

Exercise 4- Solution

1- At first, we have to figure out the amount of losses for each one of the switches.

Calculate IGBT Energy per pulse Figure 3 upholds when $V_{ge} = \pm 15$ and $R_g = 3.8 \Omega$, However, voltage is 560 V not 600 V. Using linear scaling for pulse energy $E_{on} = 14 \text{ mJ} * 560 \text{ V} / 600 \text{ V} = 13 \text{ mJ}$

$E_{off} = 21 \text{ mJ} * 560 \text{ V} / 600 \text{ V} = 20 \text{ mJ}$

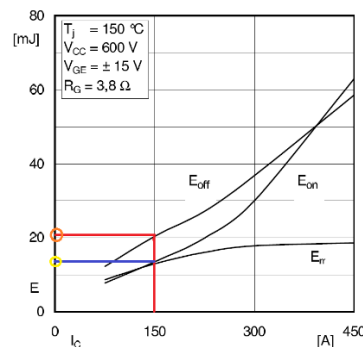


Fig. 3: Typ. turn-on /-off energy = f(Ic)

Conduction losses can be calculated using figure 1 voltage. $U_{ce} = 2.0 \text{ V}$, when $I_c = 150 \text{ A}$, $V_{ge} = 15$ and $T_j = 150 \text{ C}$.

or using numerical values in the datasheet

$$U_{ce} = U_{ce0} + r_{ce} * I_c = 0.98 \text{ V} + 7 \text{ m}\Omega * 150 \text{ A} = 2.03 \text{ V}$$

$$\text{Therefore, } E_{cond} = U_{ce} * I_c * t_{on} = 2.0 \text{ V} * 150 \text{ A} * 0.6 \text{ ms} = 180 \text{ mJ}$$

Switching time $< 1 \text{ us}$ while conduction time is 0.6 ms, therefore we may disregard conducting operation during dead time. IGBT loss power is:

$$P_{IGBT} = f * (E_{on} + E_{off} + E_{cond}) = 1000 \text{ Hz} * (13 \text{ mJ} + 20 \text{ mJ} + 180 \text{ mJ}) = 213 \text{ W}$$

Diode Losses

Also diode reverse recovery causes switching losses, which are also depicted in figure 3. Again lets use linear voltage scaling $E_{rr} = 13 \text{ mJ} * 560 \text{ V} / 600 \text{ V} = 12 \text{ mJ}$.

Voltage for 150 A I_{rr} is given in figure 10. $U_F = 1.9 \text{ V}$, when $T_j = 150 \text{ C}$.

Or numerical values, $U_F = U_{F0} + r_F * I_f = 1.1 \text{ V} + 5.9 \text{ m}\Omega * 150 \text{ A} = 1.99 \text{ V}$

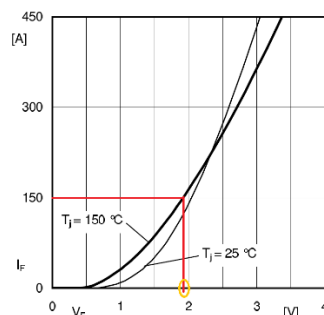
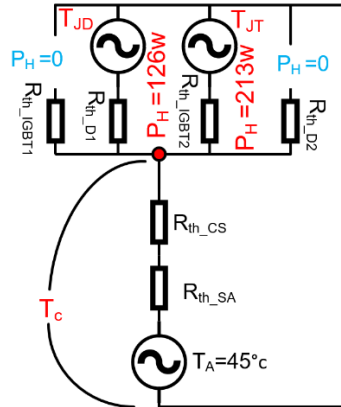


Fig. 10: Typ. CAL diode forward char., incl. R_{cc+EE}

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Therefore conduction energy is $E_{\text{cond}_D} = 1.9 \text{ V} * 150 \text{ A} * 0.4 \text{ ms} = 114 \text{ mJ}$
 and average losses $P_{\text{HD}} = f * (E_{\text{rr}} + E_{\text{cond}_D}) = 1000 \text{ Hz} * (12 \text{ mJ} + 114 \text{ mJ}) = 126 \text{ W}$
 Module thermal equivalent circuit when frequency is 1 kHz, as in. The thermal circuit is constant during switching action.



Maximum thermal resistances for the junction to case and case to sink are given:

$$R_{th_IGBT} = 0.14 \text{ k/W} \quad R_{th_D} = 0.23 \text{ k/W} \quad R_{th_cs} = 0.04 \text{ k/W}$$

Therefore:

$$T_c = (P_{H_IGBT2} + P_{H_D1}) \times (R_{th_cs} + R_{th_SA}) + T_A = (213 + 126) \times (0.04 + 0.08) + 45^\circ\text{C} = 86^\circ\text{C}$$

$$T_{J_IGBT2} = P_{H_IGBT2} \times R_{th_IGBT2} + T_c = 213 \times 0.14 + 86^\circ\text{C} = 116^\circ\text{C}$$

$$T_{J_D1} = P_{H_D1} \times R_{th_D1} + T_c = 126 \times 0.23 + 86^\circ\text{C} = 115^\circ\text{C}$$

- 2- According to the given datasheet, we are not able to find the absolute values of I_{rr} and t_{rr} at the given operating point and we need more detailed data. Nevertheless, we can define a boundary for them by considering the maximum values.

Figure 11 gives the I_{rr} of around 210 A, when Gate resistor is 3,8 Ω .

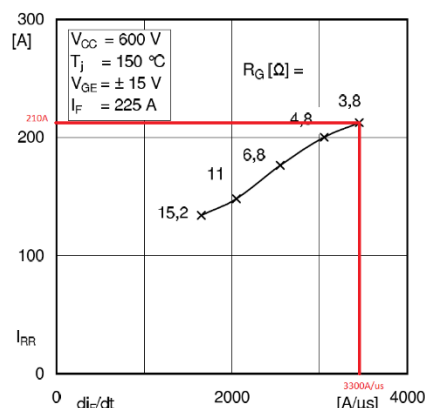


Fig. 11: Typ. CAL diode peak reverse recovery current

Figure 12 gives 3,8 Ω R_G and 150 A I_c , di/dt value of around 3300 A/us

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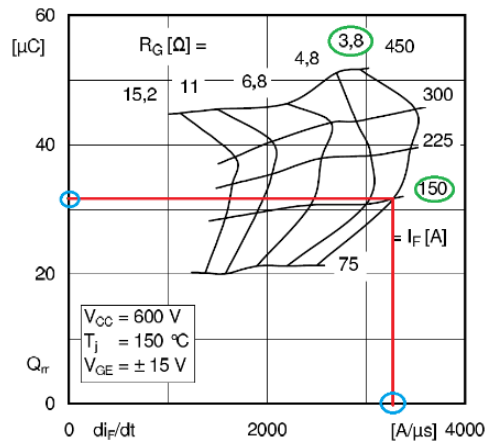


Fig. 12: Typ. CAL diode recovery charge

Reverse recovery equation is $Q_{rr} = I_{rr} * t_{rr} / 2$

then $t_{rr} = 2 * 32 \mu\text{C} / 210 \text{ A} = 0.3 \mu\text{s}$