

2. ENTHALPY AND SPECIFIC HEAT CAPACITY

In this chapter, definition of enthalpy is discussed for a chemically reacting substance, whose thermodynamic state is defined by the equation

$$h = h(T,p) \quad (2.1)$$

at a temperature of T and pressure p . When defining the enthalpy of real gases and real liquid mixtures, the mole amounts of different components have to be taken into account.

Enthalpy according to equation (2.1) is called specific enthalpy, i.e. its dimension is J/mol or J/kg depending on whether considering the mole amount 1 mol or the mass 1 kg. The same notion applies also for thermodynamic quantities, specific volume $v=v(T,p)$, specific internal energy u (J/mol or J/kg), specific entropy s (J/mol K or J/kgK), specific heat capacity at constant pressure c_p (J/mol K or J/kgK) and specific heat capacity in constant volume c_v (J/mol K or J/kgK). Every equation presented after this are exactly the same regardless of choice of molar or mass based specific quantities^{*)}.

2.1 Definitions

Specific heat capacity c_p is defined with the equation

$$c_p \equiv \left(\frac{\partial h}{\partial T} \right)_p. \quad (2.2)$$

Equations (2.1) and (2.2) result in

$$c_p = c_p(T,p). \quad (2.3)$$

Specific volume v is similarly dependent on temperature and pressure

$$v = v(T,p). \quad (2.4)$$

Equation (2.4) is called the equation of state for a substance. Based on the equation of state, the volumetric thermal expansion coefficient γ can be defined as

^{*)} The connection between a molar based specific quantity g_{mol} ($g = u, h, v, s, c_p, c_v, \dots$) and a mass based specific quantity g_{mas} is $g_{\text{mol}} = M g_{\text{mas}}$, where M is the molar mass of the substance (kg/mol).

$$\gamma \equiv \frac{1}{v} \left(\frac{\partial v}{\partial T} \right)_p \quad (2.5)$$

and the isothermal compressibility factor κ_T as

$$\kappa_T \equiv -\frac{1}{v} \left(\frac{\partial v}{\partial p} \right)_T. \quad (2.6)$$

Note that $\gamma = \gamma(T, p)$ and $\kappa_T = \kappa_T(T, p)$.

Example 2.1. The specific molar volume of an ideal gas is

$$v = \frac{V}{n}.$$

Inserting the ideal gas law $pV=nRT$ to this results in

$$v = v(T, p) = \frac{RT}{p},$$

where it can be seen that the specific molar volume of an ideal gas is the same for every gas.

For an ideal gas, the equation (2.5) results in

$$\gamma = \frac{1}{v} \frac{\partial v}{\partial T} = \frac{1}{v} \frac{R}{p} = \frac{1}{v} \frac{1}{T} \frac{RT}{p} = \frac{1}{v} \frac{1}{T} v = \frac{1}{T}$$

and accordingly, for an ideal gas, the equation (2.6) results in

$$\kappa_T = -\frac{1}{v} \frac{\partial v}{\partial p} = -\frac{1}{v} \frac{-RT}{p^2} = \frac{1}{v} \frac{1}{p} \frac{RT}{p} = \frac{1}{p}.$$

For enthalpy change with respect to pressure, an equation can be derived [2]

$$\frac{\partial h}{\partial p} = v - T \left(\frac{\partial v}{\partial T} \right)_p, \quad (2.7)$$

which can be written with the volumetric thermal expansion coefficient equation (2.5) as

$$\frac{\partial h}{\partial p} = v(1 - T\gamma). \quad (2.8)$$

The following applies for the total differential of enthalpy $h=h(T,p)$

$$dh = \frac{\partial h}{\partial T} dT + \frac{\partial h}{\partial p} dp,$$

with equations (2.2) and (2.8) this becomes

$$dh = c_p dT + v(1 - T\gamma)dp. \quad (2.9)$$

Integrating equation (2.9) results in

$$\begin{aligned} h(T, p) - h(T_o, p_o) &= \\ &= \int_{T_o}^T c_p(T, p_o) dT + \int_{p_o}^p v(T, p)(1 - T\gamma(T, p)) dp \end{aligned} \quad (2.10)$$

In order to calculate enthalpy changes compared to a known state (T_o, p_o) , the function $c_p(T, p_o)$ has to be known, which is the specific heat capacity as a function of temperature at pressure p_o , as well as the equation of state (2.4), which results in the volumetric thermal expansion coefficient $\gamma(T, p)$ by applying the equation (2.5).

Example 2.2. For an ideal gas $\gamma(T, p) = 1/T$ and the equation (2.8) results in $(\partial h / \partial p)_T = 0$, meaning that

$$h(T, p) = h(T).$$

Generally, gases are closer to an ideal gas the lower the pressure p is. For example, air at a pressure of 1 bar can be considered as an ideal gas with reasonable accuracy, but at higher pressures the deviation becomes significant.

2.2 Reaction enthalpy

Enthalpy change

$$\Delta H \equiv H(B) - H(A) \quad (2.11)$$

from state $A = (T, p, n_1, n_2, \dots, n_m)$ to state $B = (T, p, n'_1, n'_2, \dots, n'_m)$ is called reaction enthalpy, when temperatures and pressures are equal in the initial state (A) and the final state (B).

When the reaction enthalpy $\Delta H < 0$, the reaction is exothermic, and heat is released. If $\Delta H > 0$, the reaction is endothermic, and heat is absorbed. If the reaction takes place in a thermally insulated container, an endothermic reaction lowers the temperature and an exothermic reaction increases it.

Example 2.3. Let's consider the combustion reaction of carbon



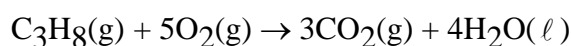
At the initial state of the process A the reactants carbon C(s) and oxygen O₂(g) are not yet reacting. At the final state of the process B carbon and oxygen have reacted and formed carbon dioxide.

When the initial and final states of the combustion reaction are at the standard state $T = 298.15 \text{ K}$ and $p = 1.0 \text{ bar}$, the reaction enthalpy becomes

$$\Delta H = \Delta H^\circ = H(\text{B}) - H(\text{A}) = - 393.5 \text{ kJ/mol},$$

where mole corresponds to the number of gross reactions according to the combustion reaction equation, which in this case is the same as the amount of carbon C(s) or oxygen O₂(g) consumed or carbon dioxide CO₂(g) formed during the reaction in moles. Therefore, the number of these written reactions occurring is equal to one mole, i.e. the Avogadro number $6.023 \cdot 10^{23}$ *). The enthalpy at the initial state is $H(\text{A}) = H(\text{C(s)}) + H(\text{O}_2(\text{g}))$ and at the final state $H(\text{B}) = H(\text{CO}_2(\text{g}))$. The notation ΔH° means that the reaction enthalpy is defined at the standard state.

Example 2.4. The gross reaction of combustion of propane gas is



and the stated reaction enthalpy at the standard state is $\Delta H^\circ(298.15\text{K}) = - 2220 \text{ kJ/mol}$. The mole corresponds to the number of gross reactions according to the equation above, which in this case is equal to the amount of combusted propane gas C₃H₈(g) in moles.

*) A mole is equal to the Avogadro number, i.e. $1 \text{ mol} \equiv 6.023 \cdot 10^{23}$. It is therefore an abbreviation quantity similar to for example million.

2.3 Enthalpy of formation

The combustion reaction of carbon $C(s) + O_2(g) \rightarrow CO_2(g)$ is an example of a formation reaction for carbon dioxide. Enthalpy of formation of a chemical compound ΔH_f° is the enthalpy change between the compound at the standard state and its reference state, where its elements are in a stable form. The enthalpy of formation is dependent on temperature: $\Delta H_f^\circ(T)$. The lower index f denotes the word formation. For example, the enthalpy of formation of liquid water at the standard state (table 2.1) at a temperature of 25 °C is $\Delta H_f^\circ(l; 298.15 \text{ K}) = -285.830 \text{ kJ/mol}$ and accordingly, the enthalpy of formation of water vapor at the same temperature is $\Delta H_f^\circ(g; 298.15 \text{ K}) = -241.826 \text{ kJ/mol}$ (table 2.1 or table 1.1). According to the definition, the enthalpy of formation at the reference state is zero, for example $\Delta H_f^\circ(O_2(g)) = 0$.

The enthalpy of formation of a compound depicts the total amount of energy absorbed or released to the environment by a process occurring at constant temperature and pressure. If ΔH_f° is positive, energy is required to form the compound.

Table 2.1. Enthalpies of formation for a selection of substances [3] at the standard state ($p = 100 \text{ kPa}$) at a temperature of $T = 298.15 \text{ K}$.

	ΔH_f° (MJ/kmol)		ΔH_f° (MJ/kmol)
$CO_2(g)$	-393.505	$SO_2(g)$	-296.813
$CO(g)$	-110.541	$SO_3(g)$	-395.765
$H_2O(g)$	-241.826	$NO(g)$	90.291
$H_2O(l)$	-285.830	$NO_2(g)$	33.095
$CH_4(g)$	-74.873	$N_2O(g)$	82.048
$C_2H_6(g)$	-84.684	$NH_3(g)$	-45.940
$C_3H_8(g)$	-103.847	$HCN(g)$	-135.143
$C_4H_{10}(g)$	-126.148	CaO	-635.089
$H_2S(g)$	-20.502	$CaCO_3(\text{calcite})$	-1206.921
$COS(g)$	-138.407	$Ca(OH)_2$	-986.085

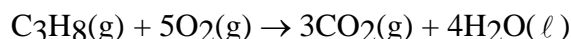
The enthalpy $h(T,p)$ (J/mol) of gases, pure solid substance and pure liquid at the standard state is denoted as $h^\circ(T)$ [often in tables as $H^\circ(T)$]. Its value at the starting point of an enthalpy scale ($T_o, p_o = p^\circ$) is defined as the value of enthalpy of formation

$$h^\circ(T_o) \equiv h(T_o, p_o) \equiv \Delta H_f^\circ(T_o). \quad (2.13)$$

When using the enthalpy scale agreement 1° presented in section 1.3, a common agreement is that $T_o = 298.15 \text{ K}$.

The deeper meaning of equation (2.13) is that by using enthalpies of formation the composing of impossible absolute internal energy and enthalpy scales can be avoided. This is proven in the following example where the reaction enthalpy of the combustion of propane gas is defined with the enthalpies of formation. In other words, the example shows why enthalpies based on the definition (2.13) yield correct values of enthalpies of reaction.

Example 2.5. For the reaction



the reaction enthalpy at the standard state at a temperature of T according to the definition is

$$\Delta H^\circ = [3h^\circ(\text{CO}_2(\text{g})) + 4h^\circ(\text{H}_2\text{O}(\ell))] - [h^\circ(\text{C}_3\text{H}_8(\text{g})) + 5h^\circ(\text{O}_2(\text{g}))],$$

where quantities $h^\circ(\text{CO}_2(\text{g}))$, ..., $h^\circ(\text{O}_2(\text{g}))$ depict the enthalpies of the components at the standard state expressed with a physically correct common energy scale. We can assume that such scale exists or that at least in principle such a scale can be composed.

The expression of reaction enthalpy can be written in the following equivalent form

$$\begin{aligned} \Delta H^\circ = & [3\{h^\circ(\text{CO}_2(\text{g})) - h^\circ(\text{C}(\text{s})) - h^\circ(\text{O}_2(\text{g}))\} + 4\{h^\circ(\text{H}_2\text{O}(\ell)) - \\ & h^\circ(\text{H}_2(\text{g})) - 1/2 h^\circ(\text{O}_2(\text{g}))\}] - [\{h^\circ(\text{C}_3\text{H}_8(\text{g})) - 3h^\circ(\text{C}(\text{s})) - \\ & 4h^\circ(\text{H}_2(\text{g}))\} + 5\{h^\circ(\text{O}_2(\text{g})) - h^\circ(\text{O}_2(\text{g}))\}], \end{aligned}$$

since the enthalpy terms $h^\circ(\text{C}(\text{s}))$, $h^\circ(\text{O}_2(\text{g}))$ ja $h^\circ(\text{H}_2(\text{g}))$ of the elements present in the equation balance each other out. On the other hand, the expressions in round brackets in the equation are exactly the same as the enthalpies of formation of the compounds:

$$\begin{aligned} \Delta H_f^\circ(\text{CO}_2(\text{g})) &= h^\circ(\text{CO}_2(\text{g})) - h^\circ(\text{C}(\text{s})) - h^\circ(\text{O}_2(\text{g})) \\ \Delta H_f^\circ(\text{H}_2\text{O}(\ell)) &= h^\circ(\text{H}_2\text{O}(\ell)) - h^\circ(\text{H}_2(\text{g})) - 1/2 h^\circ(\text{O}_2(\text{g})) \\ \Delta H_f^\circ(\text{C}_3\text{H}_8(\text{g})) &= h^\circ(\text{C}_3\text{H}_8(\text{g})) - 3h^\circ(\text{C}(\text{s})) - 4h^\circ(\text{H}_2(\text{g})) \\ \Delta H_f^\circ(\text{O}_2(\text{g})) &= h^\circ(\text{O}_2(\text{g})) - h^\circ(\text{O}_2(\text{g})). \end{aligned}$$

When both the reactants and the products are at the standard state at a temperature of T, the equation can be written as

$$\Delta H^{\circ} = 3 \Delta H_f^{\circ}(\text{CO}_2(\text{g})) + 4 \Delta H_f^{\circ}(\text{H}_2\text{O}(\text{l})) - \Delta H_f^{\circ}(\text{C}_3\text{H}_8(\text{g})) - 5 \Delta H_f^{\circ}(\text{O}_2(\text{g}))$$

and with enthalpies according to the enthalpy scale agreement 2° ($T_0=T$) and the definition (2.13), $\Delta H^{\circ} = 3 h^{\circ}[\text{CO}_2(\text{g})] + 4 h^{\circ}[\text{H}_2\text{O}(\text{l})] - h^{\circ}[\text{C}_3\text{H}_8(\text{g})] - 5 h^{\circ}[\text{O}_2(\text{g})]$, which proves the usefulness of the definition (2.13).

Was it a pure coincidence that the decomposition done in the example, which was used to form enthalpies of formation in the round brackets, is identical with the reaction equation? No. By decomposing the elements of each compound it can be always shown that the element terms cancel each other since there is an equal amount of moles on both sides of the reaction equation. This is a direct result of the element balance. A reaction equation is one way to represent element balance. When the enthalpies of the elements according to the mole amounts are reduced from the enthalpy terms, they cancel each other when calculating the enthalpy difference between the initial and final states according to the element balance, given that the temperatures are the same. This procedure is therefore universal when calculating the reaction enthalpy.

Example 2.6. Let's calculate the reaction enthalpy of the combustion reaction of propane gas $\text{C}_3\text{H}_8(\text{g}) + 5\text{O}_2(\text{g}) \rightarrow 3\text{CO}_2(\text{g}) + 4\text{H}_2\text{O}(\ell)$ at $T=T_0 = 298.15 \text{ K}$ using the enthalpies of formation:

$$\text{C}_3\text{H}_8(\text{g}; 298.15 \text{ K}), \Delta H_f^{\circ} = - 103.8 \text{ kJ/mol}$$

$$\text{O}_2(\text{g}; 298.15 \text{ K}), \Delta H_f^{\circ} = 0$$

$$\text{CO}_2(\text{g}; 298.15 \text{ K}), \Delta H_f^{\circ} = - 393.5 \text{ kJ/mol}$$

$$\text{H}_2\text{O}(\ell ; 298.15 \text{ K}), \Delta H_f^{\circ} = - 285.8 \text{ kJ/mol}$$

and therefore

$$\begin{aligned} \Delta H^{\circ}(298.15 \text{ K}) &= [3(- 393.5) + 4(- 285.8)] - [1(- 103.8) + 5 \cdot 0] = \\ &= - 2220 \text{ kJ/mol}. \end{aligned}$$

When analyzing reactions where the temperatures at the initial and final states are not equal, the enthalpies of the compounds at different temperatures are needed. In this case, the enthalpy difference between reactants and products cannot be calculated as in examples 2.5-2.6 (enthalpy scale agreement 2°, section 1.3) only based on the

enthalpies of formation, even if they are known at different temperatures. In the next section, defining enthalpies according to the enthalpy scale agreement 1° is discussed.

2.4 Enthalpy scale agreement 1° for a chemically reacting compound

2.4.1 Temperature dependence of enthalpy and specific heat capacity

If the enthalpy of formation and specific heat capacity are known, the enthalpy at the standard state at a given temperature can be written according to equations (2.10) and (2.13) as

$$h(T, p^\circ) = h^\circ(T) = \Delta H_f^\circ(T_0) + \int_{T_0}^T c_p^\circ(T) dT \quad (2.14)$$

where a notation $c_p(T, p^\circ) = c_p^\circ(T)$ is used. The equation (2.14) follows the enthalpy agreement 1° presented in section 1.3, according to which the starting point of the enthalpy scale is set at a temperature of T_0 and at the starting point of the scale $h^\circ(T_0) = \Delta H_f^\circ(T_0)$.

In tables the integral term is often already calculated in the form

$$h^\circ(T) - h^\circ(T_0) \equiv \int_{T_0}^T c_p^\circ(T) dT,$$

which results in

$$h^\circ(T) = \Delta H_f^\circ(T_0) + [h^\circ(T) - h^\circ(T_0)]. \quad (2.15)$$

The term $[h^\circ(T) - h^\circ(T_0)]$ is called *sensible enthalpy* or *table enthalpy*. In chapter 12, where combustion is discussed, the table enthalpies of important gases related to combustion are presented.

In the case of a phase change from phase I to phase II at a temperature of T_{tr} , for example the liquification of a substance, the enthalpy change taking place during the phase change ΔH_{tr}° has to be added to equation (2.14):

$$h(T, p^\circ) = \Delta H_f^\circ(T_0) + \underbrace{\int_{T_0}^{T_{tr}} c_{p,I}^\circ(T) dT}_{\substack{\text{temperature rise} \\ \text{of phase I } T_0 \rightarrow T_{tr}}} + \underbrace{\Delta H_{tr}^\circ(T_{tr})}_{\substack{\text{phase change} \\ \text{between phases} \\ \text{I and II}}} + \underbrace{\int_{T_{tr}}^T c_{p,II}^\circ(T) dT}_{\substack{\text{temperature rise} \\ \text{of phase II } T_{tr} \rightarrow T}} \quad (2.16)$$

Example 2.7. Aluminum oxide (α - Al_2O_3 , crystal (delta)) is a heat resistant ceramic substance. Calculate its enthalpy at temperatures of 273.15 K and 1000 K.

The reference state of the compound is crystalline aluminum metal $\text{Al}(\text{cr})$ and oxygen gas $\text{O}_2(\text{g})$. From table 2.2 we can see at a temperature of $T_0 = 298.15\text{K}$ (in Janaf tables T_0 is denoted with the symbol T_r)

$$\Delta H^\circ_f(T_0) = -1666.487 \text{ kJ/mol.}$$

At a temperature of $T_0 = 298.15 \text{ K}$ the specific heat capacity of aluminum oxide is

$$c_p(T_0) = 81.385 \text{ J mol}^{-1} \text{ K}^{-1}.$$

The enthalpy of aluminum oxide at a temperature of 273.15 K is according to equation (2.14)

$$\begin{aligned} h(T=273.15 \text{ K}, p^\circ) &= -1666.487 + 81.385 \cdot 10^{-3} \cdot (273.15-298.15) \\ &= -1668.522 \text{ kJ/mol.} \end{aligned}$$

Specific heat capacity c_p is highly dependent on the temperature. For example, for aluminum oxide at a temperature of 600 K it is $c_p = 115.92 \text{ J mol}^{-1} \text{ K}^{-1}$. Therefore, the enthalpy at 1000 K is best defined with a beforehand calculated tabulated integral based on equation (2.15). From the table we can easily see that

$$h^\circ(1000 \text{ K}) - h^\circ(T_0) = 80.304 \text{ kJ/mol } (T_0 = 298.15 \text{ K})$$

and with equation (2.15) the enthalpy is

$$h(T = 1000 \text{ K}, p^\circ) = -1666.487 + 80.304 = -1586.183 \text{ kJ/mol.}$$

Enthalpy per unit mass is accordingly

$$h(T = 1000 \text{ K}, p^\circ) = -1586.183/0.10196 = -15.56 \text{ MJ/kg,}$$

where $M_{\text{Al}_2\text{O}_3} = 0.10196 \text{ kg/mol}$.

Specific heat capacities c_p of gases at different temperatures are presented in table 2.3. For monatomic gases, so called noble gases, the specific heat capacity is independent on the temperature. For example, for argon gas $c_p = 20.786 \text{ J/(molK)}$.

In table 2.4 standard enthalpy values $h^\circ(T)$ of gases at different temperatures based on the equation (2.14) are presented. When calculating the integral expression, the

Table 2.2. Aluminum oxide (α-Al₂O₃, crystal (delta)).

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Aluminum Oxide, Delta (Al₂O₃)

T/K	C _p ^o	S ^o - J K ⁻¹ mol ⁻¹	H ^o - H ^o (T)/T	Δ _f H ^o	Δ _f G ^o	Log K _f
100	0					
200	81.385	50.626	0.	-1686.487	-1572.974	275.579
298.15	81.799	51.131	0.151	-1686.507	-1572.394	273.778
400	84.968	77.231	54.070	-1686.867	-1540.932	201.225
500	108.315	100.518	61.079	-1687.719	-1509.504	157.697
600	115.922	121.073	69.400	-1685.192	-1478.248	128.693
700	123.738	135.809	76.795	-1680.689	-1456.311	104.476
800	129.342	143.764	82.251	-1675.571	-1385.582	80.417
1000	144.514	183.764	103.460	-1661.850	-1355.447	70.697
1100	130.406	196.103	111.329	-1660.516	-1320.670	62.713
1200	136.630	206.155	118.108	-1660.255	-1285.486	56.446
1300	135.013	216.155	126.108	-1677.500	-1255.486	50.946
1400	136.013	228.113	133.042	-1675.837	-1223.086	45.634
1500	136.258	237.471	139.698	-1674.664	-1190.819	41.468
1600	137.382	246.301	146.085	-1673.253	-1158.660	37.826
1700	138.197	254.658	152.248	-1672.535	-1126.690	34.547
1800	138.973	262.537	158.288	-1672.212	-1094.900	31.597
1900	139.706	270.137	163.838	-1672.000	-1063.272	28.920
2000	140.706	277.336	169.335	-1671.962	-1031.160	26.831
2100	141.438	284.218	174.643	-1672.283	-999.550	24.862
2200	142.171	290.815	179.774	-1672.888	-968.056	22.994
2300	142.898	297.162	184.766	-1673.712	-937.092	21.304
2400	143.636	303.248	189.652	-1674.770	-906.932	19.704
2500	144.412	309.128	194.219	-1676.000	-877.087	18.263
2600	145.188	314.806	198.748	-1677.425	-847.963	16.935
2700	146.007	320.301	203.148	-1679.050	-819.007	15.707
2800	146.818	325.597	207.429	-1680.875	-790.768	14.597
2900	147.618	330.797	211.594	-1682.900	-763.718	13.597
3000	148.408	335.824	215.651	-1685.125	-737.364	11.759

Aluminum Oxide, Delta (Al₂O₃)

Aluminum Oxide, Delta (Al₂O₃)

CRYSTAL (DELTA)

M_r = 101.96128

Δ_fH^o(0 K) = [-1683.9 ± 4] kJ mol⁻¹

Δ_fH^o(298.15 K) = [-1686.5 ± 4] kJ mol⁻¹

Δ_fG^o(298.15 K) = [-1686.5 ± 4] kJ mol⁻¹

T_{fus} = [93.3] kJ mol⁻¹

Enthalpy of Formation

Δ_fH^o is calculated from that of α-Al₂O₃ (1) using Δ_hH^o(978 K) = -2.720.4 kcal mol⁻¹ for the irreversible process $\delta-\alpha$. This yields Δ_fH^o(298.15 K) = -2.3 kcal mol⁻¹ based on our adopted functions. Yokokawa and Kleppa (2) determined Δ_fH^o for the two crystalline forms from their heats of solution in an oxide melt at 978 K. DTA studies by Gani and McPherson (3) gave Δ_fH^o = -2.850.5 kcal mol⁻¹. Assuming T = -1600 K, we derive Δ_fH^o(298.15 K) = -1.9 kcal mol⁻¹. This confirms the calorimetric result. Both samples of δ-Al₂O₃ had been obtained by rapid quenching from high temperature, one (2) from combustion of Al₂O₃ and the other (3) by a plasma method.

Heat Capacity and Entropy

C_p is assumed to be 3% larger than that of α-Al₂O₃ (1) by comparison with the observed values for ε-Al₂O₃ (1) and the adopted values for γ-Al₂O₃ (1). S^o is selected such that Δ_fG^o(ε-δ) < 0 below T_{fus} and Δ_fG^o(ε-α) < 0 at T₂₄₀₀ K. Marchand et al. (4) measured enthalpy data (573-1177 K) for a sample designated only as TΔ-600 alumina. They attributed a transition at -993 K (720°C) to the irreversible process α→δ. This temperature corresponds roughly to processes designated as either (γ or η)→δ by Lippens and Steggoda (5). DTA data of Alevra et al. (6) showed an endotherm near 750°C subsequent to the dehydration of hydroxide samples; however, TGA data indicated that the resulting alumina still retained considerable water at this temperature. The enthalpy data (4), 1003-1177 K are 4.7±0.3% larger than those of α-Al₂O₃ (1) and presumably correspond to an alumina containing a significant amount of water. The δ-Al₂O₃ used in Δ_fH^o studies was presumably essentially anhydrous. Thus, we omit the enthalpy data (4) on the presumption that they are larger than those of our standard state which is anhydrous ε-Al₂O₃.

Phase Data

The stable crystalline form is corundum (α-alumina). Delta-alumina is one of several structurally related, metastable forms. These occur in "active alumina" and are much studied (5) due to their importance in adsorbents and catalysts. Lippens and Steggoda (5) summarized the classifications of metastable forms, their crystal structures and conditions of formation by dehydration. Mixtures of the closely related ε- and δ-aluminas are also formed by rapid cooling of droplets of molten alumina following their passage through a flame (7). There is some controversy (5) over the X-ray data and unit-cell dimensions of ε-Al₂O₃ formed by the two methods. Recent data (8) for ε-Al₂O₃ (5) suggest a similar controversy. Delta-alumina belongs to the "nearly anhydrous", high-temperature classification (5) based on the temperature of 600° to 900°C at which it forms during dehydration. The irreversible transition ε-δ(ε)→ε are thermally activated at temperatures of 800°-1050°C for the first step (5, 6) and ~1200°C for the final step (5).

Fusion Data

The hypothetical melting point of metastable δ-phase is calculated as the temperature at which Δ_fG^o(ε-δ)=0. Δ_{fus}H^o is the corresponding difference in Δ_fH^o.

- References
- JANAF Thermochemical Tables: Al₂O₃(cr, α), Al₂O₃(cr, ε), and Al₂O₃(cr, γ), 12-31-79.
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temperature dependence is taken into account with a power series according to the database of the HSC software. The starting point of the enthalpy scale in table 2.4 is $T_0 = 298.15$ K.

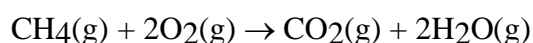
The standard state of gases is defined according to the ideal gas state. Since the enthalpy of an ideal gas is not dependent on the pressure or the composition of the gas mixture, tabulated values of h° (H° in Janaf tables) correspond to values of enthalpy of ideal gases at any pressure other than the standard pressure p° . The enthalpy of an ideal gas is also not dependent on the mole amounts in the mixture and therefore values of h° can be used for the components of an ideal gas mixture.

These enthalpies are very convenient in calculations since they include the energy changes associated with reactions.

Table 2.3. Specific heat capacities c_p of gases.

T C	T K	J/(mol*K)													
		CH4	C2H6	C3H8	C4H10	H2	CO	N2	Ar	O2	CO2	H2S	H2O	COS	NH3
25	298.15	34.96	52.39	73.46	98.25	28.88	29.11	29.11	20.78	29.15	37.46	34.17	33.56	41.71	35.54
26.85	300	35.07	52.87	74.19	98.83	28.88	29.11	29.11	20.78	29.17	37.53	34.19	33.57	41.79	35.60
76.85	350	38.10	63.85	90.77	113.34	29.03	29.22	29.15	20.78	29.75	39.40	34.86	33.92	43.75	37.27
126.85	400	41.09	72.17	103.17	126.15	29.13	29.39	29.25	20.78	30.30	41.14	35.60	34.31	45.53	38.93
176.85	450	44.03	78.91	113.10	137.82	29.20	29.61	29.41	20.78	30.81	42.77	36.39	34.76	47.14	40.57
226.85	500	46.91	84.65	121.44	148.63	29.26	29.88	29.62	20.78	31.29	44.28	37.23	35.25	48.60	42.18
276.85	550	49.72	89.70	128.72	158.75	29.31	30.17	29.87	20.78	31.75	45.68	38.09	35.77	49.92	43.76
326.85	600	52.47	94.27	135.24	168.29	29.36	30.49	30.15	20.78	32.17	46.98	38.97	36.32	51.11	45.32
376.85	650	55.14	98.46	141.19	177.29	29.41	30.82	30.45	20.78	32.57	48.19	39.87	36.90	52.18	46.84
426.85	700	57.72	102.37	146.69	185.80	29.48	31.16	30.76	20.78	32.95	49.31	40.76	37.49	53.14	48.33
476.85	750	60.23	106.04	151.84	193.85	29.56	31.50	31.08	20.78	33.30	50.34	41.64	38.11	54.00	49.78
526.85	800	62.64	109.52	156.69	201.46	29.65	31.85	31.40	20.78	33.63	51.29	42.50	38.73	54.77	51.19
576.85	850	64.97	112.83	161.29	208.64	29.76	32.18	31.72	20.78	33.94	52.17	43.35	39.36	55.47	52.57
626.85	900	67.20	115.99	165.67	215.40	29.89	32.51	32.04	20.78	34.22	52.97	44.17	40.00	56.09	53.90
676.85	950	69.34	119.02	169.84	221.75	30.04	32.83	32.35	20.78	34.50	53.71	44.97	40.64	56.65	55.19
726.85	1000	71.38	121.93	173.84	227.69	30.20	33.13	32.65	20.78	34.75	54.38	45.73	41.27	57.14	56.44
776.85	1050	73.33	124.72	177.67	233.24	30.37	33.42	32.94	20.78	34.99	55.00	46.46	41.90	57.59	57.65
826.85	1100	75.18	127.41	181.34	238.39	30.56	33.69	33.21	20.78	35.21	55.56	47.16	42.53	58.00	58.81
876.85	1150	76.94	129.99	184.86	243.14	30.76	33.94	33.48	20.78	35.42	56.08	47.82	43.14	58.36	59.93
926.85	1200	78.61	132.48	188.24	247.50	30.96	34.18	33.72	20.78	35.62	56.54	48.45	43.75	58.69	61.01
976.85	1250	80.18	134.87	191.48	251.46	31.18	34.40	33.95	20.78	35.80	56.97	49.05	44.34	58.99	62.04
1026.85	1300	81.66	137.17	194.60	255.04	31.40	34.61	34.17	20.78	35.98	57.35	49.61	44.92	59.26	63.03
1076.85	1350	83.06	139.38	197.58	258.23	31.62	34.79	34.37	20.78	36.15	57.70	50.13	45.48	59.51	63.98
1126.85	1400	84.36	141.51	200.43	261.04	31.85	34.97	34.55	20.78	36.30	58.02	50.62	46.03	59.74	64.89

Example 2.8. The combustion reaction of methane is



and its reaction enthalpy can be determined directly from table 2.4. Let's calculate its value at $T_0 = 298.15$ K according to table 2.4:

$$\begin{aligned} \Delta H^\circ &= h^\circ[\text{CO}_2] + 2h^\circ[\text{H}_2\text{O}] - h^\circ[\text{CH}_4] - 2h^\circ[\text{O}_2] \\ &= -393.51 + 2 \cdot (-241.83) - (-74.87) - 2 \cdot 0 \end{aligned}$$

Table 2.4. Values of standard enthalpy $h^{\circ}(T)$ (kJ/mol) for different gases. Source: HSC.

T K	CH ₄ metaani	C ₂ H ₆ etaani	C ₃ H ₈ propaani	C ₃ H ₈ propeeni	C ₄ H ₁₀ n-butaani	C ₄ H ₁₀ iso- butaani	C ₄ H ₁₀ 2-metyyli- propaani	CH ₃ OH metanoli	H ₂ vety	CO hiili- monoksidi	CO ₂ hiili- dioksidi
298.15	-74.87	-84.68	-103.93	-103.85	-126.15	-134.61	-134.73	-201.87	0.00	-110.54	-393.51
300	-74.81	-84.59	-103.79	-103.71	-125.97	-134.43	-134.55	-201.79	0.05	-110.49	-393.44
350	-72.97	-81.77	-99.80	-99.72	-120.70	-129.17	-129.69	-199.50	1.51	-109.02	-391.51
400	-70.98	-78.63	-95.29	-95.19	-114.80	-123.24	-124.82	-197.02	2.96	-107.55	-389.45
450	-68.85	-75.16	-90.30	-90.18	-108.30	-116.68	-119.96	-194.34	4.42	-106.08	-387.28
500	-66.58	-71.40	-84.86	-84.73	-101.22	-109.55	-115.10	-191.47	5.88	-104.59	-385.03
550	-64.16	-67.35	-78.99	-78.86	-93.60	-101.86	-110.23	-188.40	7.34	-103.08	-382.72
600	-61.61	-63.02	-72.72	-72.60	-85.46	-93.65	-105.37	-185.14	8.81	-101.57	-380.35
650	-58.93	-58.44	-66.08	-65.97	-76.83	-84.96	-100.51	-181.71	10.27	-100.04	-377.93
700	-56.11	-53.61	-59.08	-58.99	-67.74	-75.81	-95.64	-178.11	11.74	-98.50	-375.46
750	-53.17	-48.54	-51.75	-51.69	-58.22	-66.24	-90.78	-174.34	13.22	-96.94	-372.96
800	-50.10	-43.25	-44.11	-44.07	-48.30	-56.27	-85.91	-170.42	14.70	-95.37	-370.41
850	-46.92	-37.74	-36.18	-36.16	-38.01	-45.94	-81.05	-166.37	16.19	-93.78	-367.84
900	-43.62	-32.04	-27.98	-27.98	-27.38	-35.27	-76.19	-162.18	17.68	-92.19	-365.23
950	-40.22	-26.16	-19.54	-19.55	-16.44	-24.29	-71.32	-157.87	19.18	-90.57	-362.58
1000	-36.70	-20.10	-10.86	-10.87	-5.21	-13.03	-66.46	-153.45	20.69	-88.95	-359.91
1050	-33.09	-13.87	-1.98	-1.98	6.27	-1.52	-61.60	-148.94	22.21	-87.31	-357.22
1100	-29.38	-7.50	7.09	7.12	17.98	10.20	-56.73	-144.33	23.73	-85.66	-354.49
1150	-25.58	-0.99	16.32	16.41	29.88	22.12	-51.87	-139.65	25.26	-84.00	-351.74
1200	-21.69	5.64	25.70	25.87	41.94	34.21	-47.01	-134.90	26.81	-82.33	-348.97
1250	-17.71	12.39	35.20	35.48	54.15	46.42	-42.14	-130.09	28.36	-80.64	-346.17
1300	-13.66	19.24	44.81	45.23	66.45	58.75	-37.28	-125.24	29.92	-78.94	-343.35
1350	-9.53	26.18	54.50	55.10	78.84	71.15	-32.42	-120.36	31.50	-77.24	-340.51
1400	-5.34	33.20	64.26	65.07	91.28	83.59	-27.55	-115.45	33.08	-75.52	-337.65
1450	-1.08	40.28	74.06	75.13	103.73	96.06	-22.69	-110.53	34.67	-73.79	-334.78
1500	3.25	47.41	83.88	85.26	116.17	108.52	-17.83	-105.61	36.28	-72.05	-331.88

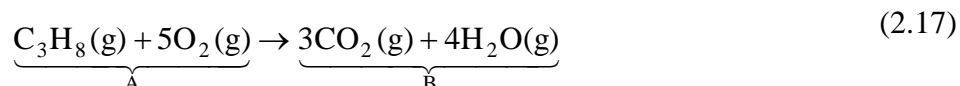
Table 2.4 (continued).

T K	N ₂ typpi	O ₂ happi	Ar argon	H ₂ S rikkivety	H ₂ O vesi	COS karbonyyli- sulfidi	HCN vety- syanidi	NH ₃ ammoni- akki	NO typpi- monoksidi	NO ₂ typpi- dioksidi	SO ₂ rikki- dioksidi	SO ₃ rikki- trioksidi
298.15	0.00	0.00	0.00	-20.50	-241.83	-138.41	-135.14	-45.94	90.29	33.10	-296.81	-395.77
300	0.05	0.05	0.04	-20.44	-241.77	-138.33	-135.08	-45.87	90.35	33.16	-296.74	-395.67
350	1.51	1.53	1.08	-18.72	-240.08	-136.18	-133.23	-44.05	91.84	35.06	-294.70	-393.04
400	2.97	3.06	2.12	-16.98	-238.37	-133.90	-131.31	-42.16	93.34	37.06	-292.57	-390.25
450	4.44	4.62	3.16	-15.19	-236.65	-131.53	-129.31	-40.19	94.87	39.15	-290.36	-387.30
500	5.91	6.21	4.20	-13.36	-234.91	-129.09	-127.26	-38.14	96.41	41.30	-288.07	-384.20
550	7.39	7.81	5.24	-11.49	-233.13	-126.58	-125.15	-36.01	97.97	43.51	-285.70	-380.99
600	8.89	9.44	6.27	-9.58	-231.33	-124.03	-122.99	-33.81	99.54	45.78	-283.27	-377.66
650	10.41	11.08	7.31	-7.62	-229.50	-121.43	-120.79	-31.53	101.13	48.10	-280.79	-374.24
700	11.94	12.74	8.35	-5.62	-227.65	-118.79	-118.53	-29.17	102.73	50.46	-278.26	-370.75
750	13.48	14.40	9.39	-3.58	-225.76	-116.12	-116.23	-26.73	104.34	52.86	-275.69	-367.20
800	15.05	16.09	10.43	-1.49	-223.84	-113.41	-113.89	-24.21	105.97	55.30	-273.08	-363.59
850	16.63	17.78	11.47	0.63	-221.89	-110.67	-111.50	-21.61	107.61	57.78	-270.45	-359.92
900	18.22	19.48	12.51	2.79	-219.91	-107.90	-109.07	-18.94	109.26	60.29	-267.78	-356.22
950	19.84	21.19	13.55	4.99	-217.89	-105.11	-106.60	-16.20	110.93	62.84	-265.09	-352.47
1000	21.46	22.92	14.59	7.23	-215.84	-102.29	-104.10	-13.40	112.61	65.41	-262.38	-348.70
1050	23.10	24.65	15.63	9.51	-213.76	-99.45	-101.56	-10.54	114.30	68.02	-259.65	-344.89
1100	24.76	26.39	16.67	11.82	-211.65	-96.59	-99.00	-7.62	116.00	70.65	-256.90	-341.05
1150	26.43	28.15	17.71	14.16	-209.51	-93.70	-96.41	-4.65	117.71	73.30	-254.14	-337.19
1200	28.11	29.91	18.75	16.54	-207.34	-90.79	-93.79	-1.63	119.43	75.98	-251.36	-333.31
1250	29.80	31.68	19.79	18.94	-205.13	-87.87	-91.15	1.44	121.16	78.67	-248.57	-329.41
1300	31.51	33.45	20.83	21.38	-202.90	-84.93	-88.49	4.55	122.91	81.39	-245.76	-325.49
1350	33.22	35.24	21.86	23.85	-200.64	-81.97	-85.80	7.71	124.66	84.12	-242.94	-321.55
1400	34.94	37.03	22.90	26.34	-198.35	-78.99	-83.09	10.92	126.42	86.87	-240.11	-317.60
1450	36.68	38.84	23.94	28.87	-196.03	-76.00	-80.37	14.16	128.18	89.63	-237.27	-313.63
1500	38.42	40.65	24.98	31.41	-193.69	-72.99	-77.62	17.45	129.96	92.40	-234.43	-309.65

$$= - 802.30 \text{ kJ/mol,}$$

which is equal to the so-called heat of combustion for methane gas.

Example 2.9. Calculate the reaction enthalpy of the combustion reaction of propane gas



at a temperature of 450 K using the average specific heat capacity values at a temperature range of 298.15-400 K and compare the result with the value calculated using table 2.4. First, let's calculate the enthalpies of different compounds with enthalpies of formation and average specific heat capacities (table 2.3)

$$\text{C}_3\text{H}_8(\text{g}), h^\circ = \Delta H^\circ_f(T_0) + \bar{c}_p^\circ (T - T_0) = - 105.8 + 93.2 \cdot 10^{-3} \cdot (450 - 298.15)$$

$$= - 91.65 \text{ kJ/mol}$$

$$\text{CO}_2(\text{g}), h^\circ = - 393.5 + 40.2 \cdot 10^{-3} \cdot (450 - 298.15) = - 387.05 \text{ kJ/mol}$$

$$\text{O}_2(\text{g}), h^\circ = 0 + 30.0 \cdot 10^{-3} \cdot (450 - 298.15) = + 4.55 \text{ kJ/mol}$$

$$\text{H}_2\text{O}(\text{g}), h^\circ = -241.8 + 34.2 \cdot 10^{-3} \cdot (450 - 298.15) = - 236.61 \text{ kJ/mol}$$

$$\Delta H^\circ = H(\text{B}) - H(\text{A}) =$$

$$\{3h^\circ[\text{CO}_2(\text{g})] + 4h^\circ[\text{H}_2\text{O}(\text{g})]\} - \{h^\circ[\text{C}_3\text{H}_8(\text{g})] + 5h^\circ[\text{O}_2(\text{g})]\}$$

$$\Delta H^\circ = \{3 \cdot (- 387.05) + 4 \cdot (- 236.61)\} - \{(- 91.65) + 5 \cdot 4.55\} \text{ kJ/mol}$$

$$= - 2012 \text{ kJ/mol.}$$

The same calculation using values in table 2.4

$$\Delta H^\circ = [3 \cdot (- 387.42) + 4 \cdot (- 236.64)] - [(- 90.62) + 5 \cdot 4.56] =$$

$$- 2041 \text{ kJ/mol.}$$

The result calculated with table 2.4 is naturally more accurate since its enthalpies have been calculated with consideration to the temperature dependence of specific heat capacity.

Table 2.4 is excellent when calculating for example gas reactors. The enthalpies of gases entering and exiting the reactor at given temperatures can be found directly in table 2.4 and the power of heat absorbed or emitted by the reactor can be calculated with the difference in the enthalpy streams.

Example 2.10. Calculate the heat released in reaction (2.17) when propane gas and oxygen enter the reactor at a temperature of 350K and the products carbon dioxide and water vapor exit it at a temperature of 450K. From table 2.4 we get that

$$\Delta H^{\circ} = [3(-387.42) + 4(-236.64)] - [(-100.90) + 5 \cdot 1.53] = -2015.57 \text{ kJ/mol}$$

which means that the power of heat released is 2016 kW when 1 mol/s of propane gas is combusted.

Example 2.11. Table 2.4 is also very convenient when analyzing for example flue gas losses. In an example presented later in chapter 12 the composition of flue gases for a certain light fuel oil has been calculated with an air factor of 1.15 per one kilogram of fuel:

O ₂	15.6 mol/kg fuel
Ar	5.3 mol/kg fuel
N ₂	451.3 mol/kg fuel
CO ₂	71.5 mol/kg fuel
H ₂ O	67.8 mol/kg fuel

If the flue gases exit the boiler at a temperature of 450 K, how much additional power would be gained if the flue gases were cooled to 350 K, when the amount of oil combusted is 0.2 kg/s? Additional energy gained per one kilogram of oil combusted is

$$\begin{aligned} \Delta H^{\circ} &= \sum_i n_i [h_i(450\text{K}) - h_i(350\text{K})] \\ &= 15.6(4.56 - 1.53) + 451.3(4.44 - 1.51) \\ &\quad + 71.5[-387.42 - (-391.53)] \\ &\quad + 67.8[-236.64 - (-240.08)] \\ &\quad + 5.3(3.16 - 1.08) \\ &= 1.908 \cdot 10^3 \text{ kJ/kg fuel} \end{aligned}$$

and therefore, the additional power is

$$\phi = 0.2 \text{ kg/s} \cdot 1.908 \cdot 10^3 \text{ kJ/kg} = 382 \text{ kW.}$$

Example 2.12. Flue gas loss means the enthalpy stream along with flue gases compared to a situation where the flue gases would exit at the standard state temperature of 25 °C. In the previous example the flue gas losses when the flue gases exit at a temperature of 350 K can be calculated using table 2.4 with:

$$\begin{aligned}\Delta H^{\circ} &= \sum_i n_i [h_i^{\circ}(350\text{K}) - h_i^{\circ}(298.15\text{K})] \\ &= 15.6(1.53 - 0) + 451.3(1.51 - 0) \\ &\quad + 71.5[(-391.53) - (-393.52)] \\ &\quad + 67.8[(-240.08) - (-241.83)] \\ &\quad + 5.3(1.08 - 0) = 972.0 \text{ kJ/kg fuel.}\end{aligned}$$

The flue gas losses are $\phi = 0.2 \cdot 972.0 = 194.4 \text{ kW}$. These examples are further discussed in chapter 4 and calculations based on tabulated enthalpies and heating values of fuels are also presented.

2.4.2 Pressure dependence of enthalpy and specific heat capacity

Generally, the specific heat capacity of a compound is also dependent on pressure: $c_p = c_p(T,p)$. According to equation (2.8)

$$\frac{\partial h}{\partial p} = v - T \frac{\partial v}{\partial T}, \quad (2.18)$$

differentiating the definition of specific heat capacity

$$c_p = \frac{\partial h}{\partial T}$$

with respect to pressure and taking into account equation (2.18) results in

$$\frac{\partial c_p}{\partial p} = \frac{\partial}{\partial p} \left(\frac{\partial h}{\partial T} \right) = \frac{\partial}{\partial T} \left(\frac{\partial h}{\partial p} \right) = \frac{\partial}{\partial T} \left(v - T \frac{\partial v}{\partial T} \right) = \frac{\partial v}{\partial T} - \frac{\partial v}{\partial T} - T \frac{\partial^2 v}{\partial T^2}.$$

The pressure dependence of specific heat capacity is therefore

$$\frac{\partial c_p}{\partial p} = -T \frac{\partial^2 v}{\partial T^2} \quad (2.19)$$

where $v = v(T,p)$ is molar specific volume (m^3/mol).

Example 2.13. According to the ideal gas law

$$\frac{V}{N} = v(T,p) = RT/p, \quad (2.20)$$

where $R = 8.314 \text{ J}/(\text{mol K})$. Therefore,

$$\frac{\partial^2 v}{\partial T^2} = 0$$

and for an ideal gas

$$c_p(T,p) = c_p(T). \quad (2.21)$$

For a real gas $\partial^2 v / \partial T^2 \neq 0$ and therefore c_p is also a function of pressure. A gas acts like an ideal gas the further the gas is from the critical point and therefore, the specific heat capacity is only dependent on temperature. In flue gas calculations, the gases can be considered as ideal gases.

Similarly, the specific volume of solids and liquids is often approximately linearly dependent on temperature T . Therefore, according to equation (2.19), c_p is only a function of temperature with high accuracy. An important exception is for example water and water vapor at high temperatures and pressures. At high pressures water vapor deviates significantly from an ideal gas. The deviation is greater the closer to the critical point the vapor is. This is also true in general for other liquids and gases near the critical point.

Example 2.14.

$$\text{Water vapor: } c_p(573.15 \text{ K}, 1.0 \text{ bar}) = 2.010 \frac{\text{kJ}}{\text{kg K}} = 36.18 \frac{\text{J}}{\text{mol K}},$$

$$\text{water vapor: } c_p(573.15 \text{ K}, 75 \text{ bar}) = 4.686 \frac{\text{kJ}}{\text{kg K}} = 84.35 \frac{\text{J}}{\text{mol K}},$$

$$\text{water: } c_p(573.15 \text{ K}, 100 \text{ bar}) = 5.692 \frac{\text{kJ}}{\text{kg K}} = 102.46 \frac{\text{J}}{\text{mol K}},$$

$$\text{water: } c_p(573.15 \text{ K}, 190 \text{ bar}) = 5.350 \frac{\text{kJ}}{\text{kg K}} = 96.30 \frac{\text{J}}{\text{mol K}}.$$

Example 2.15. For solid substances approximately

$$\gamma \equiv \frac{1}{v} \left(\frac{\partial v}{\partial T} \right) = 10^{-5} \dots 2.0 \cdot 10^{-4} \text{ K}^{-1}, \quad (2.22)$$

and therefore, at room temperature $T = 298.15 \text{ K}$ the pressure dependence of enthalpy

$$\left(\frac{\partial h}{\partial p} \right)_T = v(1 - T\gamma) = (0.9970 \dots 0.9404)v. \quad (2.23)$$

Example 2.16. For an ideal gas

$$\left(\frac{\partial h}{\partial p} \right)_T = v - T \frac{R}{p} = 0,$$

which means that enthalpy is only dependent on temperature:

$$h(T, p) = h(T). \quad (2.24)$$

For non-ideal gases the specific enthalpy is a function of temperature and pressure. In addition, generally speaking the state and state functions of the components of a mixture are also dependent on the mole amounts of the components n_1, \dots, n_m .

If the enthalpy of formation $\Delta H_f^\circ(T_0)$, specific heat capacity $c_p(T, p)$ and specific volume $v(T, p)$ at the standard state are known, the enthalpy of a compound can be calculated at any temperature T_1 and pressure p_1

$$h(T_1, p_1) = \Delta H_f^\circ(T_0) + \int_{T_0}^{T_1} \left(\frac{\partial h}{\partial T} \right)_{p=p^\circ} dT + \int_{p^\circ}^{p_1} \left(\frac{\partial h}{\partial p} \right)_{T=T_1} dp \quad (2.25)$$

i.e. with the definition $c_p = \frac{\partial h}{\partial T}$ and equation (2.18)

$$h(T_1, p_1) = \Delta H_f^\circ(T_0) + \int_{T_0}^{T_1} c_p(T, p_0) dT + \int_{p_0}^{p_1} \left[v(T_1, p) - T_1 \left(\frac{\partial v}{\partial T} \right)_{T=T_1} \right] dp \quad (2.26)$$

2.5 Enthalpy at the absolute zero

When the enthalpy value is defined with equation (2.13) at a temperature of T_0 , the enthalpy of a compound or an element at the absolute zero can be calculated with equation (2.16). This enthalpy is noted as $h^\circ(0)$ [$H^\circ(0)$ in tables]. By taking into consideration the definition (2.13), i.e. $h^\circ(T_0) \equiv \Delta H_f^\circ(T_0)$, according to equation (2.16) we get

$$h^\circ(0) - h^\circ(T_0) = \int_{T_0}^{T_r} c_p dT + \Delta H_{tr}^\circ(T_r) + \int_{T_r}^0 c_p dT. \quad (2.27)$$

If a gas is analyzed, another phase change term, the crystallization of liquid and the enthalpy change associated with it, has to be added to equation (2.27). If a solid substance is analyzed, phase change terms are not necessarily present. However, a phase change in solid substances is possible between different crystal structures.

Values of $[h^\circ(0) - h^\circ(T_0)]$ are already calculated for different compounds in table books of chemical thermodynamics, as well as values of $[h^\circ(T) - h^\circ(T_0)]$ at certain temperature increments. For example, a table of values for aluminum oxide is presented below.

Example 2.17. Aluminum is produced from aluminum oxide (Al_2O_3) by heating it up to its melting point and performing an electrolysis. Calculate the amount of energy required to heat up aluminum oxide from 500 K to a temperature of 2500 K. Liquification occurs at a temperature of 2327 K, which has an endothermic heat of melting of 111.086 kJ/mol. From table 2.5 we can directly read ($T_0 = T_r = 298.15$ K)

$$h^\circ(T = 500 \text{ K}) - h^\circ(T_0) = 19.145 \text{ kJ/mol (crystal, alpha (corundum))}$$

$$h^\circ(T = 2500 \text{ K}) - h^\circ(T_0) = 399.143 \text{ kJ/mol, (liquid)}$$

and therefore, the required amount of energy is

$$h^\circ(T = 2500 \text{ K}) - h^\circ(500 \text{ K}) = 399.143 - 19.145 = 379.998 \text{ kJ/mol.}$$

As seen from the table below, this amount of energy also includes the amount of heat required by the liquification of aluminum oxide, i.e. the heat of melting at a temperature of 2327K.

Table 2.5. Thermodynamic properties of aluminum oxide $Al_2O_3(cr, l)$ [1].

Aluminum Oxide (Al_2O_3)				$Al_2O_3(cr, l)$			
Enthalpy Reference Temperature = $T_r = 298.15$ K				Standard State Pressure = $p^\circ = 0.1$ MPa			
T/K	J $K^{-1}mol^{-1}$			kJ mol^{-1}			Log K_f
	C_p°	S°	$-[G^\circ - H^\circ(T_r)]/T$	$H^\circ - H^\circ(T_r)$	$\Delta_f H^\circ$	$\Delta_f G^\circ$	
0	0.	0.	INFINITE	-10.020	-1663.608	-1663.608	INFINITE
100	12.855	4.295	101.230	-9.693	-1668.606	-1641.642	857.506
200	51.120	24.880	57.381	-6.500	-1673.383	-1612.656	421.183
298.15	79.015	50.950	50.950	0.	-1675.692	-1582.275	277.208
300	79.418	51.440	50.951	0.147	-1675.717	-1581.696	275.398
400	96.086	76.779	54.293	8.995	-1676.342	-1550.226	202.439
500	106.131	99.388	61.098	19.145	-1676.045	-1518.718	158.659
600	112.545	119.345	69.177	30.101	-1675.300	-1487.319	129.483
700	116.926	137.041	77.632	41.586	-1674.391	-1456.059	108.652
800	120.135	152.873	86.065	53.447	-1673.498	-1424.931	93.038
900	122.662	167.174	94.296	65.591	-1672.744	-1393.908	80.900
1000	124.771	180.210	102.245	77.965	-1672.394	-1361.437	71.114
1100	126.608	192.189	109.884	90.535	-1672.437	-1328.286	63.075
1200	128.252	203.277	117.211	103.280	-1672.366	-1295.228	56.380
1300	129.737	213.602	124.233	116.180	-1672.190	-1262.264	50.718
1400	131.081	223.267	130.965	129.222	-1672.018	-1229.393	45.869
1500	132.290	232.353	137.425	142.392	-1671.851	-1196.617	41.670
1600	133.361	240.925	143.628	155.675	-1671.688	-1163.934	37.999
1700	134.306	249.039	149.592	169.060	-1671.532	-1131.342	34.762
1800	135.143	256.740	155.333	182.533	-1671.382	-1098.841	31.888
1900	135.898	264.067	160.864	196.085	-1671.238	-1066.426	29.318
2000	136.608	271.056	166.201	209.710	-1671.100	-1034.096	27.008
2100	137.319	277.738	171.354	223.407	-1670.968	-1001.849	24.920
2200	138.030	284.143	176.336	237.174	-1670.842	-969.681	23.023
2300	138.741	290.294	181.158	251.013	-1670.722	-937.593	21.293
2327.000	138.934	291.914	182.434	254.761		ALPHA <--> LIQUID	
2327.000	192.464	339.652	182.434	365.847		TRANSITION	
2400	192.464	345.597	187.307	379.896	-1557.989	-909.127	19.787
2500	192.464	353.454	193.796	399.143	-1550.905	-882.237	18.433
2600	192.464	361.002	200.083	418.389	-1543.853	-855.629	17.190
2700	192.464	368.266	206.179	437.636	-1536.832	-829.292	16.044
2800	192.464	375.265	212.093	456.882	-1529.832	-803.279	14.948
2900	192.464	382.019	217.837	476.128	-1522.844	-777.429	13.889
3000	192.464	388.544	223.419	495.375	-1515.868	-751.732	12.865
3100	192.464	394.855	228.848	514.621	-1508.904	-726.279	11.875
3200	192.464	400.965	234.132	533.868	-1501.952	-701.062	10.918
3300	192.464	406.888	239.277	553.114	-1495.012	-676.073	9.993
3400	192.464	412.633	244.292	572.360	-1488.084	-651.302	9.098
3500	192.464	418.212	249.182	591.607	-1481.168	-626.749	8.232
3600	192.464	423.634	253.953	610.853	-1474.264	-602.414	7.393
3700	192.464	428.908	258.610	630.100	-1467.372	-578.298	6.587
3800	192.464	434.040	263.160	649.346	-1460.492	-554.401	5.811
3900	192.464	439.040	267.606	668.592	-1453.624	-530.724	5.063
4000	192.464	443.912	271.953	687.839	-1446.768	-507.277	4.341

$$dh = \left(\frac{\partial h}{\partial T} \right)_p dT + \left(\frac{\partial h}{\partial p} \right)_T dp$$

$$\Delta H = \int_{298.15}^{350} c_p dT = 38.27 \cdot (350 - 298.15) = 1.984 \text{ kJ/mol}$$