

ELEC-E4130

Lecture 13: Multilayer (Stratified Media) One layer, normal incidence

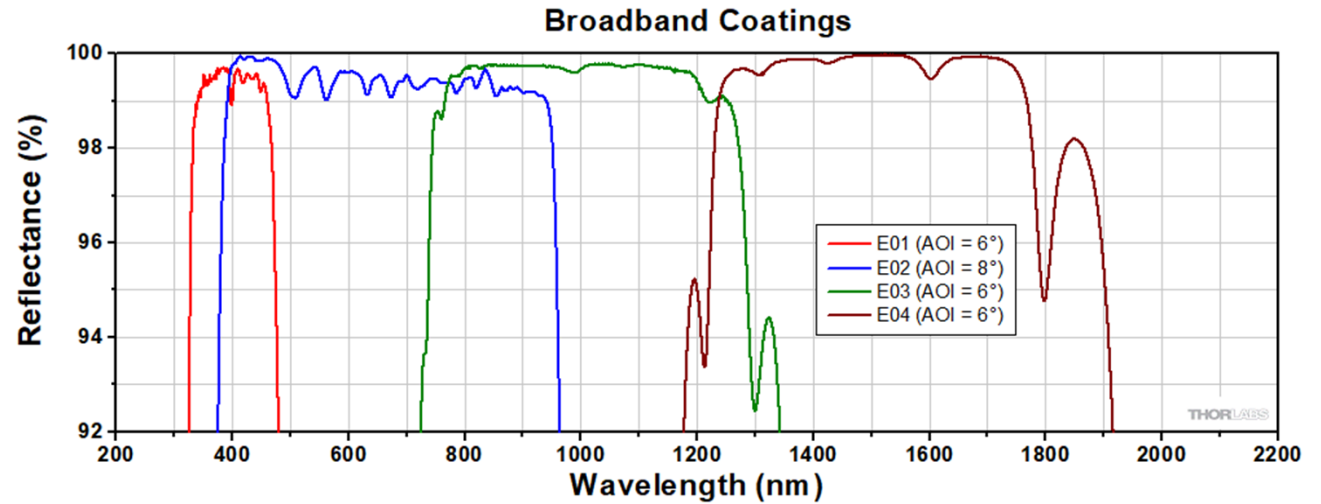
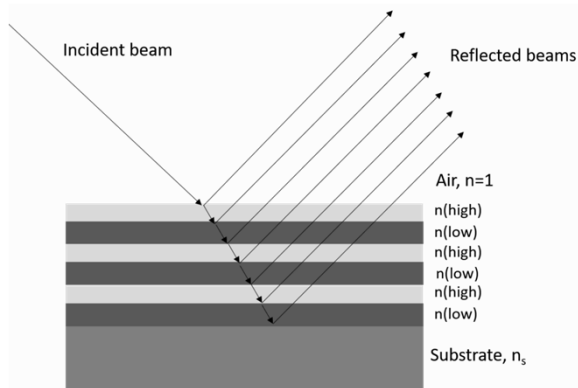


Aalto University
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ELEC-E4130 / Taylor

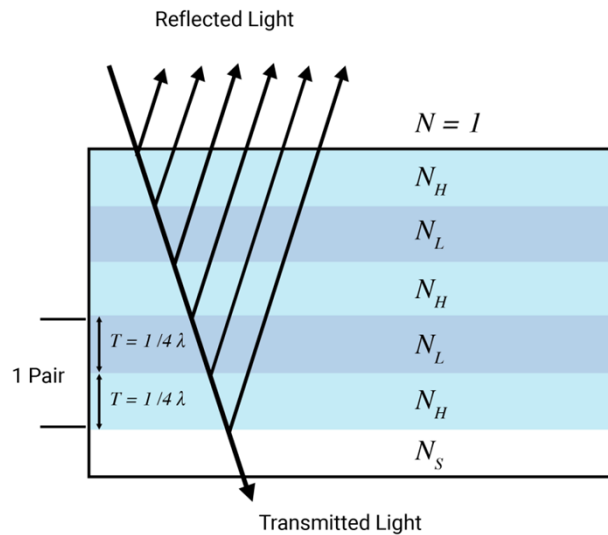
Nov. 01, 2021

Multiple layers mirrors

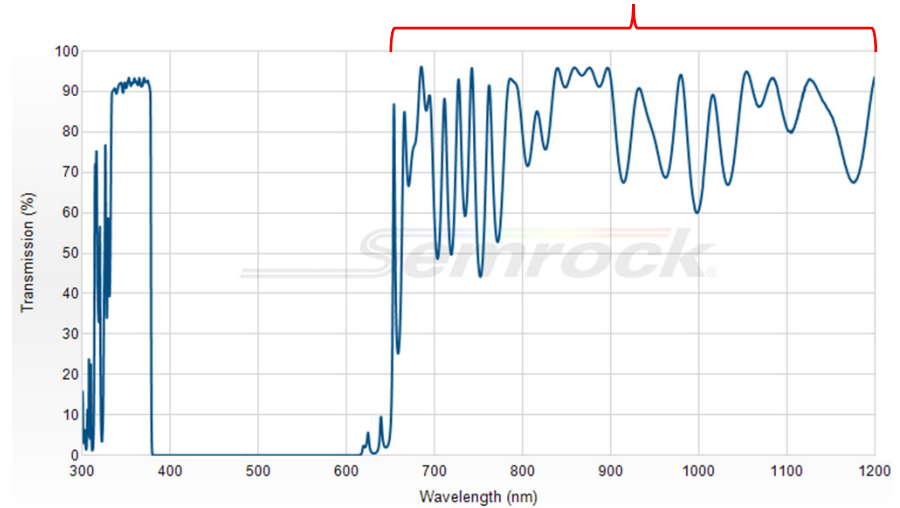


- Tune layer permittivity and thickness to enhance **constructive interference** of multiple reflections at the air dielectric interface
- Dielectric surface quality superior to metallic surface quality

Multiple layer filters

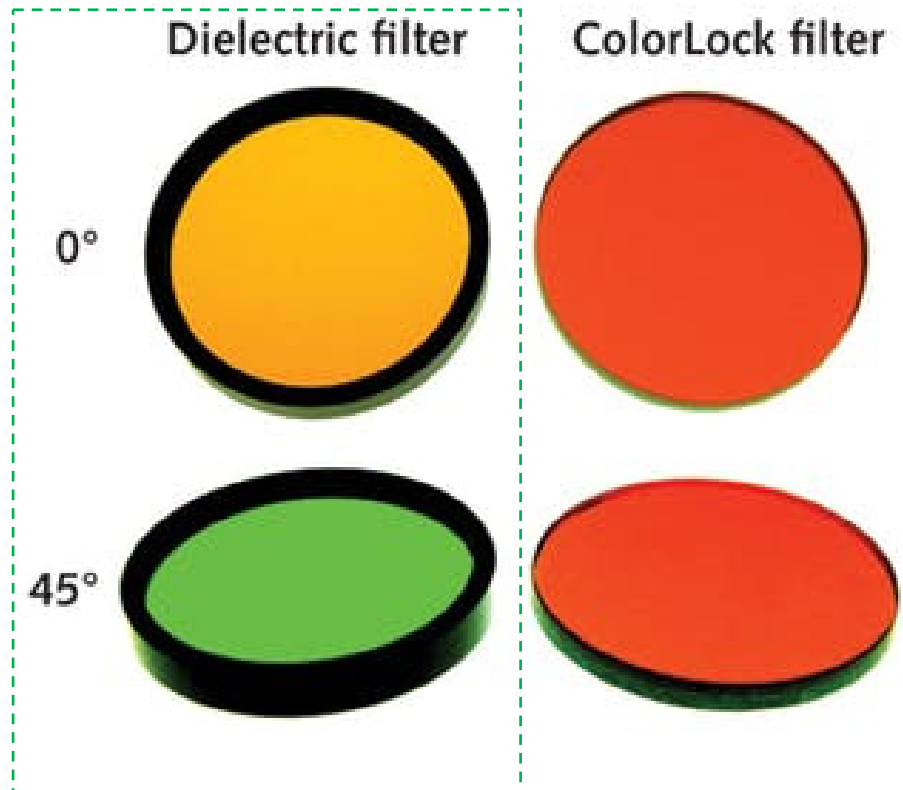


Sometimes impossible to suppress natural periodic behavior



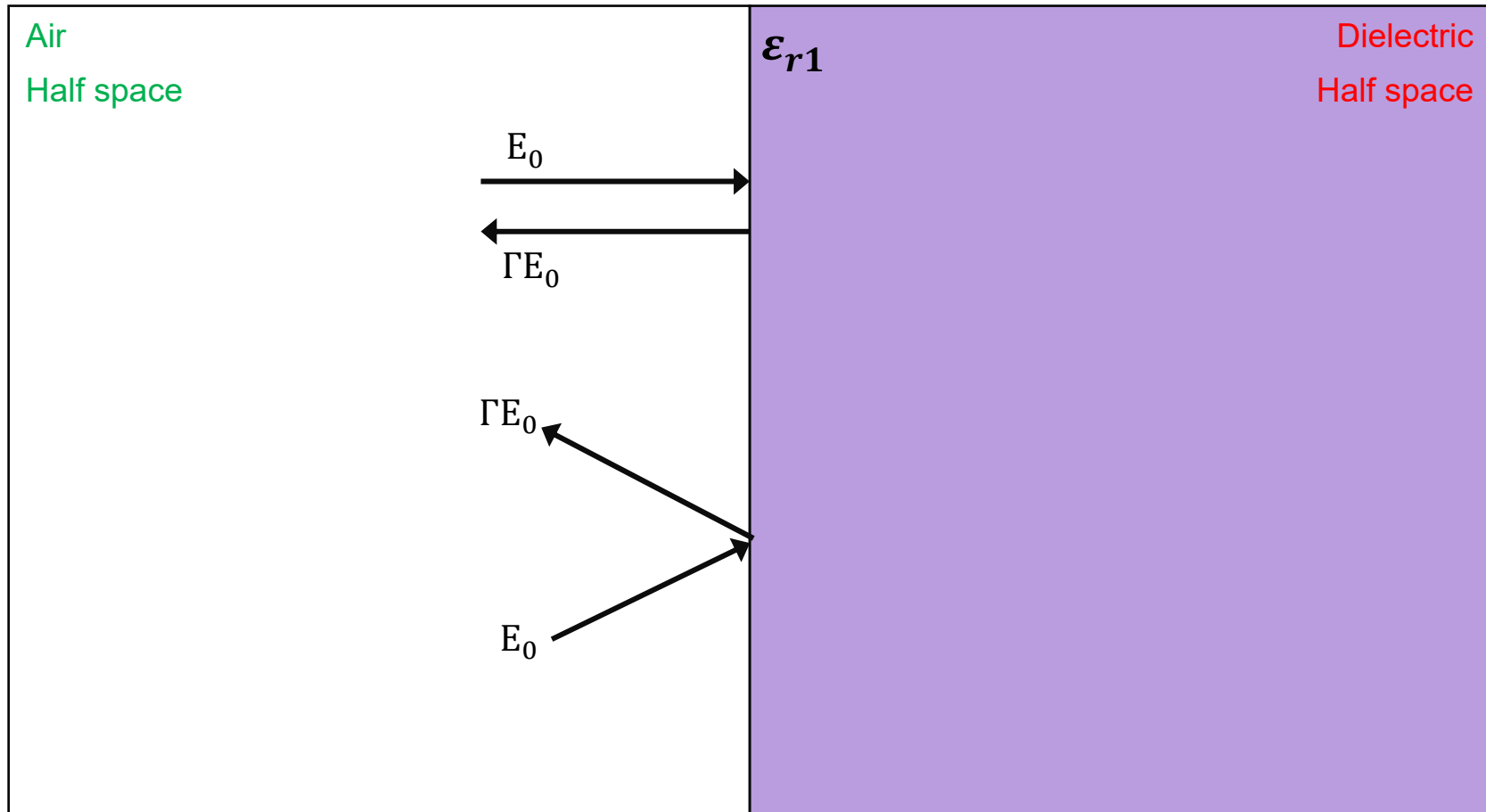
- Tune layer permittivity and thickness to enhance **destructive interference** of multiple reflections at input the air-dielectric interface
- This enhances **constructive interference** at the output dielectric-air interface

Angle dependent behavior

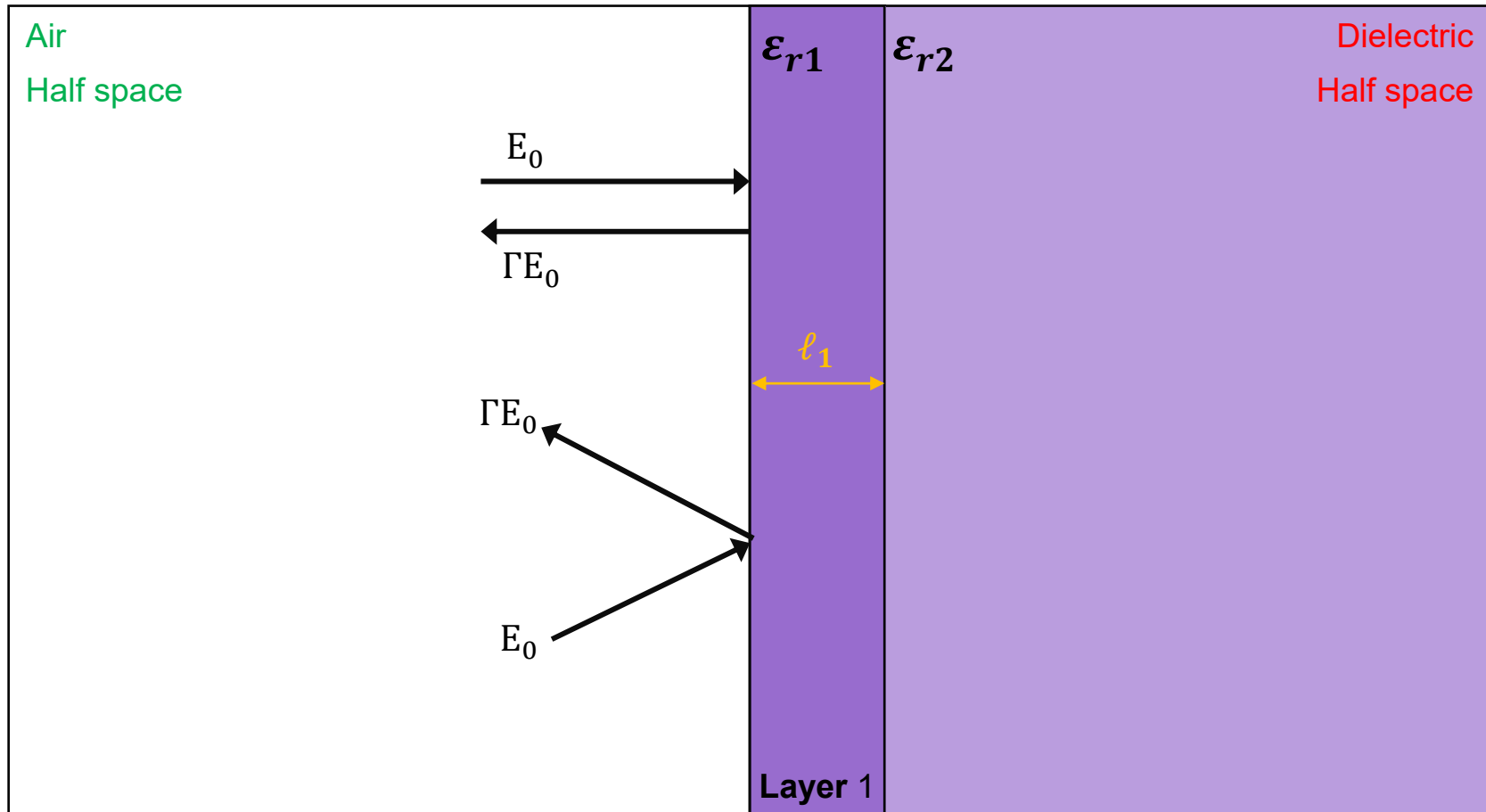


- Transmission and reflection are defined by steady state constructive and destructive interference
- Interference controlled by optical path length within the dielectric
- Optical path is increased going from normal to oblique incidence angle

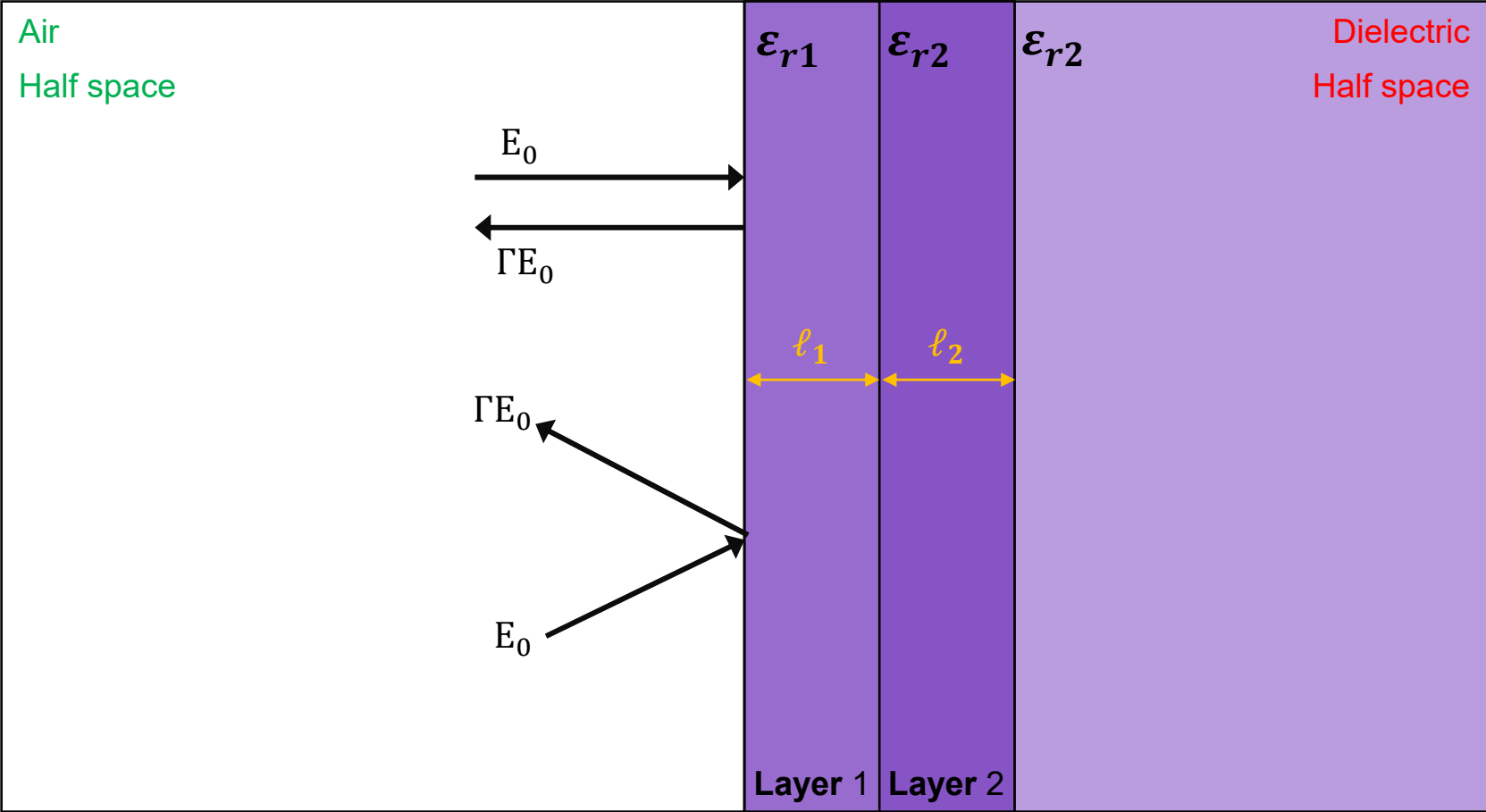
Single interface



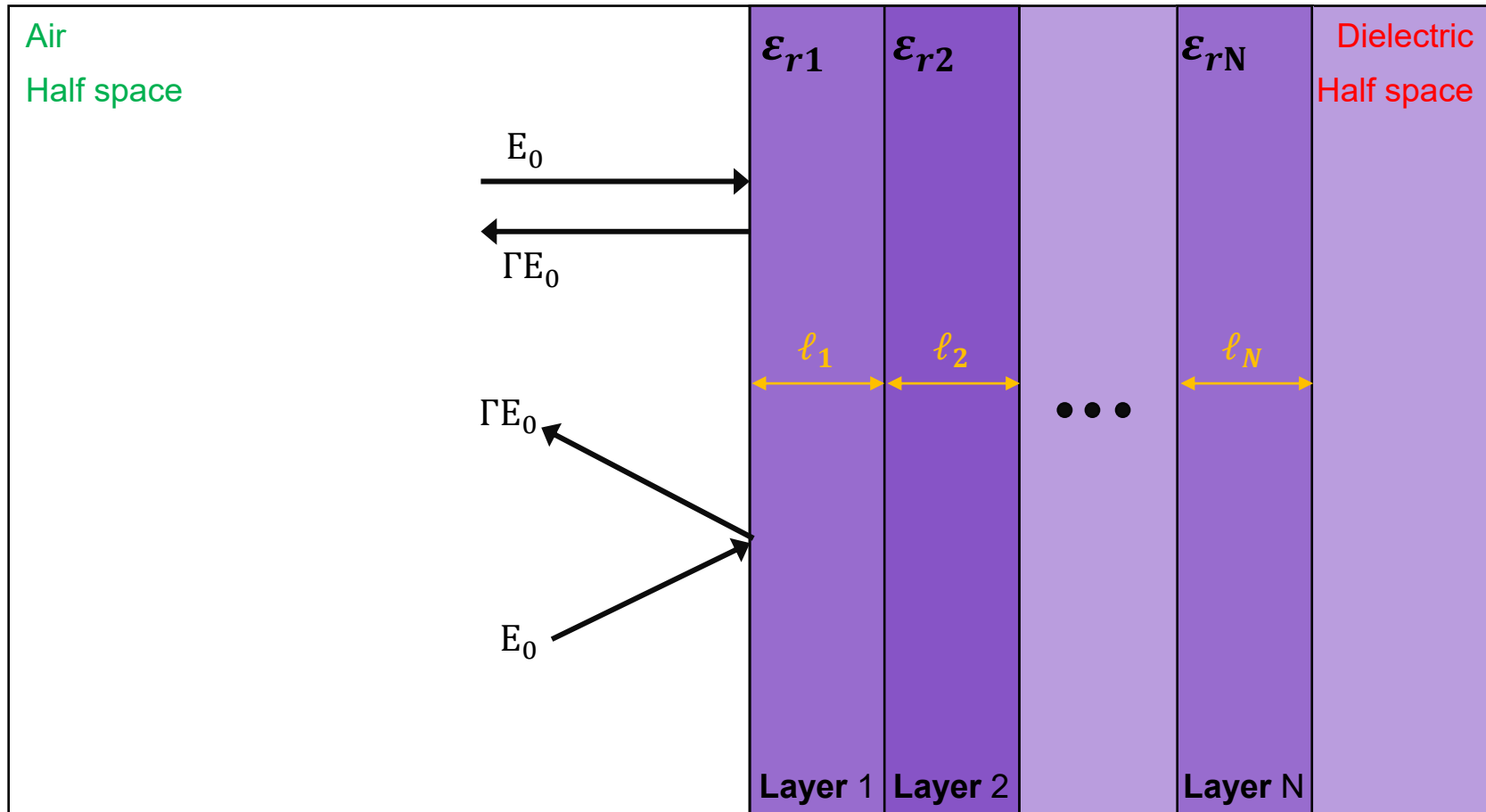
Finite thickness layer



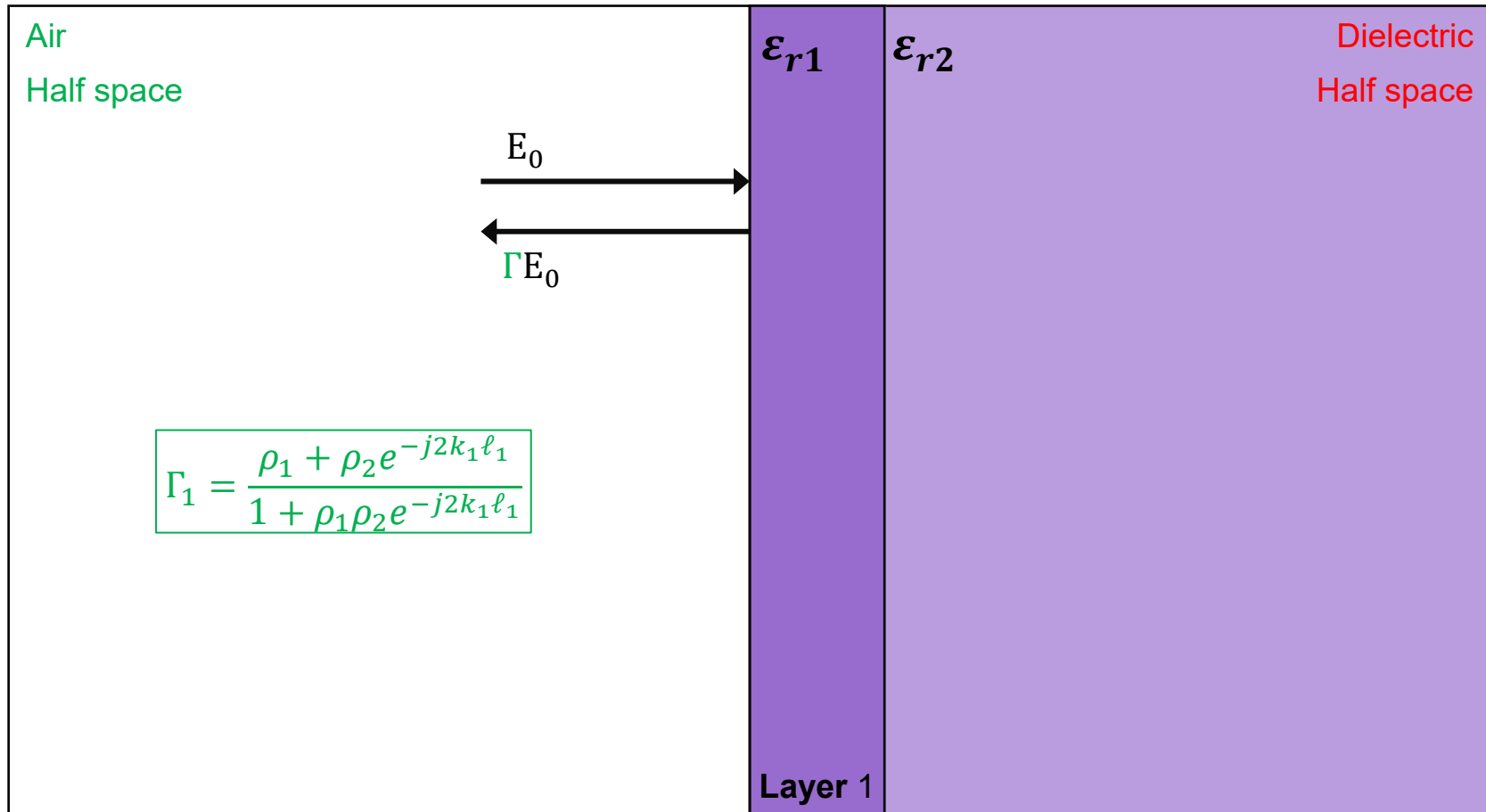
Two layers



N Layers



Today: Normal incidence, single layer



Field relations

Total E-field

$$E(z) = E_{0+}e^{-jkz} + E_{0-}e^{jkz} = E_+(z) + E_-(z)$$

Total H-field

$$H(z) = \frac{1}{\eta} [E_{0+}e^{-jkz} - E_{0-}e^{jkz}] = \frac{1}{\eta} [E_+(z) - E_-(z)]$$

Right hand rule

Algebra

Forward traveling E-field

$$E_+(z) = E_{0+}e^{-jkz}$$

Forward E-field
@ $z = 0$

$$E_{0+}$$

Reverse traveling E-field

$$E_-(z) = E_{0-}e^{jkz}$$

Reverse E-field
@ $z = 0$

$$E_{0-}$$

$$E_+(z) = \frac{1}{2} [E(z) + \eta H(z)]$$

Matrix vector
Multiplication

$$\begin{bmatrix} E(z) \\ H(z) \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ \eta^{-1} & -\eta^{-1} \end{bmatrix} \begin{bmatrix} E_+(z) \\ E_-(z) \end{bmatrix}$$

$$\begin{bmatrix} E \\ H \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ \eta^{-1} & -\eta^{-1} \end{bmatrix} \begin{bmatrix} E_+ \\ E_- \end{bmatrix}$$

$$E_-(z) = \frac{1}{2} [E(z) - \eta H(z)]$$

$$\begin{bmatrix} E_+(z) \\ E_-(z) \end{bmatrix} = \begin{bmatrix} 1 & \eta \\ 1 & -\eta \end{bmatrix} \begin{bmatrix} E(z) \\ H(z) \end{bmatrix}$$

Suppress
z-dep.

$$\begin{bmatrix} E_+ \\ E_- \end{bmatrix} = \begin{bmatrix} 1 & \eta \\ 1 & -\eta \end{bmatrix} \begin{bmatrix} E \\ H \end{bmatrix}$$

Wave impedance and reflection

z-dependent Wave impedance

$$Z(z) = \frac{E(z)}{H(z)} = \frac{E}{H} = \frac{E_+ + E_-}{\frac{1}{\eta} [E_+ - E_-]} = \eta \frac{1 + \frac{E_-}{E_+}}{1 - \frac{E_-}{E_+}} = \eta \frac{1 + \Gamma}{1 - \Gamma}$$

z-dependent Reflection coefficient

$$\Gamma(z) = \frac{E_-(z)}{E_+(z)} = \frac{E_-}{E_+} = \frac{\frac{1}{2} [E(z) + \eta H(z)]}{\frac{1}{2} [E(z) - \eta H(z)]} = \frac{\frac{E}{H} - \eta}{\frac{E}{H} + \eta} = \frac{Z - \eta}{Z + \eta}$$


Summarize

$$Z(z) = \eta \frac{1 + \Gamma(z)}{1 - \Gamma(z)}$$

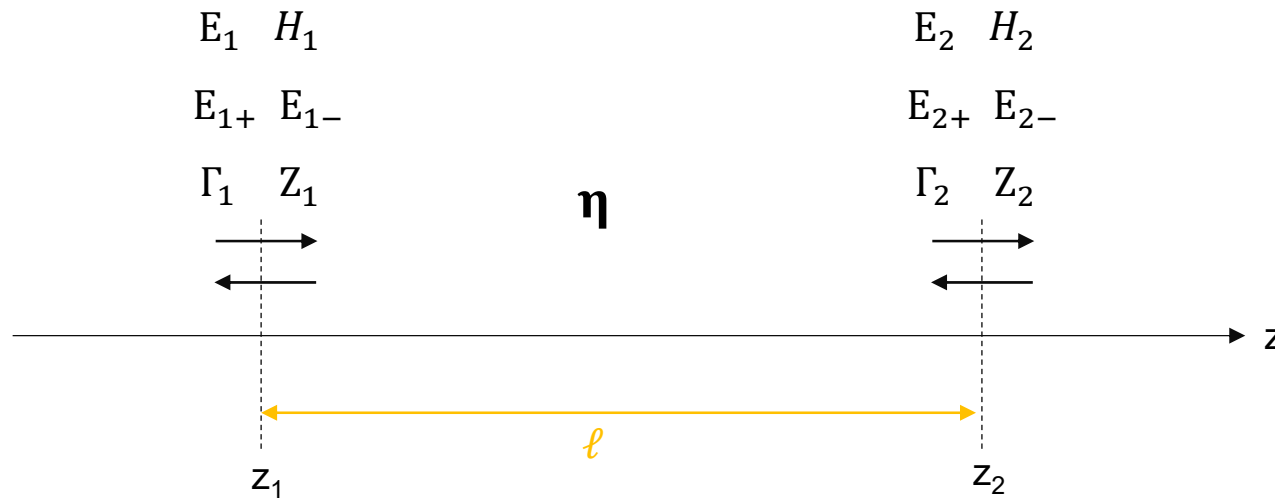
$$\Gamma(z) = \frac{Z(z) - \eta}{Z(z) + \eta}$$

Propagation of reflection coefficient

$$\Gamma(z) = \frac{E_-(z)}{E_+(z)} = \frac{E_{0+}e^{-jkz}}{E_{0-}e^{jkz}} = \frac{E_{0+}}{E_{0-}} e^{-j2kz} = \Gamma(0)e^{-j2kz}$$

- The reflection coefficient at any point along z is the reflection coefficient at $z = 0$ modified by twice the propagation phase kz
- Reflection coefficient magnitude is unchanged
- Only reflection coefficient phase is modified

Propagation matrices: two points on z-axis



“Reverse” propagation

$$E_{1+} = e^{jk\ell} E_{2+}$$

“Forward” propagation

$$E_{2+} = e^{-jk\ell} E_{1+}$$

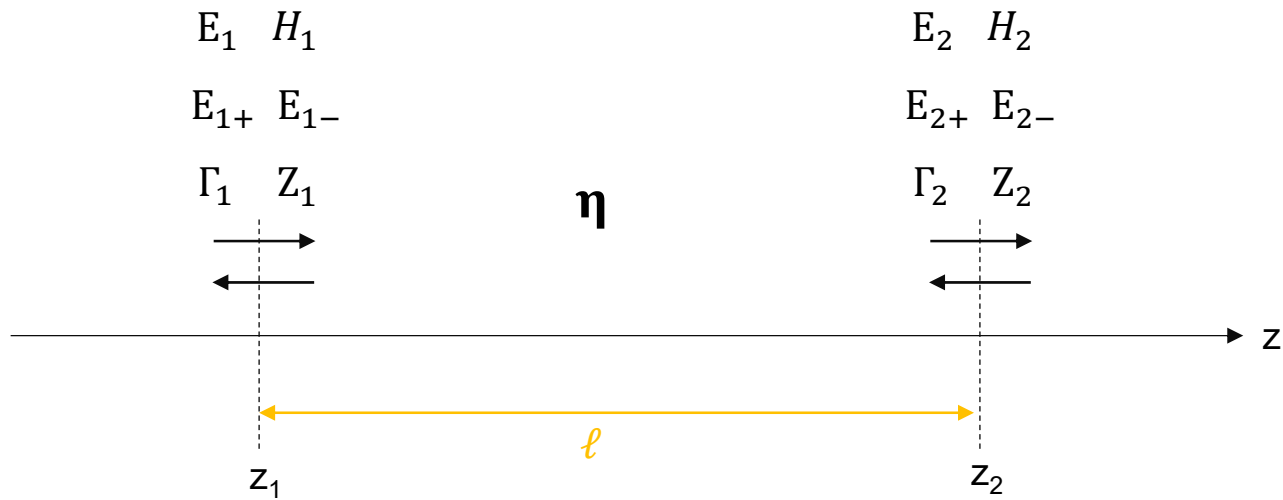
“Forward” propagation

$$E_{1-} = e^{-jk\ell} E_{2-}$$

“Reverse” propagation

$$E_{2-} = e^{jk\ell} E_{1-}$$

Propagation matrices: two points on z-axis

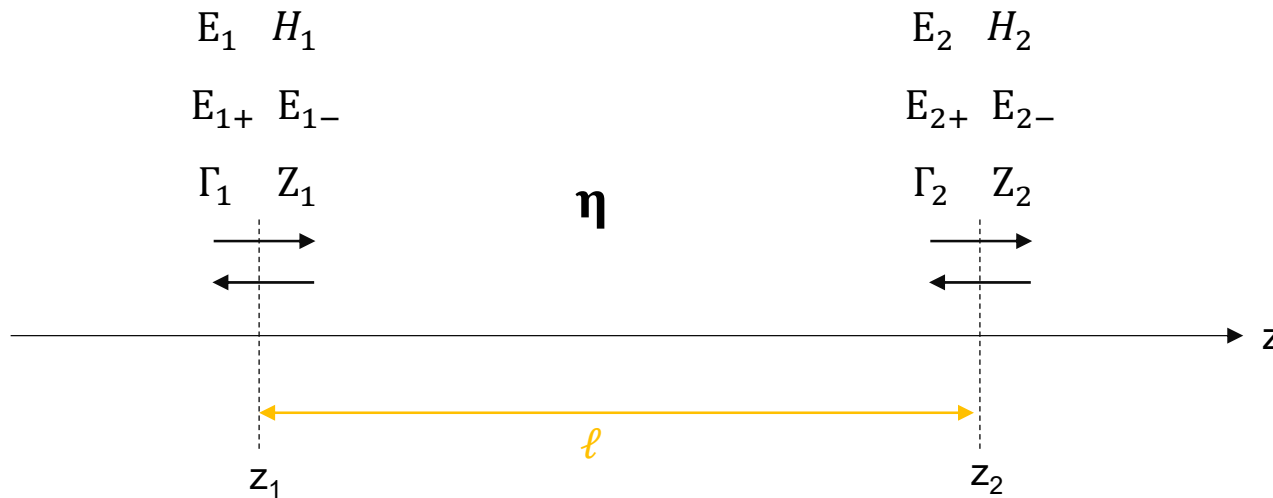


$$\begin{bmatrix} E_{1+} \\ E_{1-} \end{bmatrix} = \begin{bmatrix} e^{jk\ell} & 0 \\ 0 & e^{-jk\ell} \end{bmatrix} \begin{bmatrix} E_{2+} \\ E_{2-} \end{bmatrix}$$



$$\Gamma_1 = \frac{E_{1-}}{E_{1+}} = \frac{E_{2-} e^{-jkz}}{E_{2+} e^{jkz}} = \Gamma_2 e^{-j2kz}$$

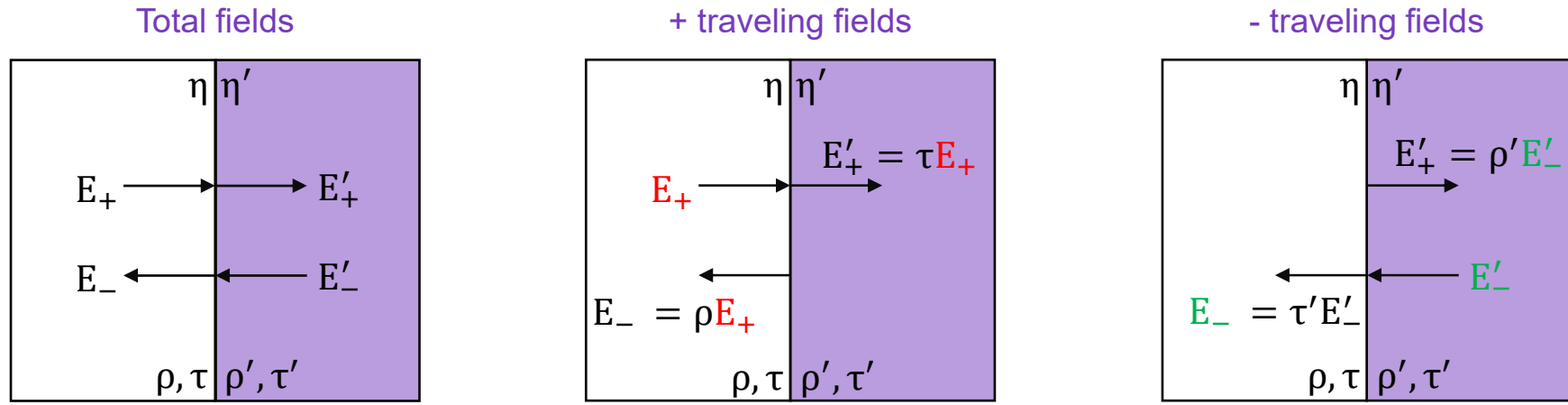
Propagation matrices: two points on z-axis



$$\begin{bmatrix} E_1 \\ H_1 \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ \eta^{-1} & -\eta^{-1} \end{bmatrix} \begin{bmatrix} E_{1+} \\ E_{1-} \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ \eta^{-1} & -\eta^{-1} \end{bmatrix} \begin{bmatrix} e^{jk\ell} & 0 \\ 0 & e^{-jk\ell} \end{bmatrix} \begin{bmatrix} E_{2+} \\ E_{2-} \end{bmatrix}$$

$$\begin{bmatrix} E_1 \\ H_1 \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ \eta^{-1} & -\eta^{-1} \end{bmatrix} \begin{bmatrix} e^{jk\ell} & 0 \\ 0 & e^{-jk\ell} \end{bmatrix} \begin{bmatrix} 1 & \eta \\ 1 & -\eta \end{bmatrix} \begin{bmatrix} E_2 \\ H_2 \end{bmatrix}$$

Matching matrices across interfaces



Total fields

$$E = E_+ + E_-$$

$$E' = E'_+ + E'_-$$

$$H = H_+ + H_-$$

$$H' = H'_+ + H'_-$$



Boundary
Conditions

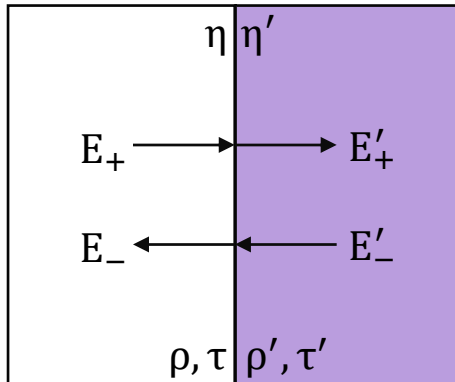
$$E = E'$$

$$H = H'$$

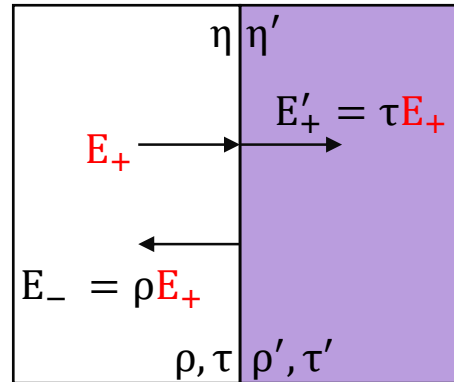
- Lossless dielectric
- No free charge
- TEM wave at normal incidence
 - All fields tangential
- Tangential field continuity

Matching matrices across interfaces

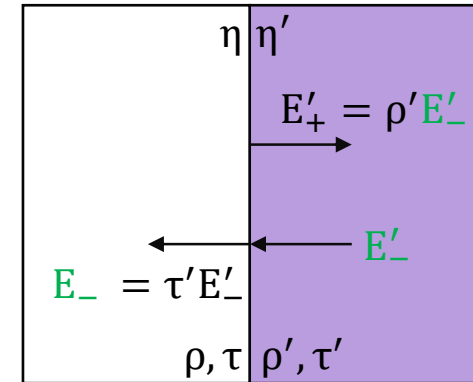
Total fields



+ traveling fields



- traveling fields



$$E_+ + E_- = E'_+ + E'_-$$

$$H_+ + H_- = H'_+ + H'_-$$



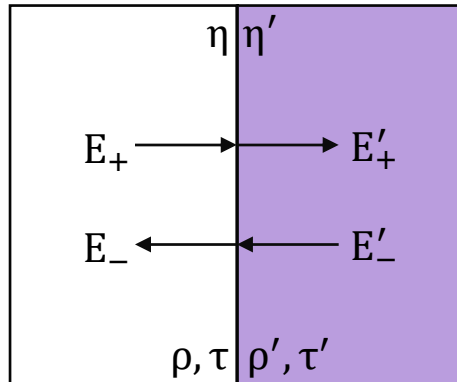
Boundary
Conditions

$$\begin{bmatrix} E_+ \\ E_- \end{bmatrix} = \frac{1}{\tau} \begin{bmatrix} 1 & \rho \\ \rho & 1 \end{bmatrix} \begin{bmatrix} E'_+ \\ E'_- \end{bmatrix}$$

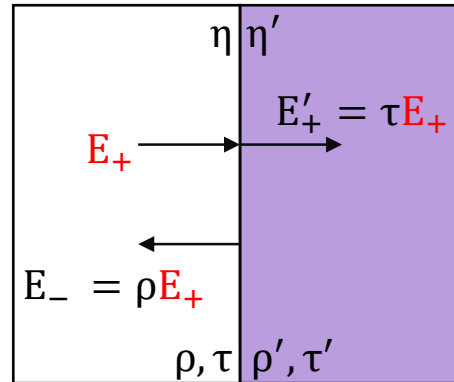
$$\begin{bmatrix} E'_+ \\ E'_- \end{bmatrix} = \frac{1}{\tau'} \begin{bmatrix} 1 & \rho' \\ \rho' & 1 \end{bmatrix} \begin{bmatrix} E_+ \\ E_- \end{bmatrix}$$

Matching matrices across interfaces

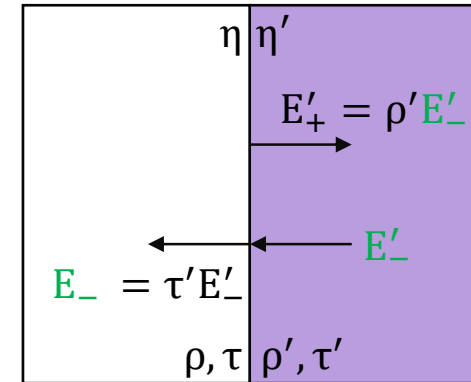
Total fields



+ traveling fields



- traveling fields



$\eta \rightarrow \eta'$

$$\rho = \frac{\eta' - \eta}{\eta' + \eta}$$

$$\tau = \frac{2\eta'}{\eta' + \eta}$$

$\eta' \rightarrow \eta$

$$\rho' = \frac{\eta - \eta'}{\eta + \eta'}$$

$$\tau' = \frac{2\eta}{\eta + \eta'}$$

Relations

$$\tau = 1 + \rho$$

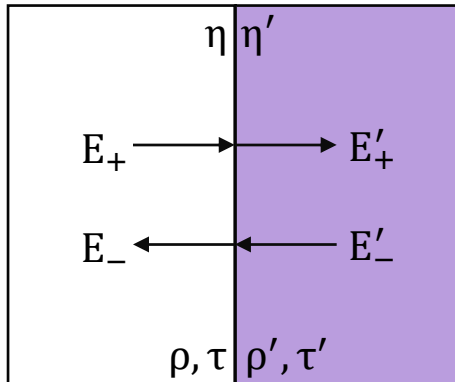
$$\rho = -\rho'$$

$$\tau' = 1 + \rho'$$

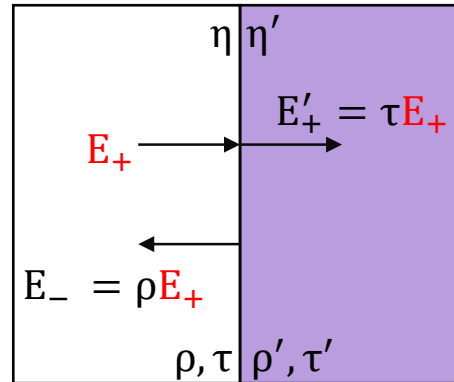
$$\tau\tau' = 1 - \rho^2$$

Matching matrices across interfaces

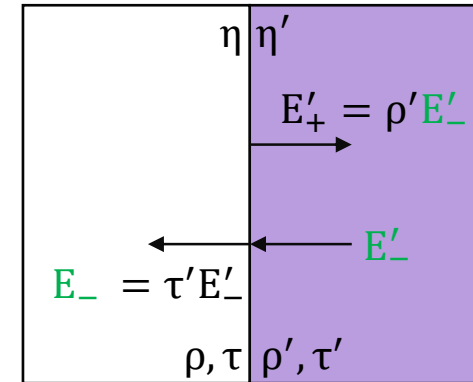
Total fields



+ traveling fields



- traveling fields



Impedance continuity

$$Z = \frac{E}{H} = \frac{E'}{H'} = Z'$$



Slide 12

$$\eta \frac{1 + \Gamma}{1 - \Gamma} = \eta' \frac{1 + \Gamma'}{1 - \Gamma'}$$



Algebra

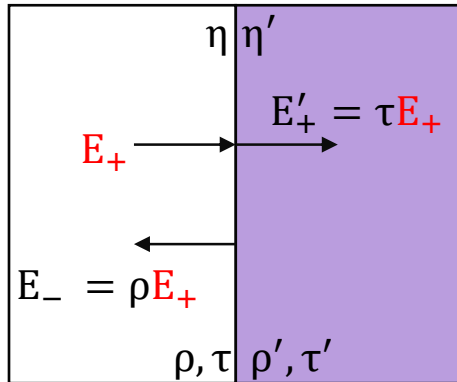


$$\Gamma = \frac{\rho + \Gamma'}{1 + \rho\Gamma'}$$

$$\Gamma' = \frac{\rho + \Gamma}{1 + \rho'\Gamma}$$

What if there only an incident field from left?

+ traveling fields



$$E'_- = 0$$

$$\Gamma' = \frac{E'_-}{E'_+} = 0$$

$$Z' = \eta' \frac{1 + 0}{1 - 0} = \eta'$$

$$Z = Z' = \eta'$$

$$\Gamma = \frac{\rho + 0}{1 + \rho \cdot 0} = \rho$$

Plug it in

$$\begin{bmatrix} E_+ \\ E_- \end{bmatrix} = \frac{1}{\tau} \begin{bmatrix} 1 & \rho \\ \rho & 1 \end{bmatrix} \begin{bmatrix} E'_+ \\ 0 \end{bmatrix}$$

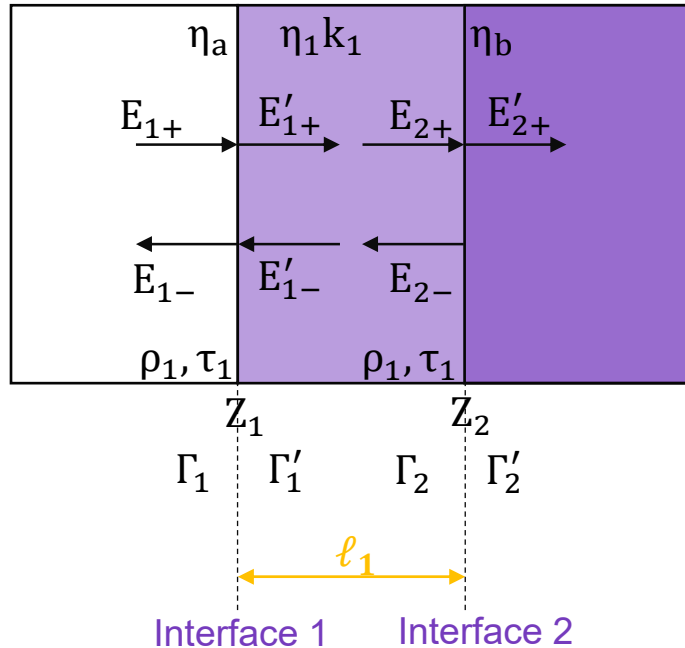
solve

$$E_- = \rho E_+$$

$$E'_+ = \tau E_+$$

- This is the final condition for the dielectric slab
- Once energy enters the half space it does not reflect back

Single Dielectric Slab

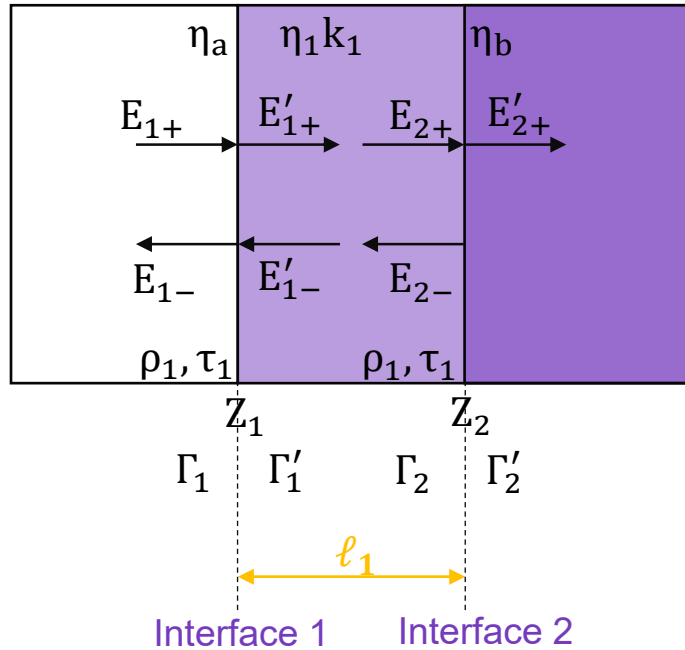


$$\rho_1 = \frac{\eta_1 - \eta_a}{\eta_1 + \eta_a} \quad \tau_1 = 1 + \rho_1$$

$$\rho_2 = \frac{\eta_b - \eta_1}{\eta_b + \eta_1} \quad \tau_2 = 1 + \rho_2$$

- Half space of η_a and half space of η_b separated by a slab of dielectric, ℓ_1 thick with η_1
- Field incident from the right
- Find total reflection: $\Gamma_1 = \frac{E_{1-}}{E_{1+}}$

Reflection coefficient propagation



From slide 19

$$\Gamma_1 = \frac{\rho_1 + \Gamma'_1}{1 + \rho_1 \Gamma'_1}$$

From slide 14

$$\Gamma'_1 = \Gamma_2 e^{-j2k_1 \ell_1}$$



$$\Gamma_1 = \frac{\rho_1 + \Gamma_2 e^{-j2k_1 \ell_1}}{1 + \rho_1 \Gamma_2 e^{-j2k_1 \ell_1}}$$



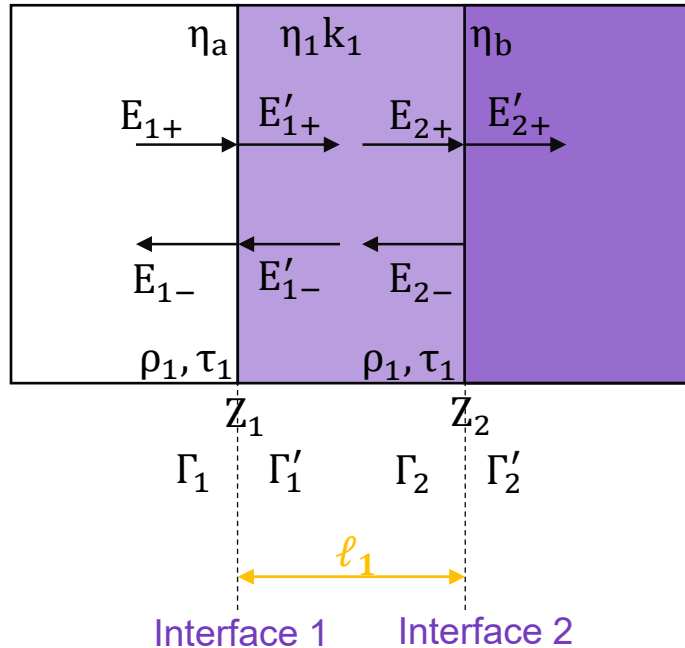
From slide 20

$$\Gamma_2 = \rho_2$$



$$\Gamma_1 = \frac{\rho_1 + \rho_2 e^{-j2k_1 \ell_1}}{1 + \rho_1 \rho_2 e^{-j2k_1 \ell_1}}$$

Matching and propagation matrices (1/2)



From slide 17

$$\begin{bmatrix} E_{1+} \\ E_{1-} \end{bmatrix} = \frac{1}{\tau_1} \begin{bmatrix} 1 & \rho_1 \\ \rho_1 & 1 \end{bmatrix} \begin{bmatrix} E'_{1+} \\ E'_{1-} \end{bmatrix}$$

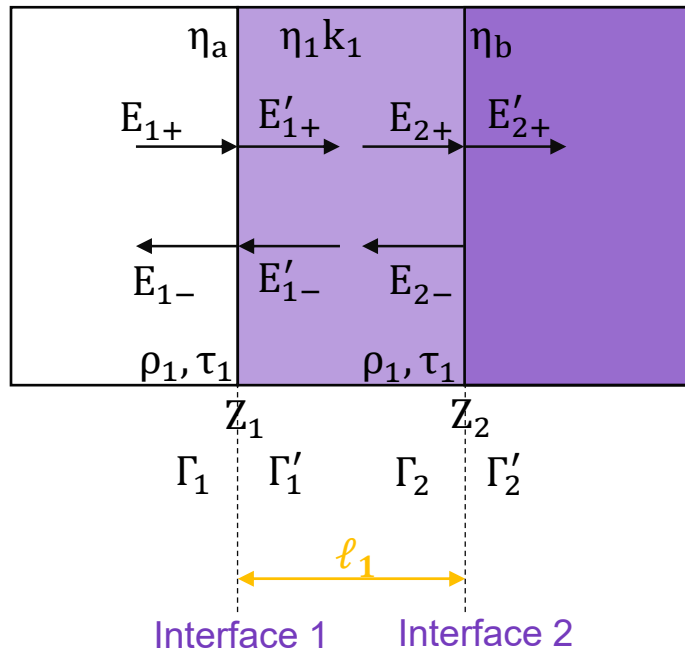
From slide 14

$$\begin{bmatrix} E_{1+} \\ E_{1-} \end{bmatrix} = \frac{1}{\tau_1} \begin{bmatrix} 1 & \rho_1 \\ \rho_1 & 1 \end{bmatrix} \begin{bmatrix} e^{jk_1 \ell_1} & 0 \\ 0 & e^{-jk_1 \ell_1} \end{bmatrix} \begin{bmatrix} E_{2+} \\ E_{2-} \end{bmatrix}$$

From slide 17

$$\begin{bmatrix} E_{1+} \\ E_{1-} \end{bmatrix} = \frac{1}{\tau_1} \begin{bmatrix} 1 & \rho_1 \\ \rho_1 & 1 \end{bmatrix} \begin{bmatrix} e^{jk_1 \ell_1} & 0 \\ 0 & e^{-jk_1 \ell_1} \end{bmatrix} \frac{1}{\tau_2} \begin{bmatrix} 1 & \rho_2 \\ \rho_2 & 1 \end{bmatrix} \begin{bmatrix} E'_{2+} \\ E'_{2-} \end{bmatrix}$$

Matching and propagation matrices (2/2)



From slide 20: $E'_{2-} = 0$

$$\begin{bmatrix} E_{1+} \\ E_{1-} \end{bmatrix} = \frac{1}{\tau_1} \begin{bmatrix} 1 & \rho_1 \\ \rho_1 & 1 \end{bmatrix} \begin{bmatrix} e^{jk_1 \ell_1} & 0 \\ 0 & e^{-jk_1 \ell_1} \end{bmatrix} \frac{1}{\tau_2} \begin{bmatrix} 1 & \rho_2 \\ \rho_2 & 1 \end{bmatrix} \begin{bmatrix} E'_{2+} \\ 0 \end{bmatrix}$$



Multiply through

$$E_{1+} = \frac{e^{jk_1 \ell_1}}{\tau_1 \tau_2} (1 + \rho_1 \rho_2 e^{-j2k_1 \ell_1}) E'_{2+}$$

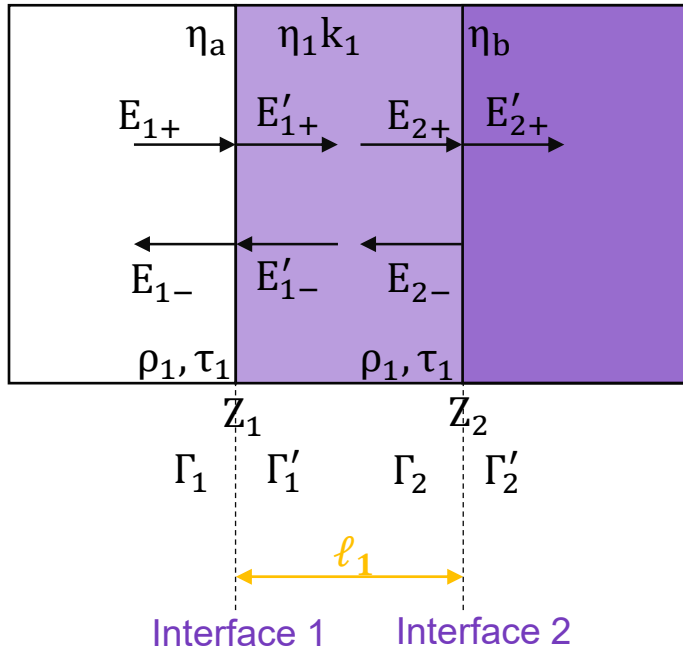
ratio



$$E_{1-} = \frac{e^{jk_1 \ell_1}}{\tau_1 \tau_2} (\rho_1 + \rho_2 e^{-j2k_1 \ell_1}) E'_{2+}$$

$$\Gamma_1 = \frac{E_{1-}}{E_{1+}} = \frac{\rho_1 + \rho_2 e^{-j2k_1 \ell_1}}{1 + \rho_1 \rho_2 e^{-j2k_1 \ell_1}}$$

Transmission



From slide 21: $E'_{2-} = 0$

$$\begin{bmatrix} E_{1+} \\ E_{1-} \end{bmatrix} = \frac{1}{\tau_1} \begin{bmatrix} 1 & \rho_1 \\ \rho_1 & 1 \end{bmatrix} \begin{bmatrix} e^{jk_1 \ell_1} & 0 \\ 0 & e^{-jk_1 \ell_1} \end{bmatrix} \frac{1}{\tau_2} \begin{bmatrix} 1 & \rho_2 \\ \rho_2 & 1 \end{bmatrix} \begin{bmatrix} E'_{2+} \\ 0 \end{bmatrix}$$



$$E_{1+} = \frac{e^{jk_1 \ell_1}}{\tau_1 \tau_2} (1 + \rho_1 \rho_2 e^{-j2k_1 \ell_1}) E'_{2+}$$



$$T_1 = \frac{E'_{2+}}{E_{1+}} = \frac{\tau_1 \tau_2 e^{-jk_1 \ell_1}}{1 + \rho_1 \rho_2 e^{-j2k_1 \ell_1}}$$

Conclusions and next time

- Boundary conditions (field continuities) allow for a solution to the steady state time harmonic total fields
- $E_+(z)$, $E_-(z)$, and $\Gamma(z)$ have **simple propagation matrices** but **complicated relations across the interface**
- $E(z)$, $E(z)$, and $Z(z)$ have **complicated propagation matrices** but **simple relations across the interface**
- The matrix from provides a natural form for recursion and enables solution of the total transmitted field
- Next time we'll
 - Solve for the reflection via geometric series (ray tracing)
 - Extrapolate to multiple layers
 - Explore oblique incidence angle