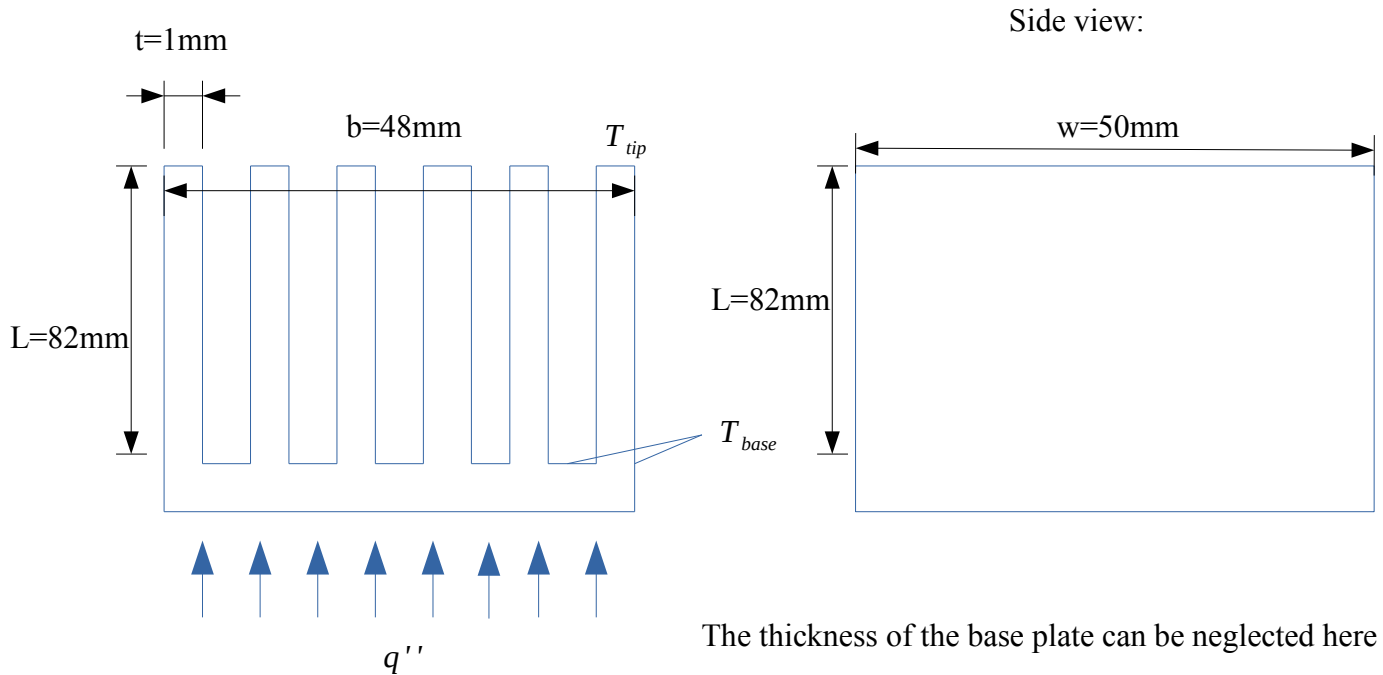


HW2, PP2



We assume a steady state condition, and the convection from the tip may be neglected. Hence, we use adiabatic tip condition. We use the equations in the table:

TABLE 3.4 Temperature distribution and heat loss for fins of uniform cross section

Case	Tip Condition ($x = L$)	Temperature Distribution θ/θ_b	Fin Heat Transfer Rate q_f
A	Convection heat transfer: $h\theta(L) = -k d\theta/dx _{x=L}$	$\frac{\cosh m(L-x) + (h/mk) \sinh m(L-x)}{\cosh mL + (h/mk) \sinh mL} \quad (3.70)$	$M \frac{\sinh mL + (h/mk) \cosh mL}{\cosh mL + (h/mk) \sinh mL} \quad (3.72)$
B	Adiabatic $d\theta/dx _{x=L} = 0$	$\frac{\cosh m(L-x)}{\cosh mL} \quad (3.75)$	$M \tanh mL \quad (3.76)$
C	Prescribed temperature: $\theta(L) = \theta_L$	$\frac{(\theta_L/\theta_b) \sinh mx + \sinh m(L-x)}{\sinh mL} \quad (3.77)$	$M \frac{(\cosh mL - \theta_L/\theta_b)}{\sinh mL} \quad (3.78)$
D	Infinite fin ($L \rightarrow \infty$): $\theta(L) = 0$	$e^{-mx} \quad (3.79)$	$M \quad (3.80)$

$$\theta \equiv T - T_\infty \quad m^2 \equiv hP/kA_c$$

$$\theta_b = \theta(0) = T_b - T_\infty \quad M \equiv \sqrt{hPkA_c}\theta_b$$

Here P is the perimeter of the fin, i.e. $P = 2w + 2t$

The base temperature can be calculated from the heat balance. The heat balance for this system is:

$$q = Nq_f + hA_{gaps}(T_b - T_{inf}) = 24 W$$

The fin efficiency means how much heat is transferred by the fin compared to a situation where the fin would be at the base temperature everywhere, i.e.

$$eff = q_f / (hA_f(T_b - T_{inf}))$$

The fin effectiveness means how much heat is transferred by the fin compared to a situation where there are no extended surfaces, i.e.

$$e = q_f / (hA_{base}(T_b - T_{inf}))$$

The tip temperature is calculated using the equations in the provided table