

GEO – E1050 Finite Element Method in Geoengineering

Boundary element method

Wojciech Sołowski

2 components:

- a) some analytical solution we will use in our approximation (FUNDAMENTAL SOLUTION)
- b) discretisation, so we use our fundamental solution over and over again, over some finite domain

of course... fundamental solution must exists ... and must be known... ... and generally should not be too complex...



Method reduce the dimension of the problem by 1 so:

2D problem becomes 1D problem; requires 2D fundamental solution

3D problem becomes 2D problem; requires 3D fundamental solution

We discretise the boundary of the problem only – hence the name: 'boundary element method'



Reducing dimensions of the problem is **HUGE**

however...

Fundamental solutions only can be analytically computed for simple cases...

- linear elasticity
- Poisson equation problems
- and similar...

Cannot be used for elasto-plasticity (at least not easily)



For example, for Poisson equation,

$$\mathbf{q} = -\mathbf{D}\nabla u$$

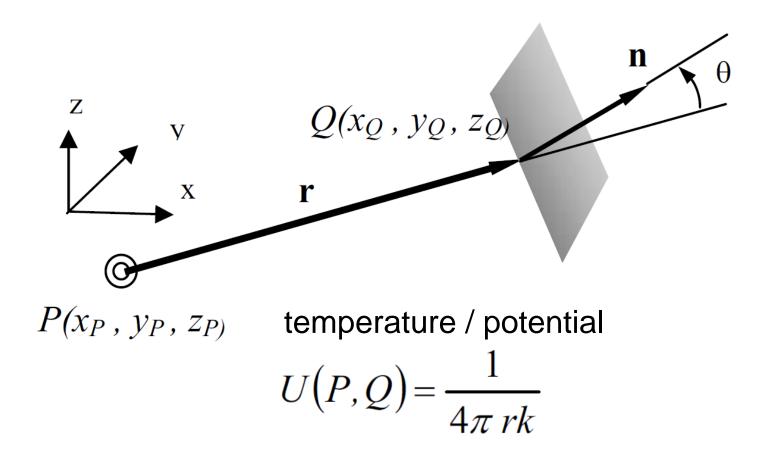
We assume some source at point $P(x_p, y_p, z_p)$ in infinite space and at some point Q the temperature / potential is:

$$U(P,Q) = \frac{1}{4\pi \, rk}$$

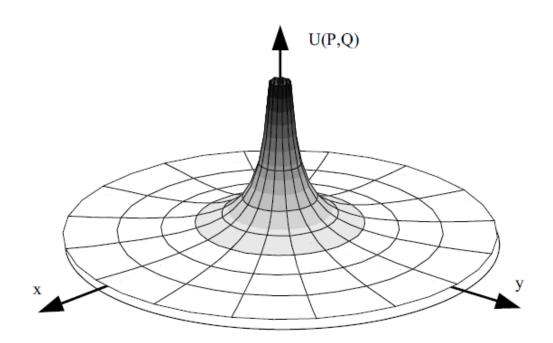
And if we assume flow in x direction, the flow at point P is:

 $T(P,Q) = \frac{\cos\theta}{4\pi r^2}$



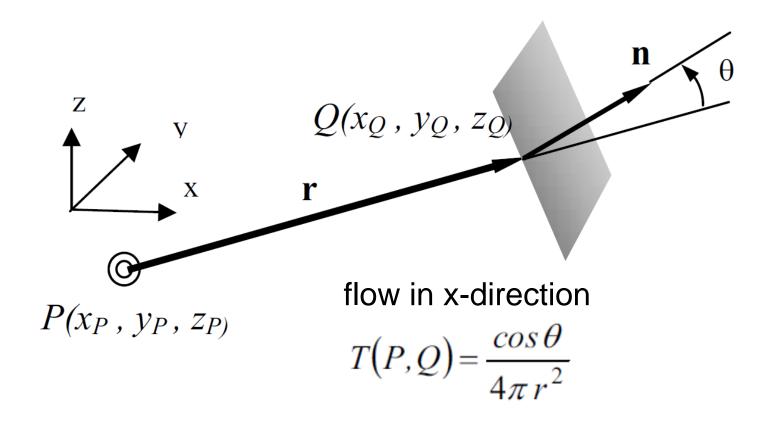




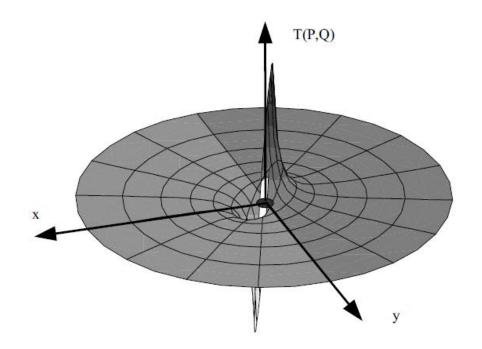


Variation of fundamental solution U (potential/temperature) in the x-y plane for 3-D potential problems (source at origin of coordinate system)









Variation of fundamental solution for $\mathbf{n} = \{1,0,0\}$ (flow in x-direction) in x-y plane for 3-D potential problems (e.g. temperature changes if flow is happening)



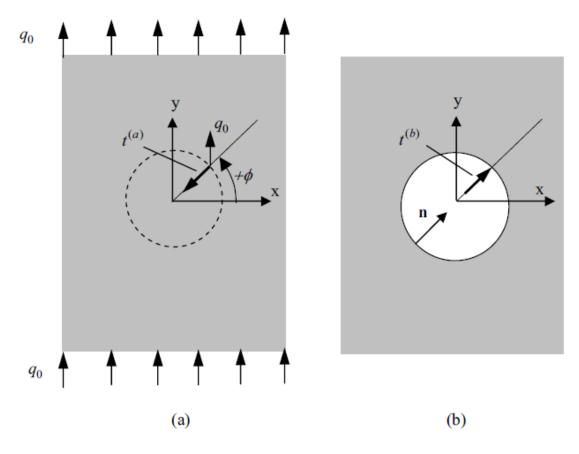


Figure 5.1 Heat flow in an infinite domain, case (a) and (b)



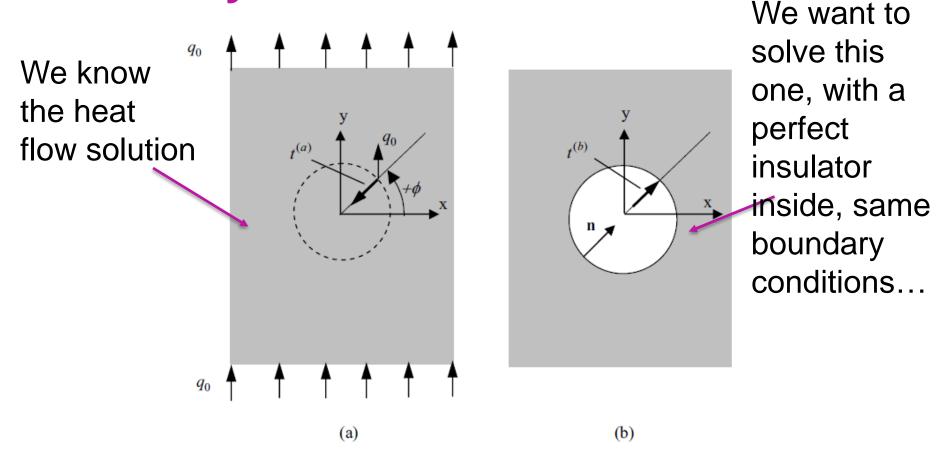
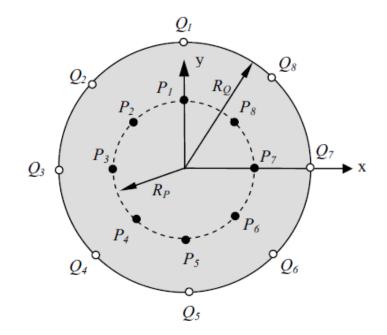


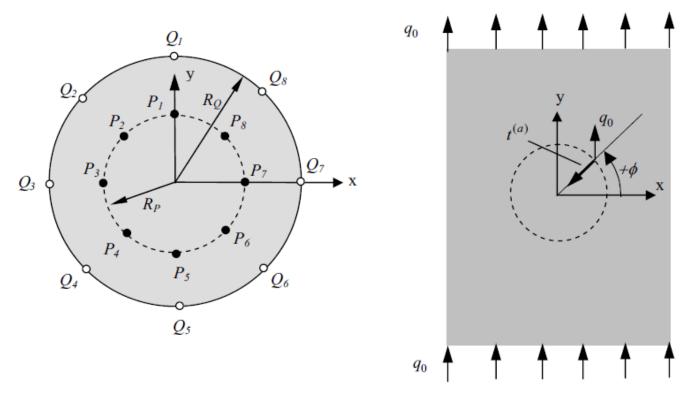
Figure 5.1 Heat flow in an infinite domain, case (a) and (b)





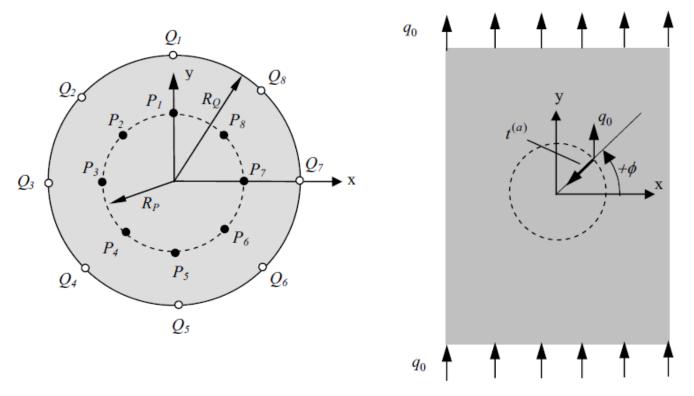
We want to approximate the known solution on the outside by the sources (we have the fundamental solution for those)





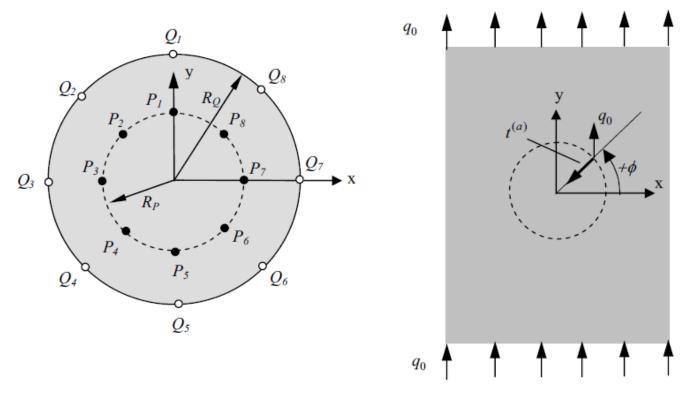
The sources should be such, that on the boundary we have exactly same solution as the one without the insulator...





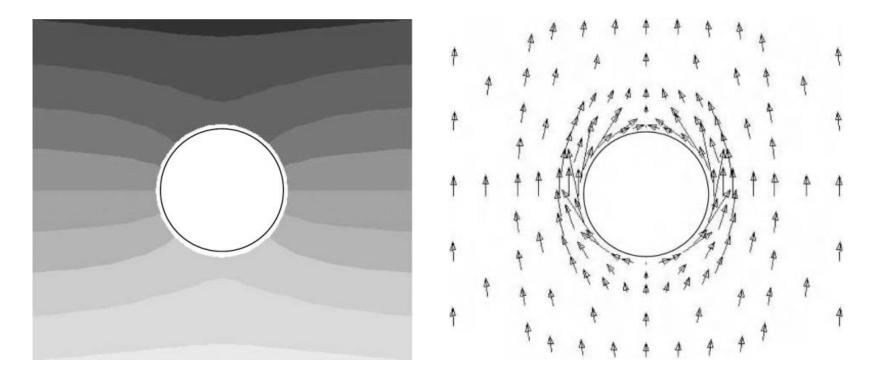
Now, to get the solution with the insulator, we use the superposition – from the known solution we subtract the one obtained with the sources... **And we are done...**





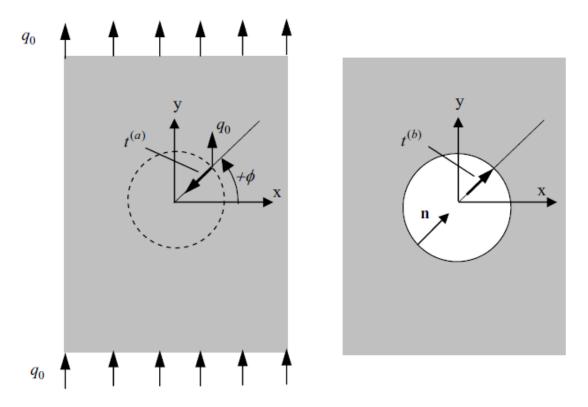
The better we discretize the boundary of the insulator, the more sources we can add, the better the solution...





Temperature and flow vectors for the solved problem





How to solve the problem on the right, where we have void and the boundary condition on the void is T=const.





GEO – E1050 Finite Element Method in Geoengineering

Lecture 11-12. Other numerical methods

To learn today & next time...

The lectures should give you overview of other numerical methods

- 1. Discrete element method (DEM, also distinct element method)
 - assumptions, solutions, problmes & accuracy
- 2. Smoothed particle hydrodynamics (SPH)
- 3. Material Point Method (MPM)
- 4. Particle Finite Element Method in Geoengineering (PFEM)
- 5. XFEM eXtended Finite Element Method in Geoengineering (XFEM)

Other existing methods, not covered today:

- 6. ALE , CLE Coupled Lagrangian Eurlerian FEM
- 7. Meshfree methods



Methods on continuous – discontinuous scale

FEM	CLE, ALE Coupled Lagrangian – FEM Eurlerian FEM			Smoothed Particle Hydrodynamics (SPH)		Discrete element method (DEM)
Continuo	ous	Classical Meshfree methods	PFEM	XFEM	Disco	ontinuous
Based on continuum mechanics			Not based on continuum mechanics			

Methods on continuous – discontinuous scale

CLE, ALE: Coupled / Arbitrary Lagrangian – FEM Eurlerian FEM			ry MPM	Smoothed Particle Hydrodyna (SPH)	Discrete element mics method (DEM)
Continuo	ous	Classical Meshfree methods	PFEM	XFEM	Discontinuous
		Based on continuum mechanics		Not based continuum mechanics	

Also known as distinct element method

Idea: we model each grain of soil separately

We need to model all the contacts and contact behaviour

Each time step – we evaluate forces and velocities of all particles

Contact & contact forces are essential

Normally used for granular materials and atoms

Also known as distinct element method

Idea: we model each grain of soil separately

We need to model all the contacts and contact behaviour

Each time step – we evaluate forces and velocities of all particles. Method is time-step dependent

Contact & contact forces are essential

Due to simplified shapes of particles and simplified contact, method is known to be **problem and size dependent** (i.e. requires different parameters for different problems with same material)

Also known as distinct element method



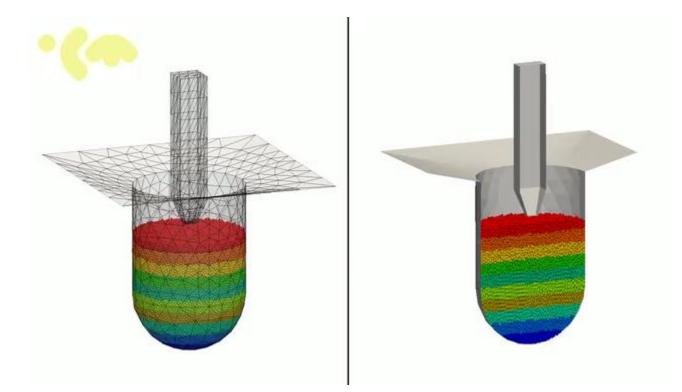
Few simulations: Hannover, group of Prof. Wriggers

Also known as distinct element method



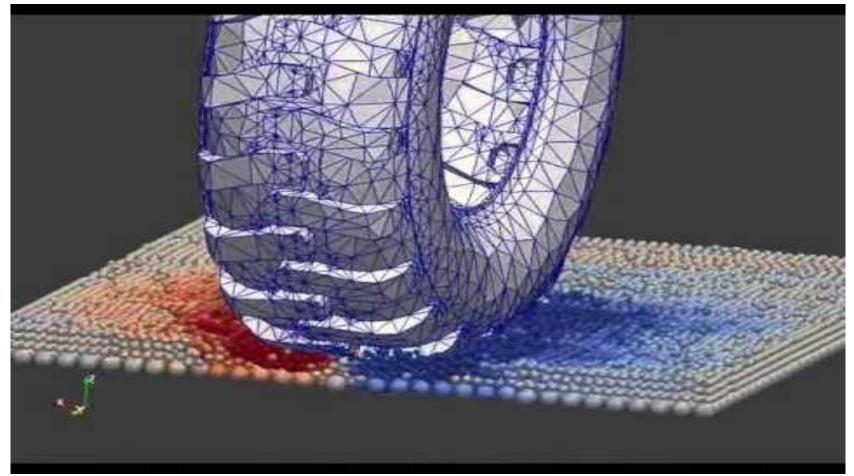
Few simulations: Hannover, group of Prof. Wriggers

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Few simulations: Hannover, group of Prof. Wriggers

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DEM FEM coupling

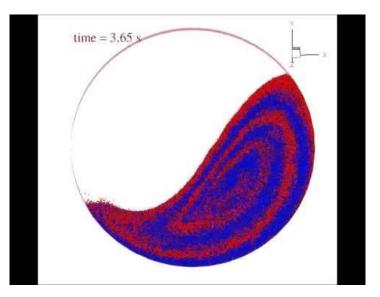
Also known as distinct element method

Convergence:

<u>UoM presentation - DEM convergence.pdf</u>

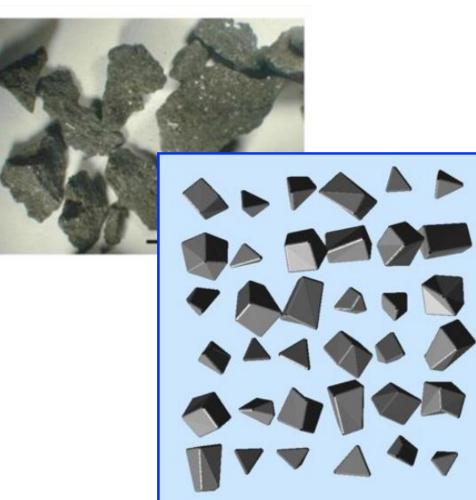
More simulations:

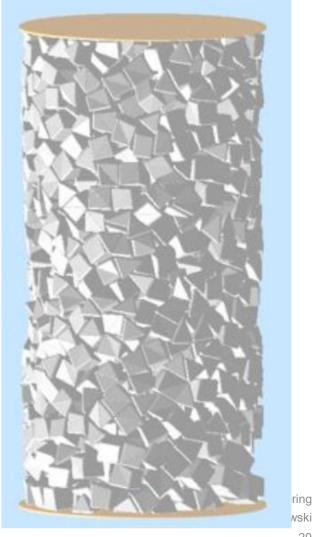
In short, 2D quite does not work and 3D is very expensive... and even then it may not work...

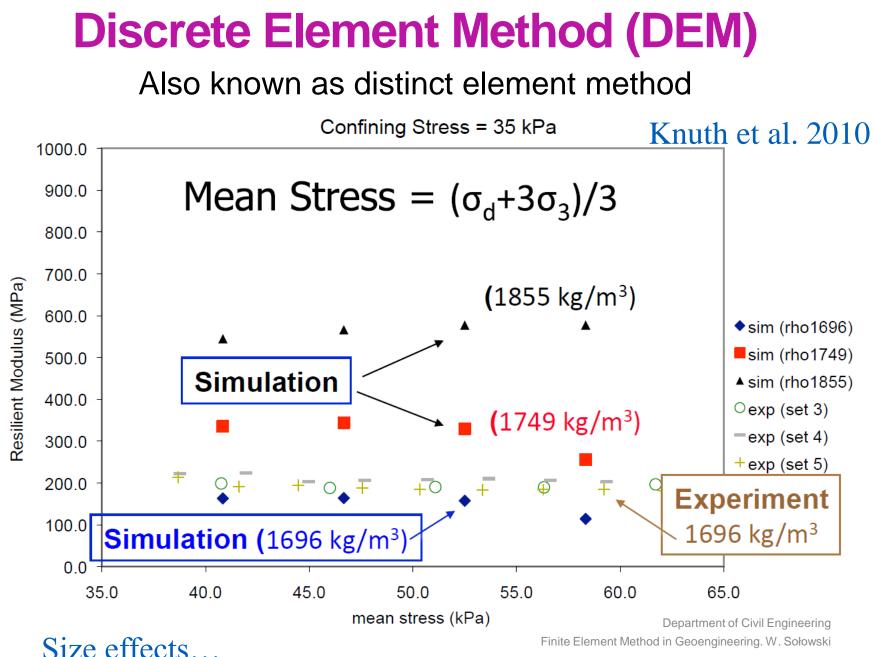


Also known as distinct element method Knuth et al. 2010

Shape effects...







Also known as distinct element method

Software:

- YADE (free & open source)
 - generally non-cohesive materials, or materials with some cohesion

Quite a lot of other software...

3DEC – by ITASCA, now popular in mining industry

Also known as distinct element method

Wait, using DEM for non-granular materials???

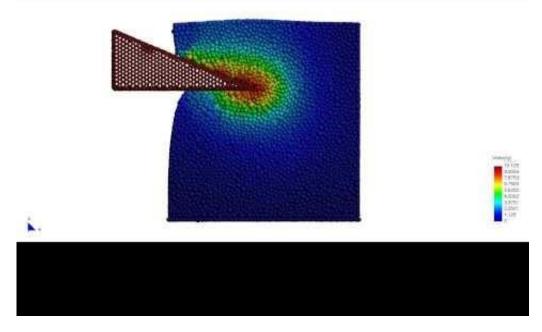
Of course leads to lots of problems and issues:

- in reality to get decent results cohesion between grains should be scale dependent
- contact between assemblies of non smooth particles (i.e. when crack is formed) is again problematic (generally, to get real surface with required roughness, MANY particles are needed, and other solutions do not work well
- currently used rather for flow than anything else...

Also known as distinct element method

Wait, using DEM for non-granular materials???

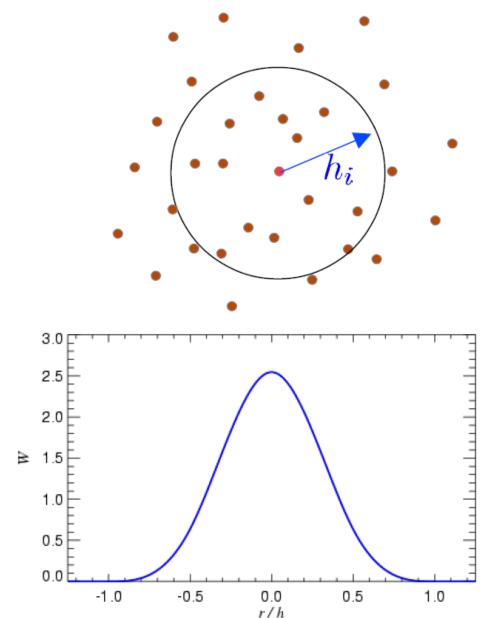






Smoothed particle hydrodynamics (SPH)

Smoothed Particle Hydrodynamics (SPH)



Density computed via weighted sum over neighbouring particles...

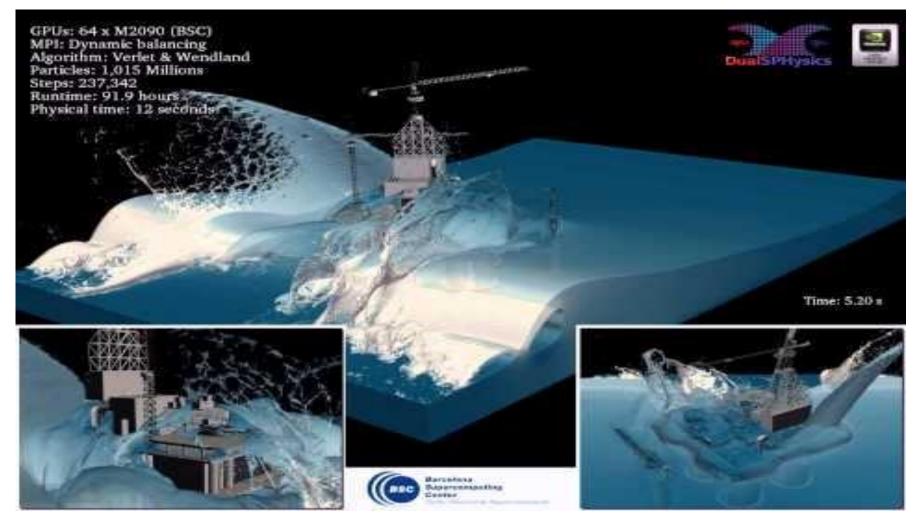
Smoothed Particle Hydrodynamics (SPH)

Problems:

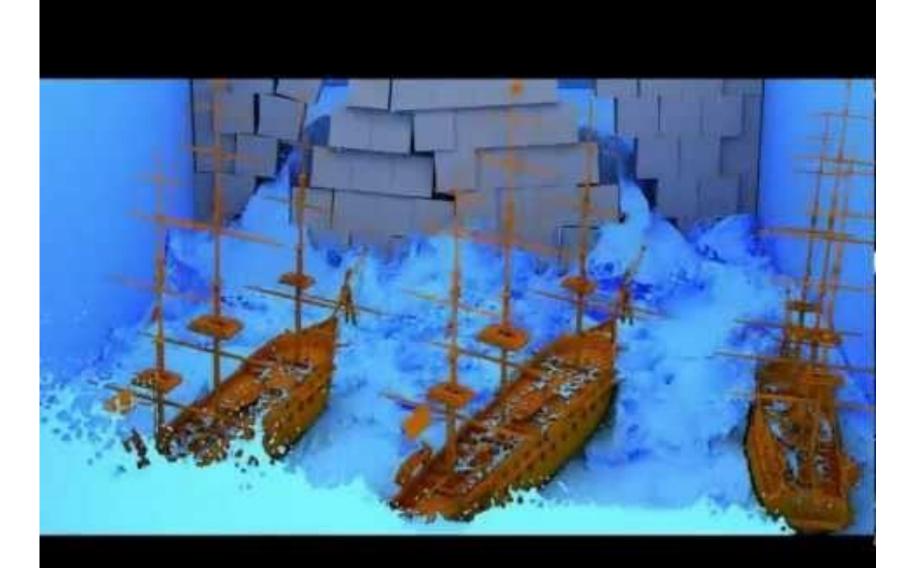
- boundary conditions
- numerical noises
 - sometimes velocity noise of few percent of local sound speed...
 - instabilities over contact discontinuities
- requires high artificial viscosity (to mute errors), giving high viscosity of the system, leading to errors

Benefits:

- versatile, simple, good conservation properties
- quite robust

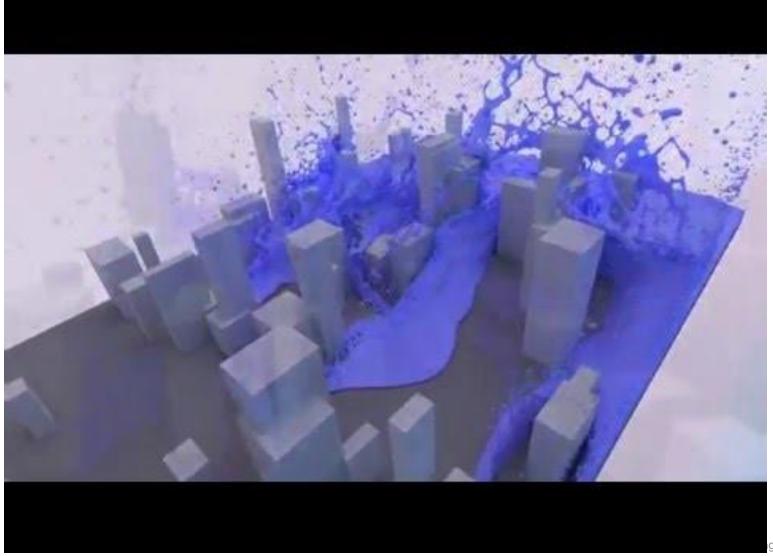


Barcelona supercomputing centre





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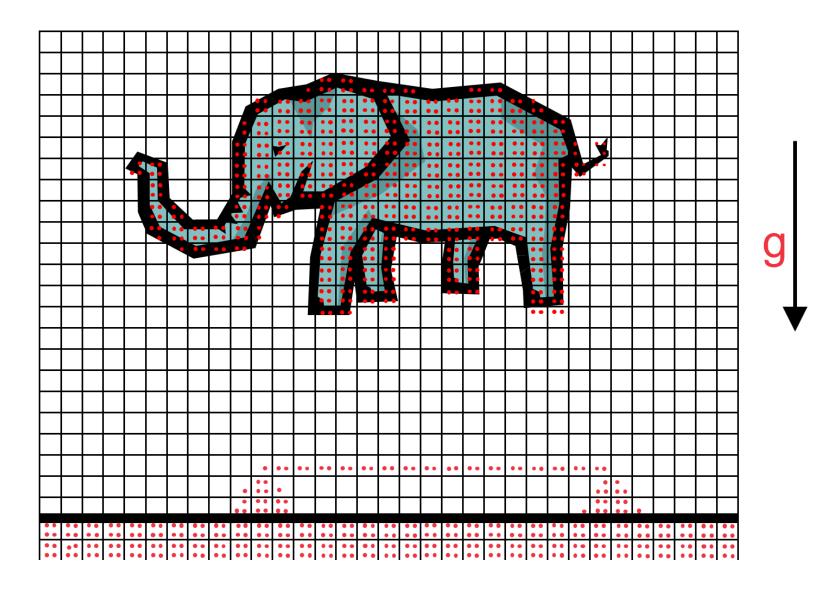
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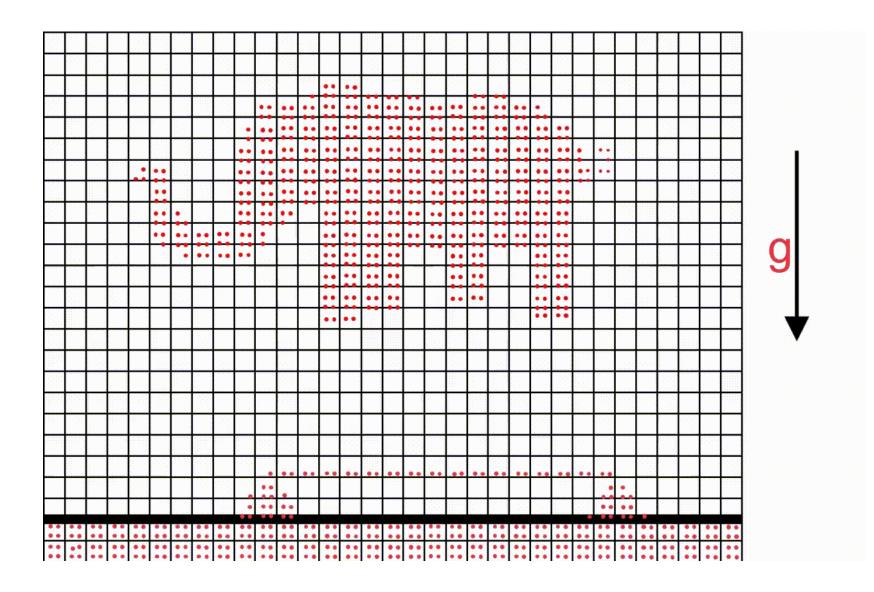
Finite Element Method in Geoengineering. W. Sołowski

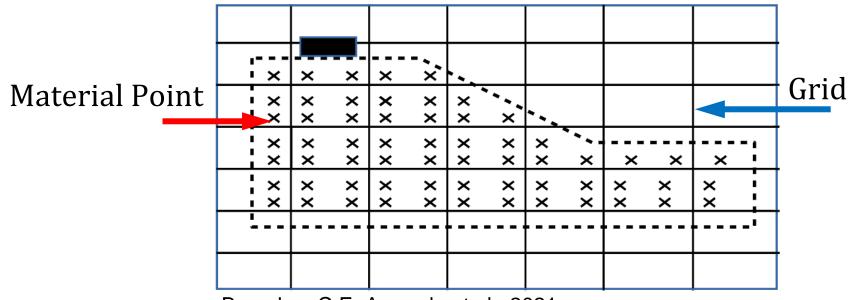
Material Point Method MPM



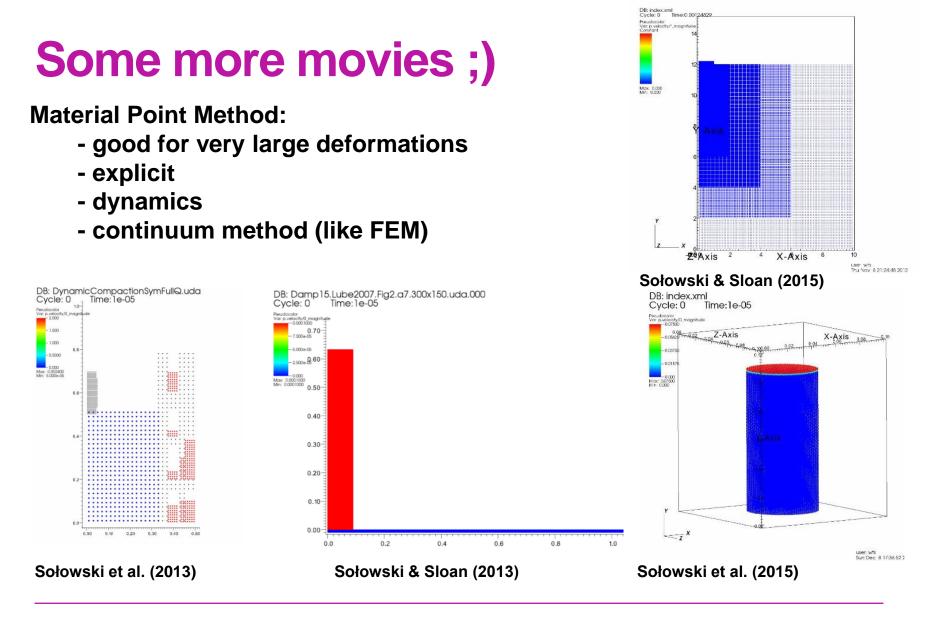








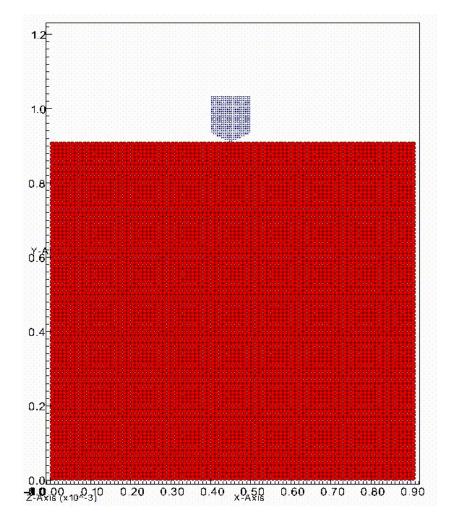
Based on C.E. Augarde et al., 2021





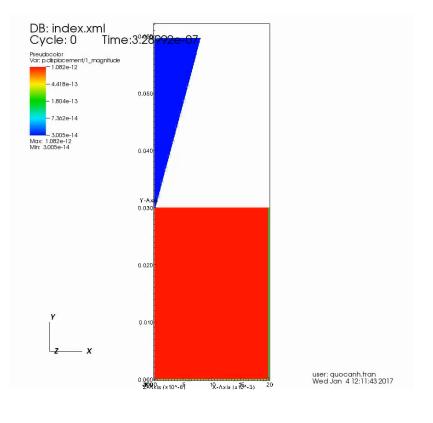
Material Point Method:

- good for very large deformations
- explicit
- dynamics
- continuum method (like FEM)



Seyedan and Sołowski (2022?)

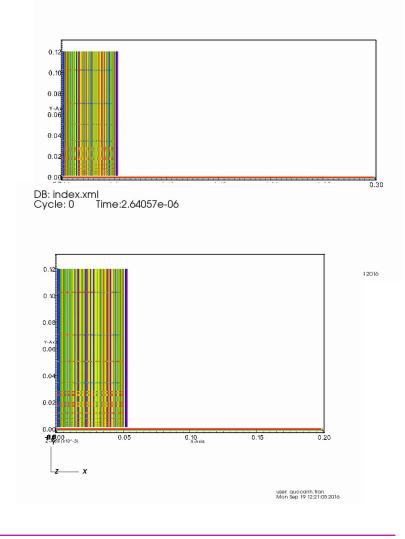


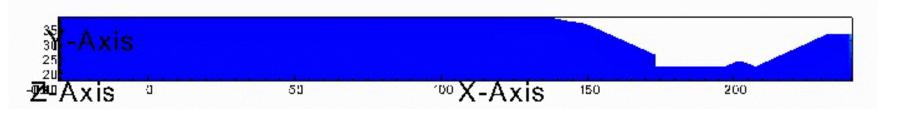


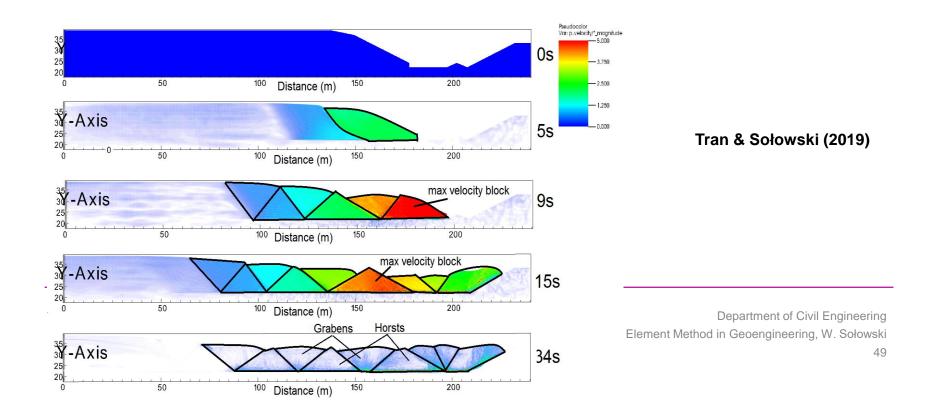
Tran et al. (2017)

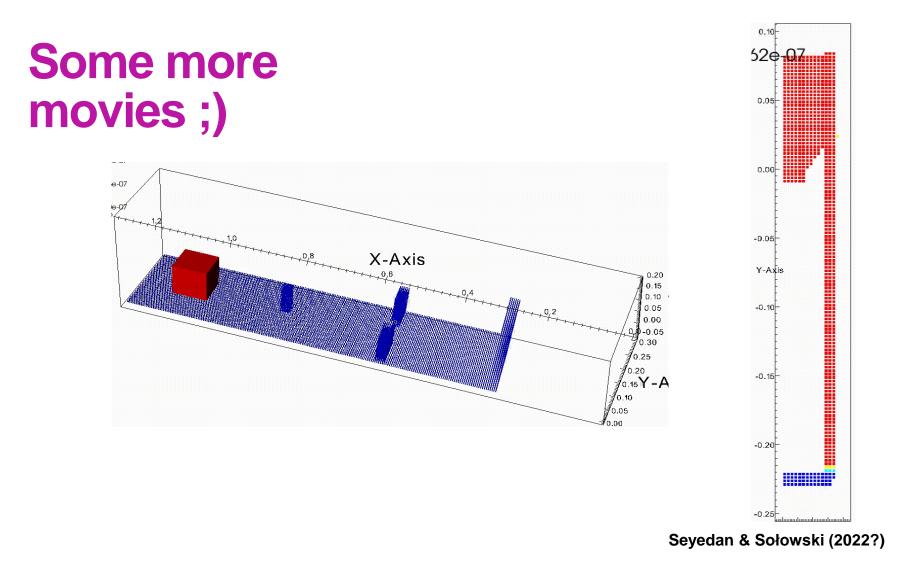


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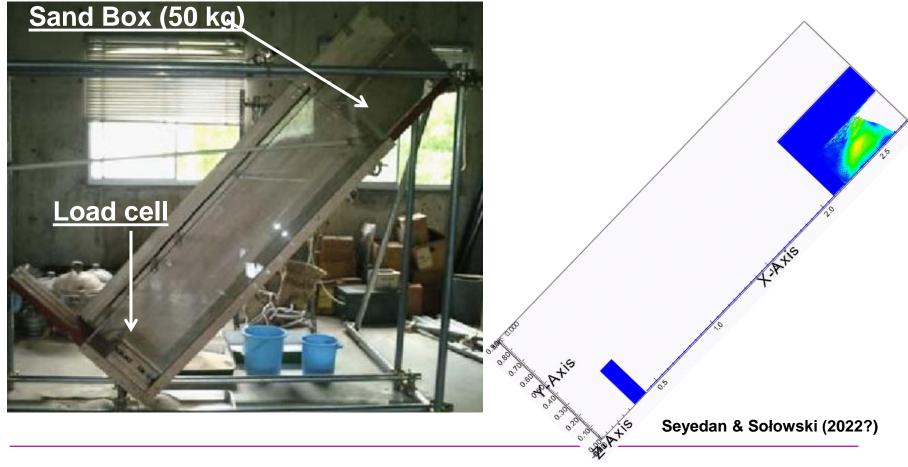






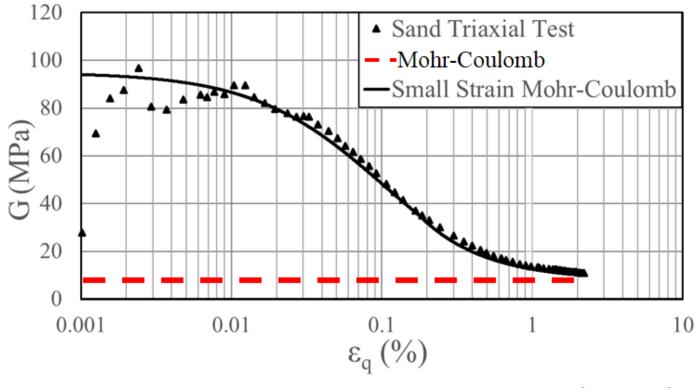






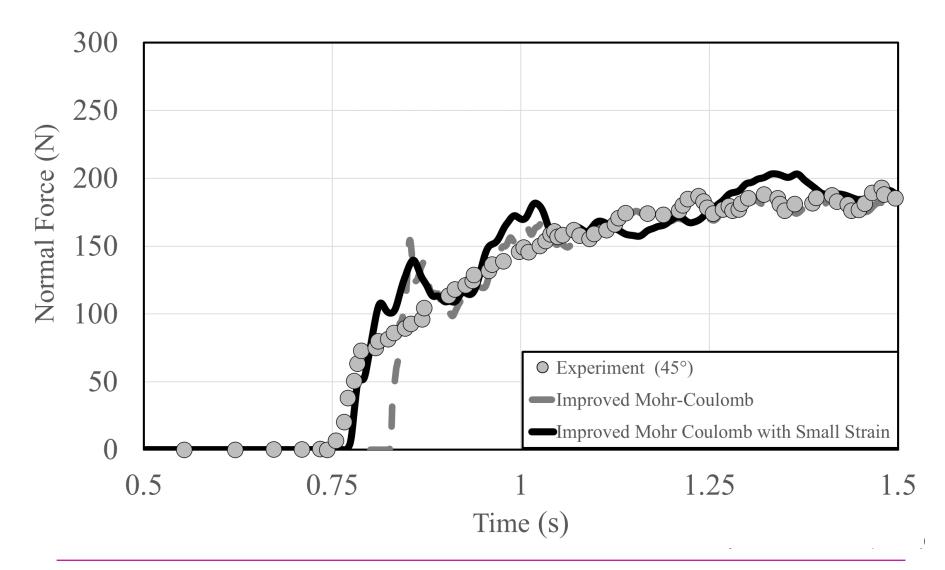


A yield surface to capture small strain behavior



Seyedan & Sołowski (2022?)











with thanks to K. Agathos (Aristotle U. of Thessaloniki) and E. Chatzi, (IBK, D-BAUG, ETH Zurich)

XFEM – eXtended Finite Element Method

Aim: to introduce discontinuities into continuous FEM

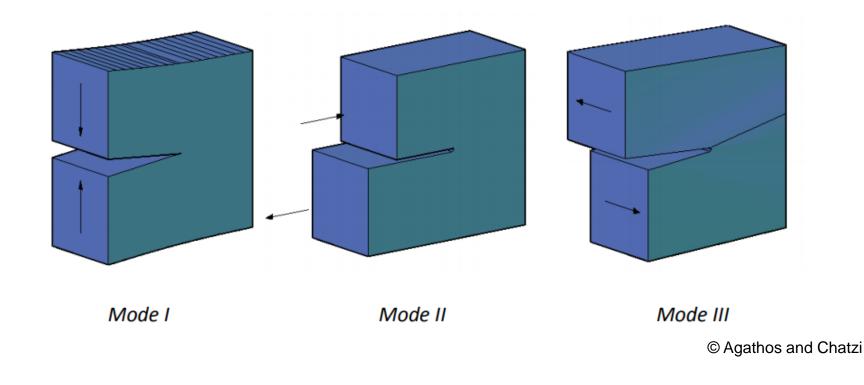
- Strong discontinuity: crack jump in displacements
- Weak discontinuity jump in strains

Used to determine displacement, strain and stress fields in structures with cracks and small holes. Allows for discontinuous displacements and strain fields



XFEM – eXtended Finite Element Method

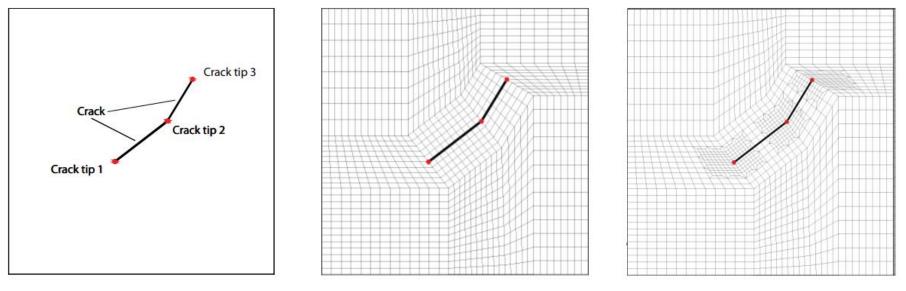
Aim: to introduce discontinuities into continuous FEM





XFEM – eXtended Finite Element Method

To model the crack, we need nodes placed across the crack and on the crack tips



[©] Agathos and Chatzi



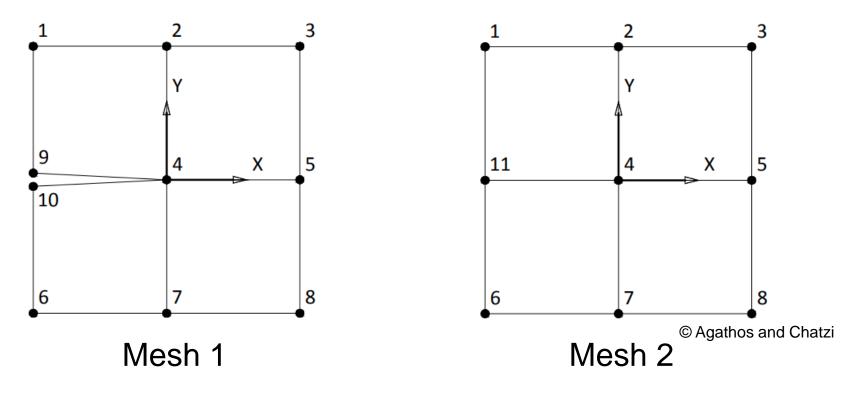
When we have a crack, we have jump in displacements. However, we want to describe it with a continuous mesh, i.e. without physically modelling crack width.

For that, we enrich the element nodes with jump function for displacements. At one side of the node, it has a different value than at the other side of the node.

Technically we use Heaviside function H(x) for that...

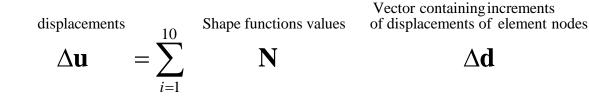


In other words, we want to represent the situation in Mesh 1 (physical crack), with Mesh 2

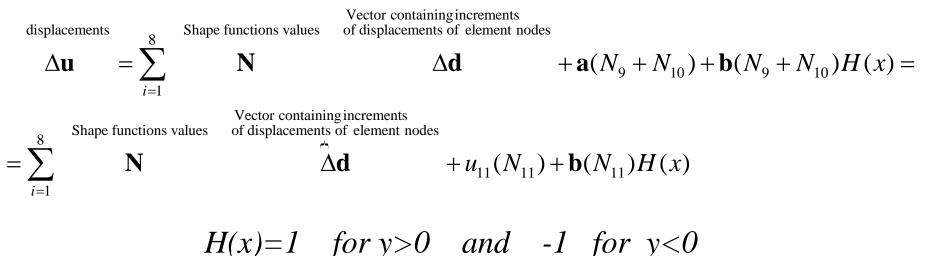




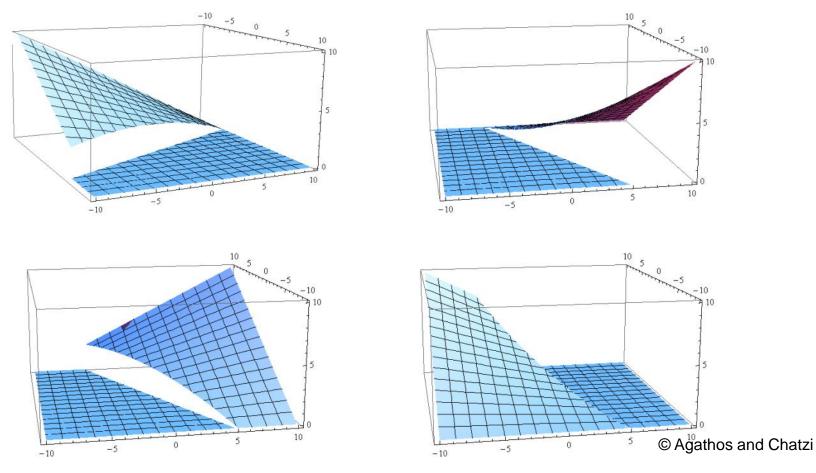
The displacements at any point (and in particular in nodes 9 and 10) are:



Defining \mathbf{a} =0,5 (\mathbf{d}_9 + \mathbf{d}_{10}) and \mathbf{b} =0,5 (\mathbf{d}_9 - \mathbf{d}_{10}) we get

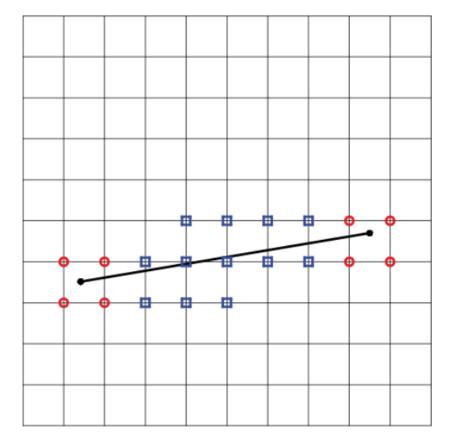


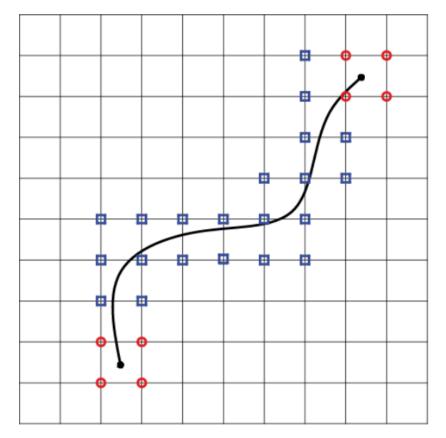




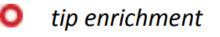
Jump enrichment in action $\ensuremath{\textcircled{\sc 0}}$







© Agathos and Chatzi



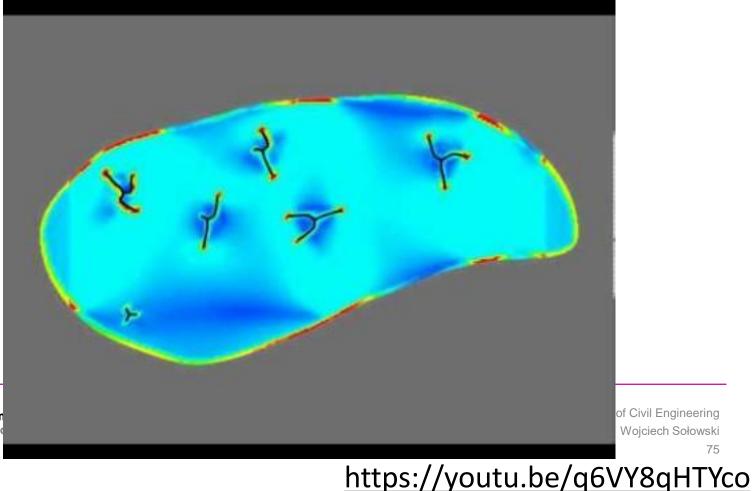
jump enrichment



Aalto University School of Engineering

XFEM – abilities

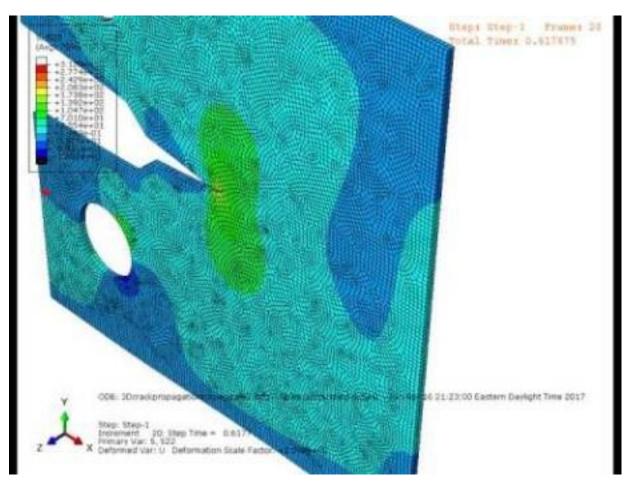
The method – with extensions – can deal with crack propagation, crack branching and intersecting etc. Also can be used with plasticity and in dynamic problems





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XFEM – abilities



https://youtu.be/eKhrRpwxOq0



Thank you

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