ of particles > size x are removed $\beta_x = 75 = 98.6 \%$ of particles > size x are removed $\beta_x = 100 = 99 \%$ of particles > size x are removed

Expressing filtration efficiency

"Filtration grade"

b-ratio ("filtration ratio" or "degree of separation")

- number of particles (before filter N_1 / after filter N_2)
- $b_{x} = \frac{N_{1}}{N_{2}}$ - ISO 4572 (Multi-pass-test)
- x denotes the size (equal or larger) of calculated particles

Absolute filtration grade

- largest spherical particle (mm) that passes the filter
- removes 99 % of the particles greater than the announced size, $b_x \le 100$

Nominal filtration grade

- removes 95 % of the particles greater than the announced size, $b_x \le 20$
- note: determination **not standardized** (depends on filter manufacturer)



Expressing filtration efficiency

Filtration efficiency S_x of filter for certain particle size

$$S_{x} = \overset{\text{eff}}{\underset{\text{eff}}{\text{eff}}} - \frac{1}{b_{x}} \overset{\ddot{o}}{\underset{\text{o}}{\text{o}}} \times 100\%$$

How great a percentage of size *x* particles that the filter will remove

in theory, but

Just a β value isn't enough - the size x matters: $\beta_5 > 75$ (removes 98.7 % of particles $> 5 \mu$ m) is better than $\beta_{10} > 75$.

Filtration rating x refers to the size of particles which the filter is able to remove from the fluid, but it does not absolutely describe the efficiency of the filter, since it is also affected by other factors. \leq

See slide 27



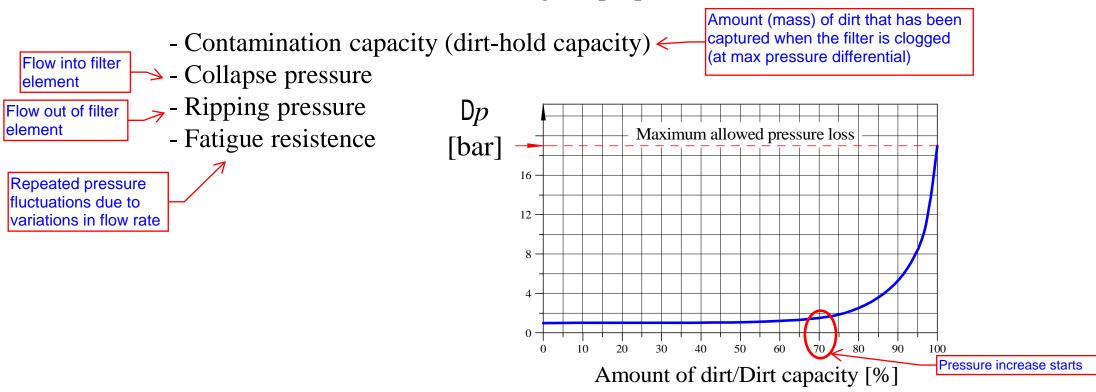
Cleanliness class and filtration rating

Example of effect of filtration rating *x* on achievable cleanliness class

μm Typical ISO 4406 Cleanliness classes achievable with different filtration ratings (class depends also on the conditions of system and environment) 19/16/13 - 22/19/1625 18/15/12 - 21/18/1520 Filtration rating x $\beta_{\rm x} \ge 200$ 15 17/14/11 - 20/17/1499.5 % 15/12/9 – 19/16/13 10 12/9/6 - 17/14/113 10/7/4 - 13/10/7

Aalto University
School of Engineering
Mechanical Engineering / Engineering Design / Fluid Power

Other factors describing the properties of filters





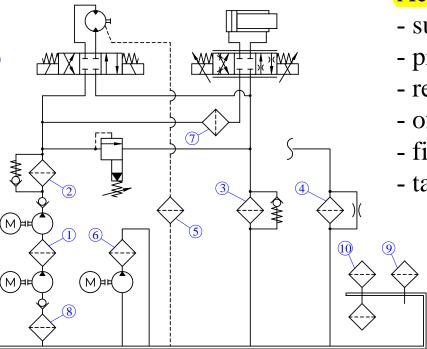
Classification of filters in system

According to the task

- work filters

(1-6; maintain cleanliness level)

- protective filters (7-10)



According to the location

- suction filters (8; beware of cavitation)
- pressure filters (eg, 2: before PRV)
- return line filters (3, 4.5)
- offline filters (6)
- filling filter (10)
- tank breather filter (9)
 - The filling&breather filter 10 is usually only a coarse mesh
 - Better to fill the tank through a separate filter corresponding to the required cleanliness level
 - Or use the system's own return filter
 - If large flow rate variations in the return line => use variant 4 as cheaper solution (don't have to dimension for highest possible return flow, as for 3)

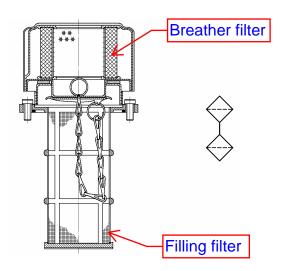


Filter types

When the filter gets clogged, the by-pass valve protects the filter element from getting damaged by the pressure differen-

Pressure filter Clogging indicator By-pass valve Housing Filter element

Filling filter and tank breather filter



tial and re-releasing the dirt into the system.

(At start-up, there will also be an increased pressure differential because of higher viscosity.)

Filtration system

Filtration system

- consists of several filters (work filters and protective filters)

(Only one filter is usually not enough)

- prevents impurities from entering the system
- removes the impurities from the system
- → Maintains the required cleanliness level

The continuity of filtration effectivity and quality requires continuous maintenance of the filtration system.



Heat exchangers

Maintain/control the operating temperature of the fluid by

- cooling
- warming

In operating state of the system the viscosity of fluid should be in its optimum range (16–36 cSt) and decreasing under 10 cSt should be prevented (lubrication limit).

In starting state of the system the viscosity of the fluid should be lower than the highest value allowed to the system (defined by some component of the system, e.g., pump).



Cooler

Transfers heat embodied in the hydraulic fluid actively to coolant that is either

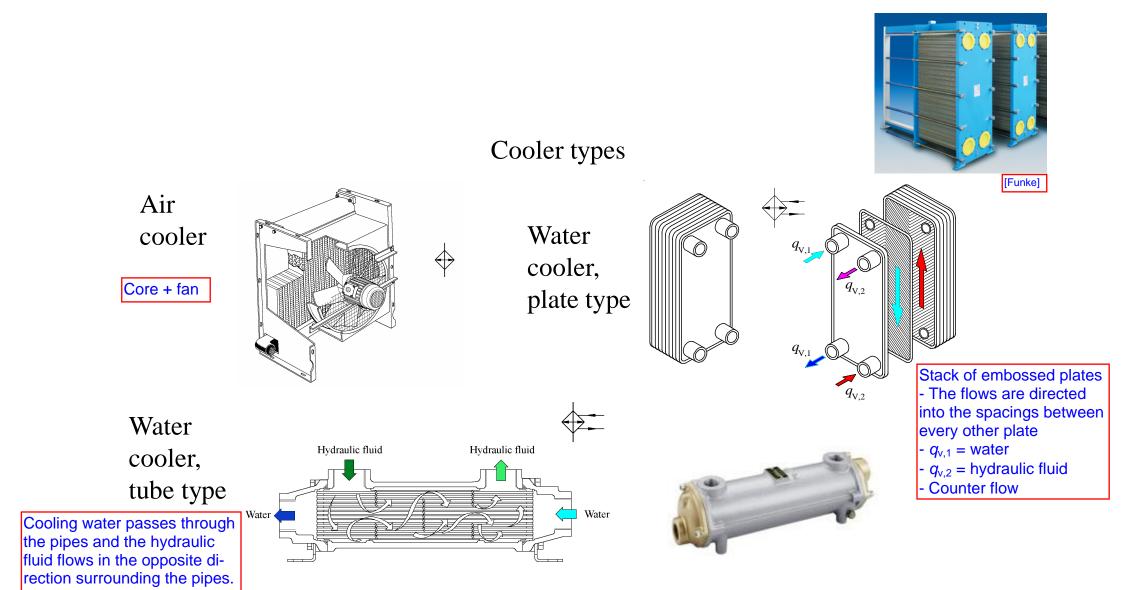
- air
- water

and thus away from the hydraulic fluid

The cooling efficiency depends on

- temperature difference between hydraulic fluid and coolant
- magnitude of coolant flow
- cooling area
- flow type (laminar or turbulent)

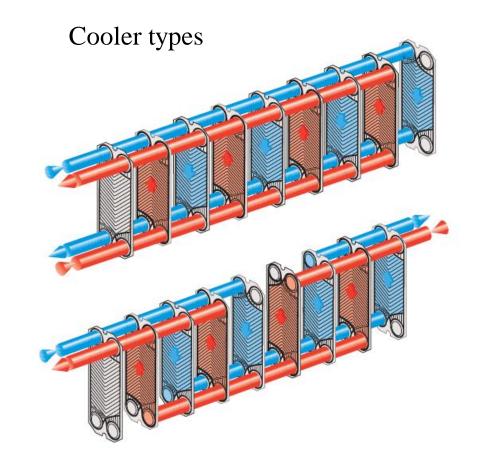






Water cooler, plate type

Arrangement of hydraulic fluid and coolant flow paths



'Single-pass flow'

This configuration is most commonly used. [Funke]

'Multi-pass flow' (≥ 2)

In cases where there are small temperature differences between process fluid and coolant. [Funke]



Coolers

Air cooler

- availability of coolant good
- heat transfer capacity poor in relation to size
- large imminent environmental load (air flow, heat and noise)
- best suitability in mobile hydraulic systems

(working environment and industrial environment)

Water cooler

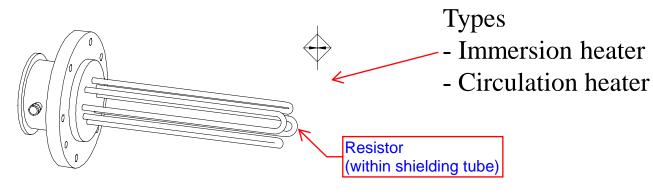
- availability and price of coolant
- heat transfer capacity good in relation to size
- minor imminent environmental load
- corrosion effect of water
- best suitability in fixed industrial hydraulic systems



Heaters

Warm hydraulic fluid either

- directly
- indirectly via transmitter fluid



Typical placement: horizontally in the tank

The heat is transferred to flowing fluid.

Heating power has to be restricted to avoid overheating and encrusting of

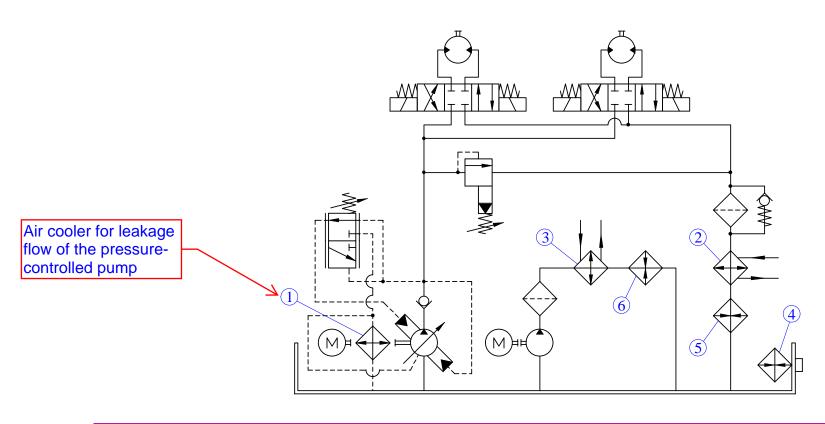
the hydraulic fluid.

E.g., 20 kW/m2 heating power for mineral oil if the oil flows, but this depends on the flow rate - in tanks, where the flow is slow, 7 kW/m2 can be appropriate.

(Carbon) deposits



Coolers and heaters in system



- Coolers (2; in return line) and (3; in separate filtering circuit).
- Heater (4; in tank) is of the immersion type.
- Heaters (5; in return line) and (6; in the filtering circuit) are circulation heaters.



EXTRA

Reservoir (= tank)

Tasks of reservoir

- fluid storage for the system
- buffer leveling the differences between suction and return flows
- heat exchanger
- -separator of the impurities of fluid
- installation base for system components



Size of reservoir

The fluid volume of reservoir is generally sized according to the average minute flow of the system pumps:

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- In fixed industrial systems V_{\text{reservoir}} = 2-5 \times q_{\text{V,pumps}}

- In mobile systems V_{\text{reservoir}} = 1-2 \times q_{\text{V,pumps}}
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"50 l/min => 100 ... 250 litres"

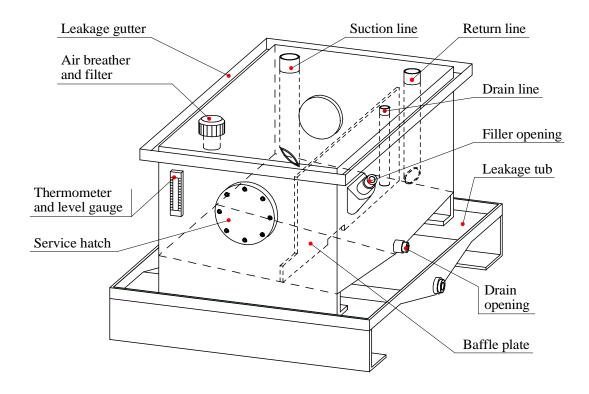
"50 l/min => 50 ... 100 litres"

In sizing of the reservoir also the following have to be considered

- momentary quantity changes of fluid in reservoir (buffer function)
- in case of system maintenance the fluid circulating in the system has to be fitted in the reservoir



Reservoir accessories



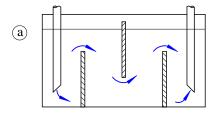


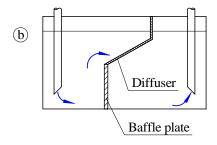
Slow down the flow in the tank in order to better remove heat as well as impurities and air.

Note also 45 degree cuts of pipes and a diffusor (on next slide) at end of the return pipe to increase the flow channel cross section and reduce the velocity of the flow.

Enhancing the functions of reservoir

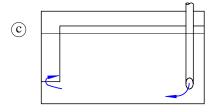
Enhancing heat exchange

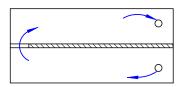


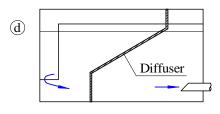


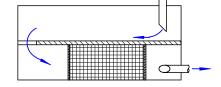
Diffuser mesh to enhance separation of air bubbles from oil

Enhancing impurities separation





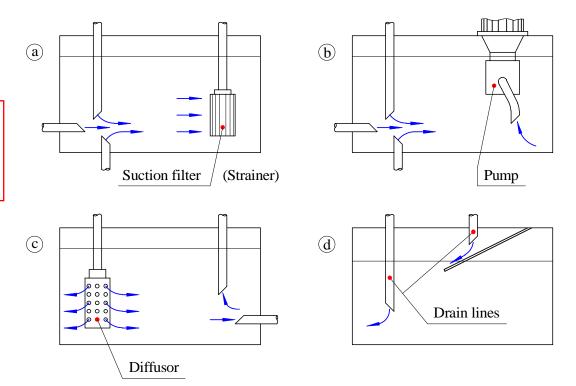






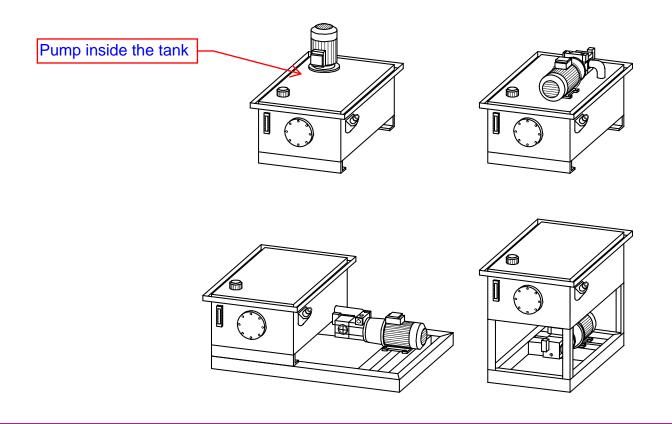
Positioning of flow channels in reservoir

The suction line should begin sufficiently below the surface, but also sufficiently above the bottom.



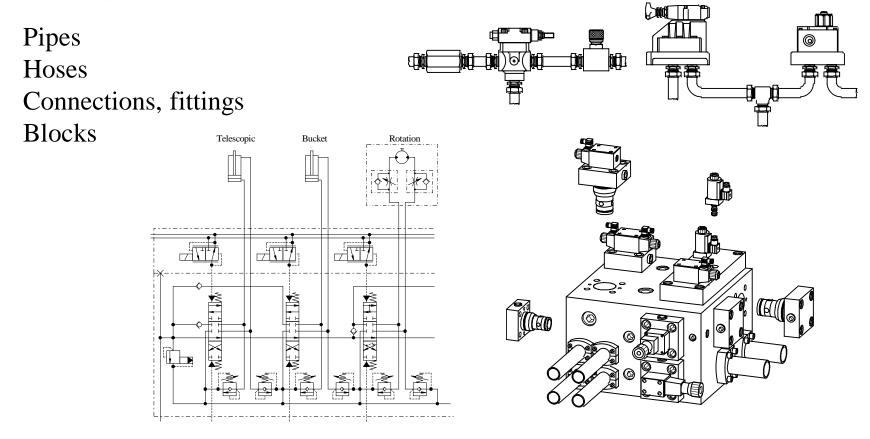


Positioning of pump in relation to reservoir





Piping components





Pipes

Rigid connection

Type, material and wall thickness of pipe are affected by system pressure, flow rate, fluid type and the connector/fitting types.

Flow channel	Recommended flow velocity v [m/s]	$\begin{array}{c} \textbf{Maximum} \\ \textbf{flow velocity } \nu_{max} \\ [m/s] \end{array}$	
Suction line	0,5-1,0	1,0-1,5	
Return line	2,0-3,0	3,0-4,0	
Pressure lines			
6,3-10 MPa	4,0-4,5	6,0	
10- 16 MPa	4,5-5,0	6,0	
16-25 MPa	5,0-5,5	6,0	
25-40 MPa	5,5-6,0	6,0	

Pipe's outer diameter	Pipe wall thickness [mm]				
d	Nominal pressure [MPa]				
[mm]	6,3	10	16	25	40
6	1	1	1	1	1,5
8	1	1	1	1,5	1,5
10	1	1	1	1,5	2
12	1	1	1,5	2	2,5
16	1,5	1,5	1,5	2	3
20	1,5	1,5	2	2,5	4
25	2	2	3	3	5
30	2	2	3	4	6
38	3	3	4	5	7
50	3	3	6	6	9

Dimensioning principle: System pressure losses should be ~ 3–10 % of the system pressure level.



Hoses

Flexible connection

Classification by the operational pressure level:

- low pressure hoses
- medium pressure hoses
- high pressure hoses
- ultra-high pressure hoses

Hoses increase the elasticity of the system!





Hoses

Most common standard SAE J517 (14 groups: SAE 100R1–14)

Size is expressed by a code number representing the inner diameter (with exceptions of SAE 100R5 and SAE 100R14, outer diameter)

The	code	number	is based	
on 1	16 th	n divisioi	n of incl	1

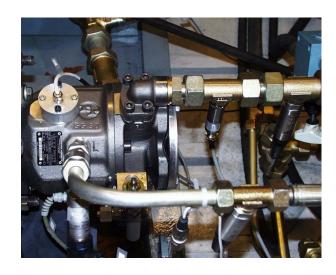
Size can also be expressed in DIN standard nominal size (= hose's inner diameter's rough value in full millimetres)

SAE	Inner dian	neter of hose	Nominal size	
size code	[<mark>in</mark>]	[mm]	NS	
-04	1/4	6,4	6	
-05	5/16	7,9	8	
-06	3/8	9,5	10	
-08	1/2	12,7	12	
-10	5/8	15,9	16	
-12	3/4	19,0	20	
-16	1	25,4	25	
-20	$1 \ 1/4$	31,8	32	
-24	1 1/2	38,1	40	
-32	2	50,8	50	

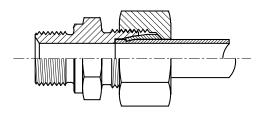


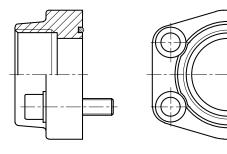
Connectors, Fittings

Connecting pipes and hoses to each other and components



Low pressure connectors High pressure connectors Threaded connectors
(BSP, BSPT, M, NPTF, UNF, etc.)

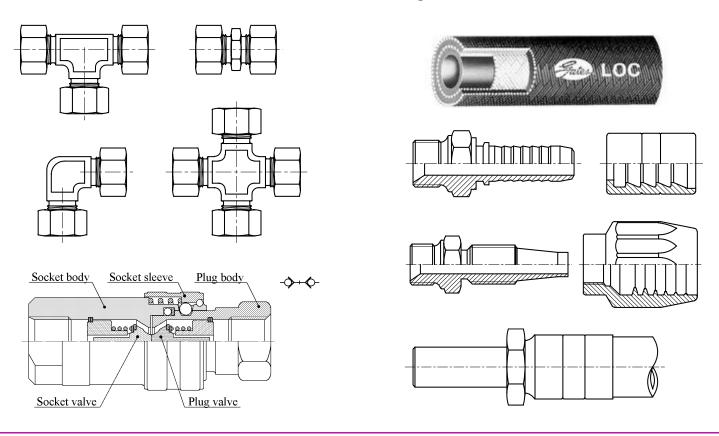




Flange connectors (SAE, DIN, CETOP)

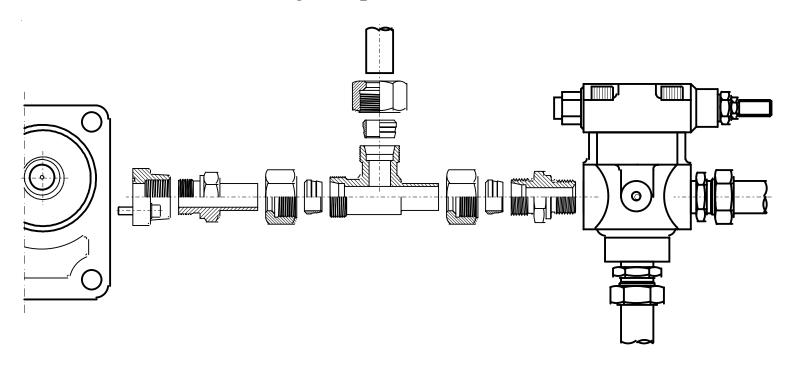


Connectors, Fittings





Connecting components to each other



Example case: connecting components with piping components



Lecture themes - Recap

Impurities in system

- effect?
- removal?

Temperature in system

- what kind of effect does it have on the system?
- how can it be kept in check?

Reservoir, what can it do for the system?

Piping, how about it?

