

**ELEC-E8116 Model-based control systems**  
**Intermediate exam 2. 12. 12. 2019**

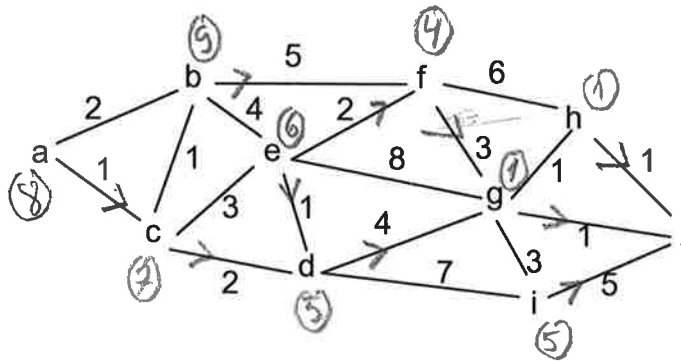
/Solutions

- Write the name of the course, your name, your study program, and student number to each answer sheet.
- There are three (3) problems and each one must be answered.
- No literature is allowed. A function calculator can be used.

Each problem gives the maximum of 5 points.

In the optimal route the controls must be optimal with respect to any state, irrespective of how that state has been reached.

1. a. Explain the concept "Principle of Optimality"  
 b. In the below figure the cost of moving from one node to another is given by the numbers; movement is allowed only from left to right.



For example

$$\begin{aligned}
 J_g^* &= \min\{J_{g+h}, J_{g+i}, J_{g+j}\} \\
 &= \min\{4+1, 1, 3+5\} \\
 &= 1 = J_{g+i} \\
 J_a^* &= 8 \\
 a-c-d-g-i-j
 \end{aligned}$$

Use *dynamic programming* to solve the following problem: Find the minimum cost path from node *a* to the desired final state *j*. (Copy the diagram on your paper and show clearly how you have solved the problem using dynamic programming).

2. For the system

$$\dot{x}(t) = 2u(t)$$

( $x(0) = x_0$ ) calculate the control law, which minimizes the criterion

$$J = \frac{1}{2} \int_0^{\infty} (x^2(\tau) + u^2(\tau)) d\tau$$

What is the optimal cost? What is the closed-loop trajectory of the system? Verify the value of optimal cost by substituting  $x^*(t)$  and  $u^*(t)$  into the integral formula of  $J$  and then calculating its value.

TURN PAPER

3. Consider a SISO-process with the transfer function

$$G(s) = \frac{s + \frac{1}{T_1}}{\left(s + \frac{1}{T_2}\right)\left(s + \frac{1}{T_3}\right)}, \quad T_1 < 0, \quad T_2 < 0, \quad T_3 > 0$$

Explain, what kind of fundamental limitations on control performance can be stated for this system? (Present also some calculations; the formulas in the end of the problems can be of help.)

**Some formulas, which might be useful:**

$$\int_0^{\infty} \log |S(i\omega)| d\omega = \pi \sum_{i=1}^M \operatorname{Re}(p_i)$$

$$|W_T(p_1)| \leq 1 \Rightarrow \omega_0 \geq \frac{p_1}{1 - 1/T_0}$$

$$|W_S(z)| \leq 1 \Rightarrow \omega_0 \leq (1 - 1/S_0)z$$

$$\dot{x} = Ax + Bu$$

$$J(t_0) = \frac{1}{2} x^T(t_f) S(t_f) x(t_f) + \frac{1}{2} \int_{t_0}^{t_f} (x^T Q x + u^T R u) dt$$

$$S(t_f) \geq 0, \quad Q \geq 0, \quad R > 0$$

$$-\dot{S}(t) = A^T S + SA - SBR^{-1}B^T S + Q, \quad t \leq t_f, \quad \text{boundary condition } S(t_f)$$

$$K = R^{-1}B^T S$$

$$u = -Kx$$

$$J^*(t_0) = \frac{1}{2} x^T(t_0) S(t_0) x(t_0)$$

$$2. \quad A=0, B=2, a=a=1$$

$$-\dot{\sigma} = -4\sigma^2 + 1 = 0 \quad \text{because the optimization horizon is infinite}$$

$$\Rightarrow \sigma = \frac{+}{-} \frac{1}{2} = \frac{1}{2} \quad \text{positive definite solution}$$

$$\underline{u^*} = -1 \cdot 2 \cdot \frac{1}{2} x = -x \quad \text{optimal control}$$

$$\dot{X} = -2X, \quad X(0) = X_0$$

$$\Rightarrow X(s) - X_0 = -2X(s) \Rightarrow (s+2)X(s) = X_0 \Rightarrow X(s) = \frac{X_0}{s+2}$$

$$\Rightarrow \underline{X^*(t)} = e^{-2t} X_0 \quad \text{optimal trajectory}$$

$$J^* = \frac{1}{2} X_0^2 \cdot \frac{1}{2} = \frac{1}{4} X_0^2 \quad \text{optimal cost}$$

Verification of the optimal cost

$$\begin{aligned} J^* &= \frac{1}{2} \int_0^{\infty} (e^{-4t} X_0^2 + e^{-4t} X_0^2) dt = X_0^2 \int_0^{\infty} e^{-4t} dt = -\frac{1}{4} X_0^2 \int_0^{\infty} -4e^{-4t} dt \\ &= -\frac{1}{4} X_0^2 \left[ e^{-4t} \right]_0^{\infty} = -\frac{1}{4} X_0^2 (0-1) = \frac{1}{4} X_0^2 \quad \text{ok!} \end{aligned}$$

3.  $T_2 < 0 \Rightarrow$  unstable system (RHP pole)

$T_1 < 0 \Rightarrow$  non-minimum phase system (RHP zero)

Interpolation formulas:

$$p_1 = -\frac{1}{T_2} > 0$$

$$z = -\frac{1}{T_1} > 0$$

"Bandwidth"  $\omega_0 \approx \frac{-\frac{1}{T_2}}{1 - \frac{1}{T_0}} = \frac{1}{\frac{T_2}{T_0} - T_2}$

$$\omega_0 \leq \left(1 - \frac{1}{S_0}\right) \left(-\frac{1}{T_1}\right) = \frac{1}{T_1 S_0} - \frac{1}{T_1}$$

$T_0$  and  $S_0$  are the maximum values of the desired complementary sensitivity and sensitivity functions in the parametrization

$$\frac{1}{W_T} = \frac{1}{\frac{1}{T_0} + \frac{S}{\omega_0}}, \quad \frac{1}{W_S} = \frac{S_0 S}{S + \omega_0 S_0}$$

For any controller  $F_y(s) \rightarrow L(s) \rightarrow S(s)$  the sensitivity function fulfills

$$\int_0^\infty \ln |S(j\omega)| d\omega = -\frac{\pi}{T_2}$$