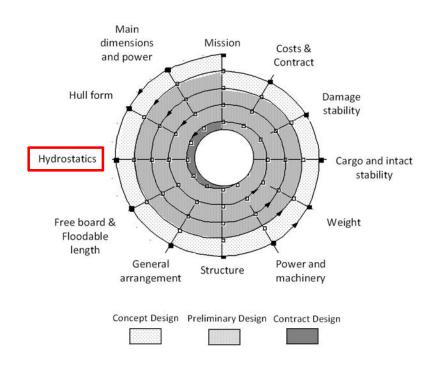


### **MEC-E1004 Principles of Naval Architecture**

*Lecture 5 – Hydrostatics* 

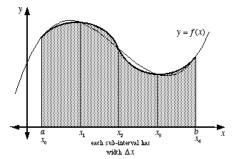
### Learning points!

- Explain the purpose of numerical integration in ship design
- Explain and apply basic hydrostatic formulas and methods



### Assignment 5 – Hydrostatics

- Create draft line drawings of your ship's hull
- Estimate the hull volume and verify the correctness of your calculations using numerical integration methods (e.g. Simpson Rules on frame area or hull volume)



The shaded area bounded by the parabolas (the thicker curves) is approximately equal to the area bounded by y=f(x).

$$\int_{A}^{A} f(x) dx = \frac{\Delta x}{3} \Big[ f(x_0) + 4f(x_1) + 2f(x_2) + 4f(x_3) + f(x_4) \Big]$$



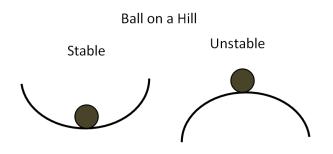
Image credit Meyer Turku

## **Hydrostatics**

Question: What is hydrostatics and why they are important in ship design?

### What is Hydrostatics?

- A branch of physics that deals with the characteristics of fluids at rest. The fluid can be gas or liquid exerting pressure on an immersed body.
- Through hydrostatics we investigate the floating position
- Applied in ship design to assess a ship's
  - Floatation
  - Stability



### **Ship Geometry**

- The determination of a ship's geometry is a complex task that requires the consideration of multiple factors
  - Volumes, dimensions of cargo holds
  - Seakeeping, i.e safety in waves
  - Resistance, i.e. hull performance and energy efficiency
  - Aesthetics
  - ...
- Accurate representation of geometry is important for
  - Safety and Performance assessment
  - Manufacturing
- Challenge
  - Complex hull shapes
    - Double curvature in many places
      - o Bended beams, plates,...





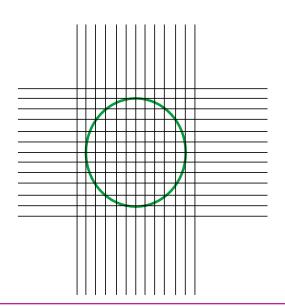


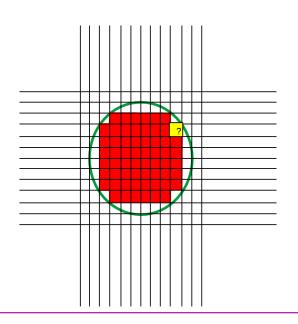
### Exact methods vs numerical aprox.

$$A = \rho r^2 = \rho (5)^2 = 25\rho^2 \gg 78.5$$

$$A \approx whole \ squares + \frac{1}{2} \ part \ squares = 59 + \frac{29}{2} = 73.5$$

$$A \gg 60 + \frac{28}{2} = 74$$





- Integration is nowadays carried out using computers, e.g.
  - AutoCAD
  - SolidEdge
  - Plot Digitizer
  - NAPA
  - *etc...*
- Numerical estimations do not always represent reality
- Useful for any geometry (even geometries which do not have analytical solutions)

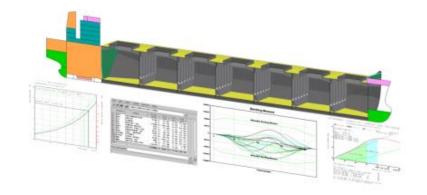
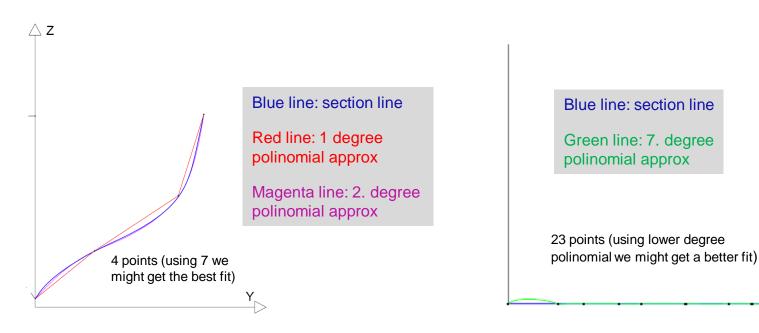


Image credit Napa

### How many points?...too many is not necessarily good!





Area

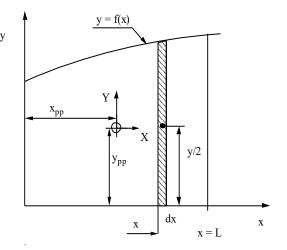
Distance from y-axis

Distance from x-axis

$$A = \int_{0}^{A} dA = \int_{0}^{L} y dx$$

$$x_{pp} = \frac{M_{y}}{A}$$

$$y_{pp} = \frac{M_x}{A}$$



### Moment of area A with respect to y-axis M<sub>v</sub>

$$M_{y} = \int_{0}^{A} \left( x + \frac{dx}{2} \right) dA = \int_{0}^{L} \left( x + \frac{dx}{2} \right) y dx = \int_{0}^{L} \left( xy dx + \frac{y(dx)^{2}}{2} \right) \approx \int_{0}^{L} xy dx$$

#### Moment with respect to x-axis

$$M_x = \int_0^A \frac{y}{2} dA = \int_0^L \frac{y}{2} y dx = \frac{1}{2} \int_0^L y^2 dx$$

#### Parallel axis theorem

$$I_Y = I_y + x_{pp}^2 A$$

#### Second moment of area (A) with respect to x-axis

$$I_{x} = \int_{0}^{A} y^{2} dA = \int_{0}^{L} \int_{0}^{y} y^{2} dy dx = \frac{1}{3} \int_{0}^{L} y^{3} dx$$

### Second moment of area (A) with respect to y-axis

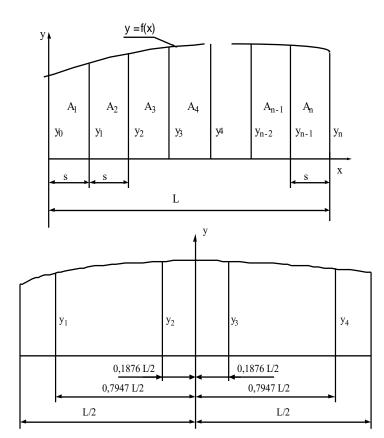
$$I_{y} = \int_{0}^{A} x^{2} dA = \int_{0}^{L} x^{2} y dx$$

### If evenly spaced ordinates

- Rectangle rule (Piecewise constant estimation of curve)
- $\bullet \ \ Trapezoidal \ rule \ \ ({\tt Piecewise \, linear \, estimation \, of \, curve})$
- Simpson I rule
- Simpson II rule

### If unevenly spaced ordinates

- Tsebysev rule
- Gauss rule (used in FEM)





$$A_i = \frac{1}{2} s \left( y_{i-1} + y_i \right)$$

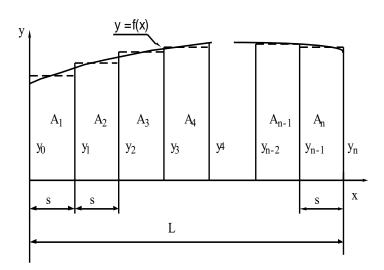
$$A = \sum_{i=1}^{n} A_{i} = A_{1} + A_{2} + A_{3} + \dots + A_{n}$$

$$= \frac{1}{2} s(y_{1-1} + y_{1}) + \frac{1}{2} s(y_{2-1} + y_{2}) + \frac{1}{2} s(y_{3-1} + y_{3}) + \dots + \frac{1}{2} s(y_{n-2} + y_{n-1}) + \frac{1}{2} s(y_{n-1} + y_{n})$$

$$= \frac{1}{2} s(y_{0} + y_{1}) + \frac{1}{2} s(y_{1} + y_{2}) + \frac{1}{2} s(y_{2} + y_{3}) + \dots + \frac{1}{2} s(y_{n-2} + y_{n-1}) + \frac{1}{2} s(y_{n-1} + y_{n})$$

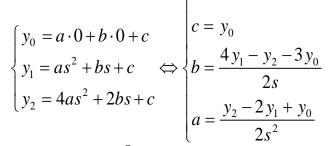
$$= s \left[ \frac{1}{2} (y_{0}) + \frac{1}{2} (y_{1} + y_{1}) + \frac{1}{2} (y_{2} + y_{2}) + \frac{1}{2} y_{3} + \dots + \frac{1}{2} (y_{n-2}) + \frac{1}{2} (y_{n-1} + y_{n-1}) + \frac{1}{2} y_{n} \right]$$

$$= s \left[ \frac{1}{2} (y_{0}) + y_{1} + y_{2} + \dots + y_{n-1} + \frac{1}{2} y_{n} \right]$$



Numerical integration – Simpson I

The spacing needs to be even, because the solution of parabolic approximation requires solution of coefficients a, b and c based on three consecutive coordinates



Equation for parabola

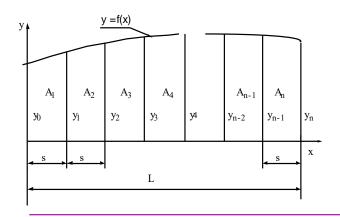
$$y = ax^2 + bx + c$$

Known values

$$x=0$$

$$x=s$$

$$x=2s$$



So area for two areas is

$$A = A_1 + A_2 = \int_0^{2s} y dx = \int_0^{2s} (ax^2 + bx + c) dx = \frac{8}{3}as^3 + 2bs^2 + 2sc$$

$$= \frac{4}{3} (y_2 - 2y_1 + y_0)s + (4y_1 - y_2 - 3y_0)s + 2s(y_0) = \frac{s}{3} (y_0 + 4y_1 + y_2)$$

And the whole area investigated

$$\begin{vmatrix}
A = (A_1 + A_2) + (A_3 + A_4) + \dots + (A_{n-1} + A_n) \\
= \left[ \frac{s}{3} (y_0 + 4y_1 + y_2) \right] + \left[ \frac{s}{3} (y_2 + 4y_3 + y_4) \right] + \dots + \left[ \frac{s}{3} (y_{n-2} + 4y_{n-1} + y_n) \right] \\
= \frac{s}{3} (y_0 + 4y_1 + 2y_2 + 4y_3 + 2y_4 + \dots + 2y_{n-2} + 4y_{n-1} + y_n)
\end{vmatrix}$$



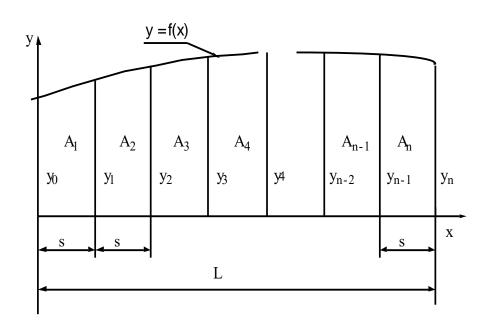
## Numerical integration – Simpson II

- Third order polynomial calls for 4 ordinates
- Spacing n should be multiple of 3

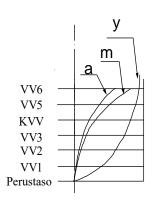
$$A_{1} + A_{2} + A_{3} = \frac{3}{8} s(y_{0} + 3y_{1} + 3y_{2} + y_{3})$$

$$A = \frac{3}{8} s(y_{0} + 3y_{1} + 3y_{2} + 2y_{3} + 3y_{4} + 3y_{5} + \dots + 3y_{n-1} + y_{n})$$

$$A_{1} + A_{2} + A_{3} \qquad A_{4} + A_{5} + A_{6}$$



### Numerical integration – use of tables



#### Frame area

kaari	puoli	1/2S	A-	M-	M-tulo	varsi	I L-tulo	y <sub>n</sub> <sup>3</sup>	IT-
no	-	Mker	tulo	vars		2			tulo
	levey	roin		i					
	s y n								
	(m)	<u> </u>	<u> </u>			<u> </u>			
1	2	3	4 =2*3	5	6= 2*3*5	7	8= 2*3*7	9	10= 3*9
0		1/4		5,0		25,0			
1/2	ì	1	İ	-	Ì	20,2		İ	
				4,5		5			
1		1/2		-		16,0	ĺ		
				4,0					
1		1		-		12,2			
1/2		<u> </u>	<u> </u>	3,5		5			
2		3/4		-		9,0			
	ļ	ļ	ļ	3,0		ļ	<u> </u>		
3		2		-		4,0			
			ļ	2,0		ļ			
4		1		-		1,0			
			ļ	1,0		ļ			
5	ļ	2	ļ	0		0		<u> </u>	<u> </u>
6		1	ļ	1,0		1,0			
7	ļ	2	ļ	2,0	ļ	4,0	ļ	<u> </u>	
8		3/4	ļ	3,0		9,0			
8		1		3,5		12,2			
1/2	ļ		ļ			5	ļ		
9	ļ	1/2	<u> </u>	4,0		16,0	<u> </u>	<u> </u>	<u> </u>
9		1		4,5		20,2			
1/2	ļ	<u> </u>	<u> </u>			5			
10	<u> </u>	1/4	<u>ļ</u>	5,0		25,0	<u> </u>	<u> </u>	
			$\Sigma_1$		$\Sigma_2$		$\Sigma_3$		$\Sigma_4$

#### Volume of the Ship

kaari	kaare	1/2S	∇-	M-	ML-	kaar	My-
no	n	Mker	tulo	vars	tulo	en	tulo
	a	roin		i		m	
	(m <sup>2</sup> )					$(m^3)$	
1	2	3	4	5	6=	7	8=3*7
			=2*3		2*3*5		
0		1/2		-			
				5,0			
1/2		2		-			
	<u> </u>			4,5			
1		1		-			
	ļ			4,0		ļ	
1		2		-			
1/2	ļ			3,5	ļ		
2		3/2		-			
	<u> </u>			3,0			
3		4		-			
	ļ			2,0		ļ	
4		2		-			
	<u> </u>		,	1,0	ļ	ļ	
5 6		4		0			
6		2		1,0			
7		4		2,0			
8		3/2		3,0			
8		2		3,5			
1/2							
9		1		4,0			
9		2		4,5			
1/2							
10		1/2		5,0			
			$\Sigma_1$		$\Sigma_2$		$\Sigma_3$

# **Hydrostatic curves**

A series of graphs that give values such as the center of buoyancy, displacement, moment causing unit trim, and center of flotation

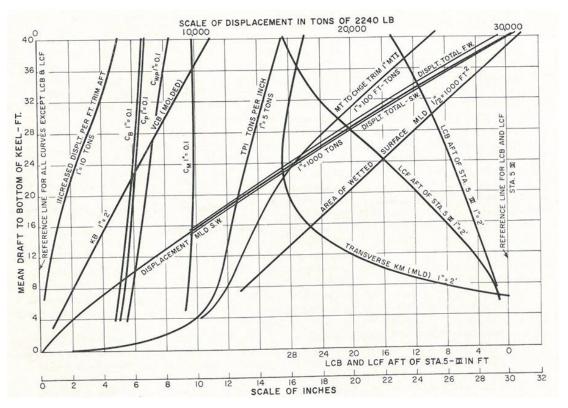


Image credit Principles of Naval Architecture



### Bonjean curves

They are used for the purpose of obtaining, for any given waterline, the areas of the immersed portion of each transverse section throughout the ship's length

### Example

- Path KCL<sub>1</sub>W<sub>1</sub>K equals frame area A at point draught Q
- This can be used to estimate the buoyancy V=A\*L of this section having length L

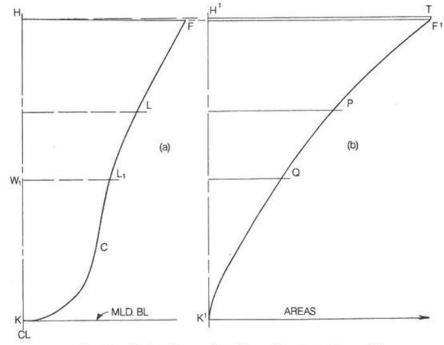
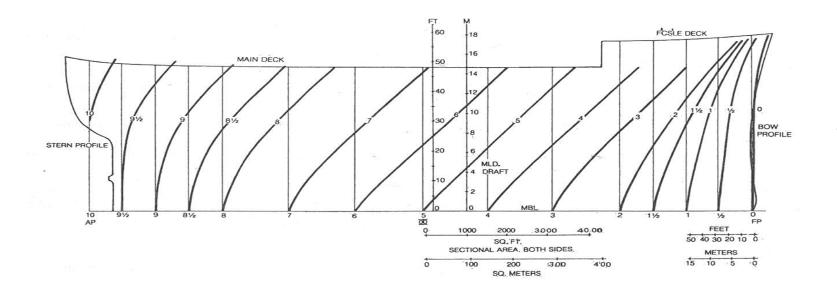


Fig. 32 Body plan section (a) and Bonjean Curve (b)

# Bonjean curves, example



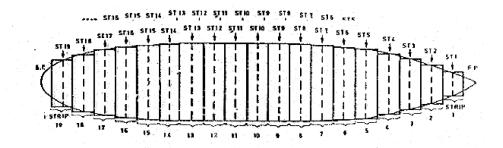
# Strip theory

### A classic method by Korvin-Kroukovsky (1955, 1957) to evaluate the loads on a hull girder in regular waves Assumption:

- The flow in length direction is negligible → the hull can be divided into strips describing 2D phenomena
- Straight hull sides

$$\sum_{k=1}^{6} \left[ \left( M_{jk} + A_{jk} \right) \eta_k + B_{jk} \eta_k + C_{jk} \eta_k \right] = F_j e^{-i\omega t}, j = 1, 2, ..., 6$$

$$\left| H(\omega) \right|^2 = \left[ \frac{Y(\omega)}{A(\omega)} \right]^2$$



## **Summary**

- ☐ Ship Hydrostatics relate with complex hull shapes.
- □ Numerical intergration methods help with the determination of areas, volumes, moments etc. These are used to assess ship characteristics such as:
  - Buoyancy
  - Wetted surface
  - Center of buoyancy
  - ...etc.