



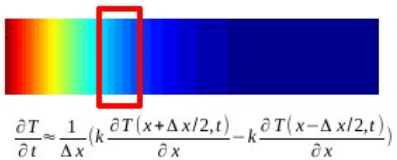
EEN-1020 Heat transfer

Week 5: Heat transfer via natural convection

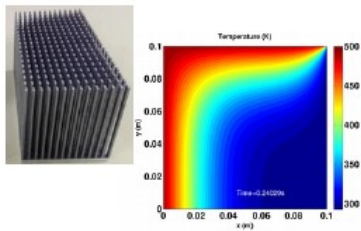
Prof. Ville Vuorinen
Nov. 21st-22nd 2023

Aalto University, School of Engineering

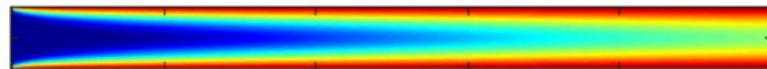
Week 1: Energy conservation, heat equation, conduction Fourier/Newton



Week 2: Fin theory, conduction, intro to convection

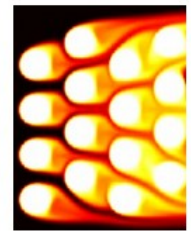


Week 3: convective heat transfer – internal flow (channel)



Week 4: convective heat transfer – external flow (fin systems)

Week 5: natural convection, boiling, correlations





On the heat transfer course, we have “5 friends”
i.e. 5 main principles that are used to explain
heat transfer phenomena

- 1) Energy conservation: “J/s thinking”
- 2) Fourier’s law
- 3) Newton’s cooling law
- 4) Energy transport equation – convection/diffusion equation
- 5) Momentum transport equation – Navier-Stokes equation



Lecture 5.1 Theory: Natural convection (free convection)

ILO 5: Student can choose Nusselt number correlation equations for different situations including natural convection.

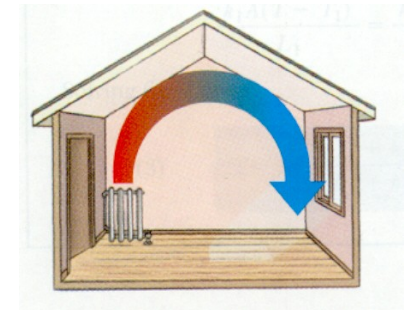
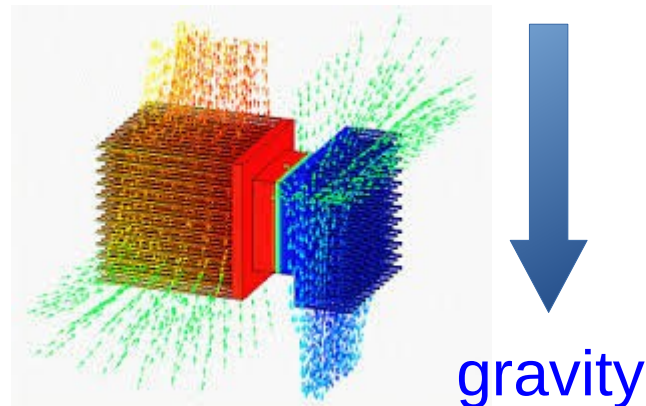
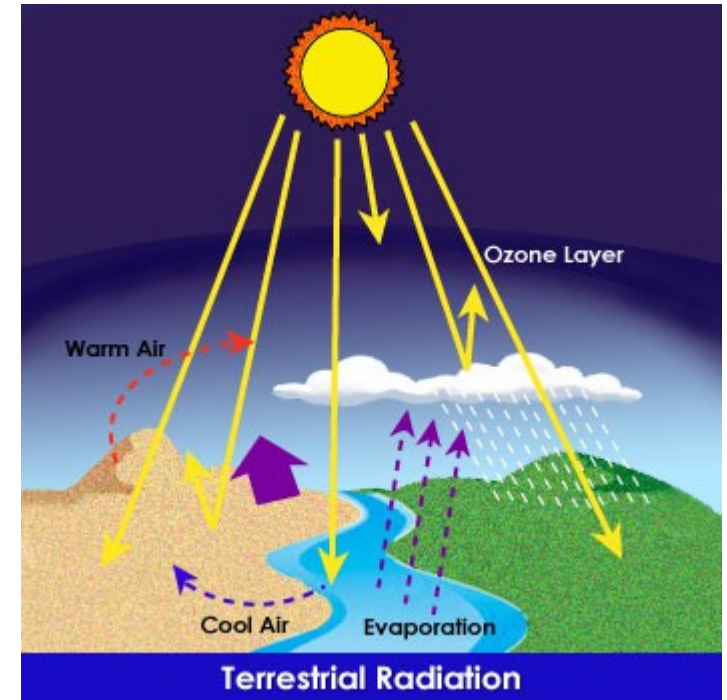
Warm fluids are lighter than cold fluids → ability to rise against gravity → buoyancy





Topics covered

- Governing equations in natural convection
- Non-dimensional numbers
- Stable vs unstable configurations
- Boundary layers in natural convection

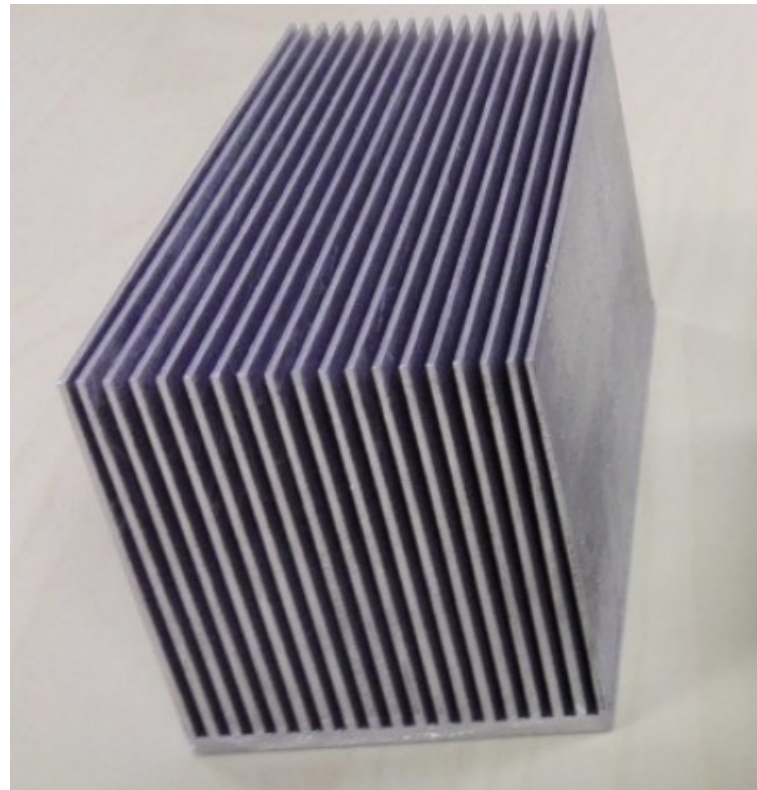




2018: we **switched off the fan** in the class room demo system
≈ 24W fixed and uniform heating power from the base plate.

→ The physical heat transfer mechanisms are natural convection and radiation.

Consequence of switching off the fan:
the heat exchanger became extremely hot!



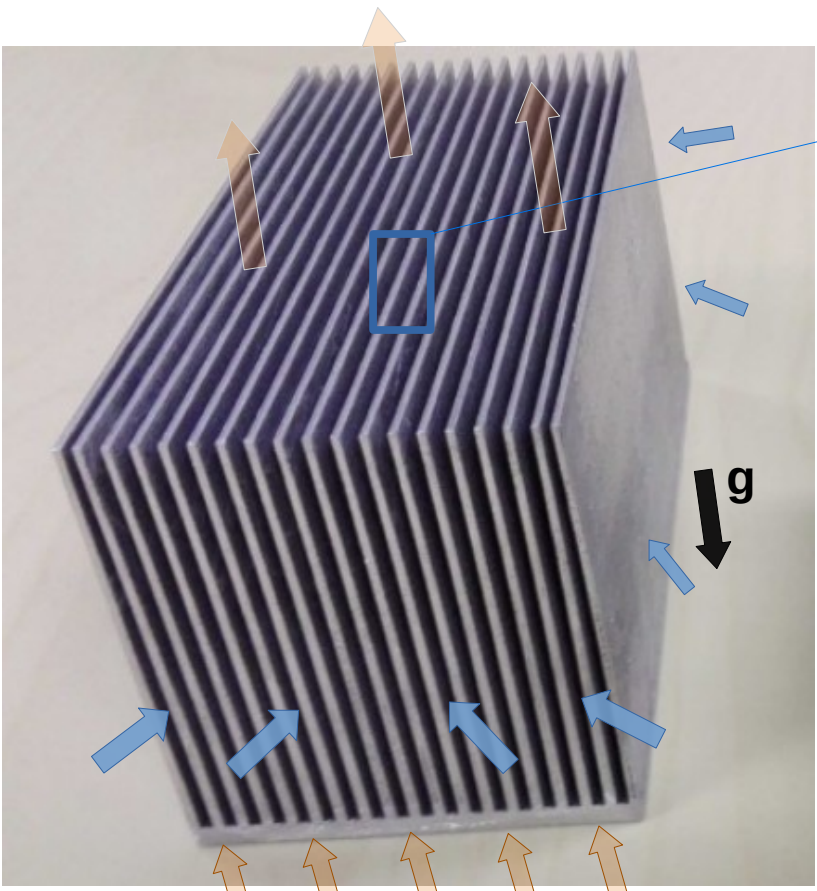
For a very slow physical cooling mechanism:

$$dT/dt \approx q/mc_p \rightarrow \text{e.g. } 0.25\text{K/s} = 15\text{K/min.}$$



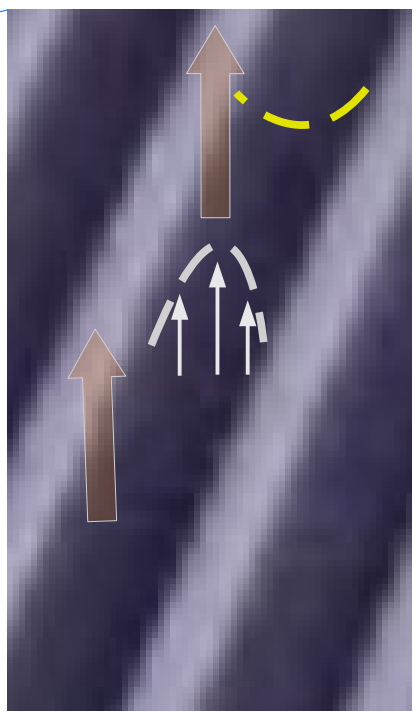
Heated air starts rising upwards and cool air enters through the sides. Heat transfers from the hot fin surfaces to the gas.

Warm air exits by rising upwards: T_{hot}



Cool air enters: T_{∞}

Power (J/s)



Airflow Temperature

Common wall boundary conditions:

- Type 1: $T_s = \text{known}$
- Type 2: $q_s = \text{known}$

Airflow velocity

Wall boundary condition:

No-slip:
 $U=V=W=0\text{m/s}$



Energy balance (J/s thinking) for gas flow when the gas is heated at power P (W). “Control volume” thinking.

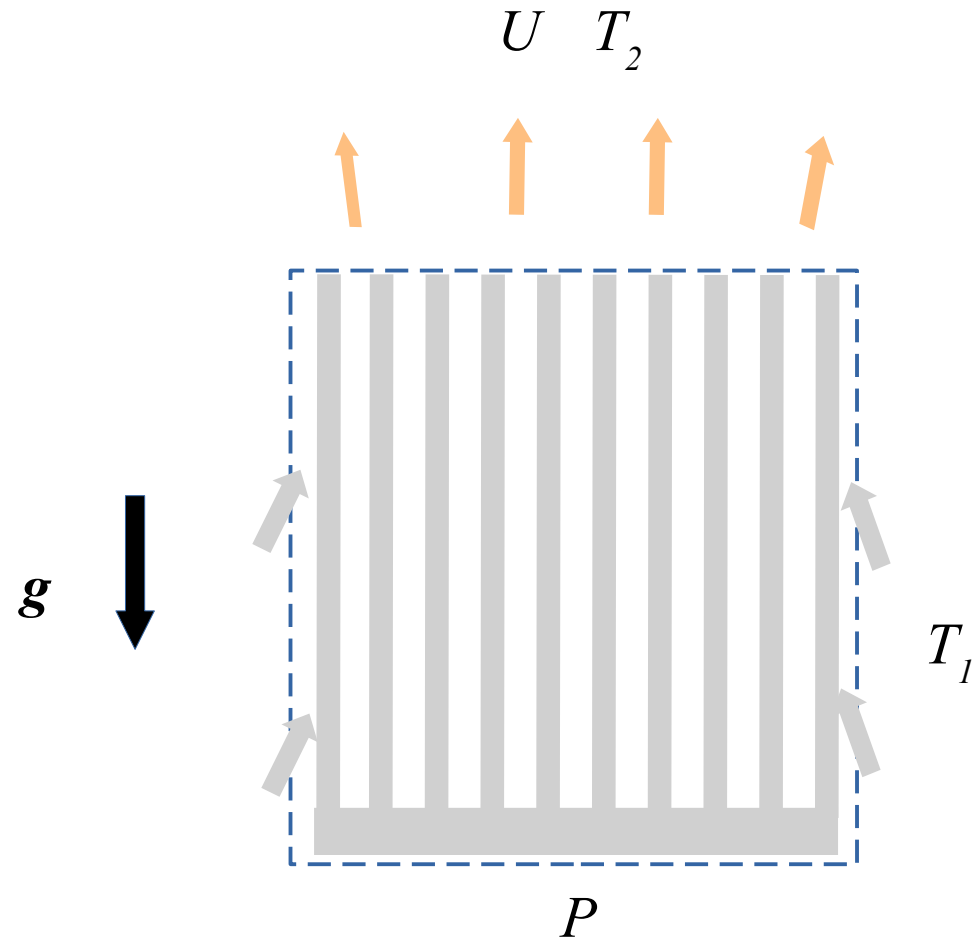
$$Q_{\text{OUT}} - Q_{\text{IN}} = c_p \dot{m} \Delta T_{\text{ave}} = P$$

Mass flow rate of the gas (kg/s)
into the system from sides = exiting
mass flow rate from the top:

$$\dot{m} = \rho U_{\text{top}} A_{\text{top}} = \rho U_s A_s$$

Average temperature change:

$$\Delta T_{\text{ave}} = T_2 - T_1$$





Why a drink can cools? Which orientation offers faster cooling: horizontal vs vertical? Why?

Newton

$$q = hA_s(T_s - T_\infty)$$



What parameters affect h and Nu ?

Note: radiation neglected on this course.



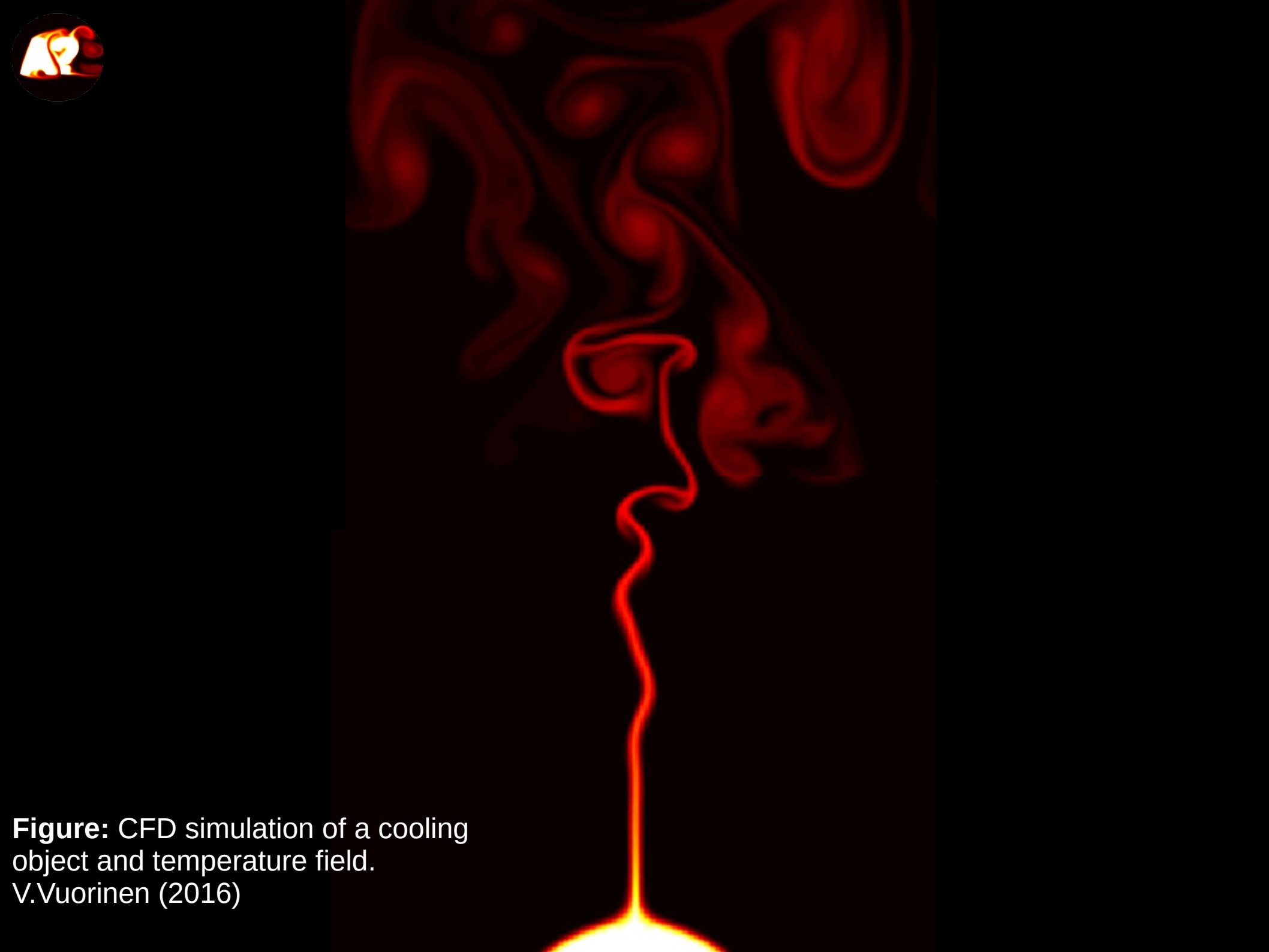


Figure: CFD simulation of a cooling object and temperature field.
V.Vuorinen (2016)



Governing equations (here 2d) in natural convection using the Boussinesq approximation for the buoyancy force

Navier-Stokes (momentum)

$$\frac{\partial U}{\partial t} + U \frac{\partial U}{\partial x} + V \frac{\partial U}{\partial y} = \frac{-1}{\rho} \frac{\partial p}{\partial x} + \nu \frac{\partial^2 U}{\partial x^2} + \nu \frac{\partial^2 U}{\partial y^2} - g_x \beta (T - T_\infty)$$

$$\frac{\partial V}{\partial t} + U \frac{\partial V}{\partial x} + V \frac{\partial V}{\partial y} = \frac{-1}{\rho} \frac{\partial p}{\partial y} + \nu \frac{\partial^2 V}{\partial x^2} + \nu \frac{\partial^2 V}{\partial y^2} - g_y \beta (T - T_\infty)$$

Buoyancy force: tries to promote motion into opposite direction from gravity

Convection-diffusion for temperature (energy equation)

$$\frac{\partial T}{\partial t} + U \frac{\partial T}{\partial x} + V \frac{\partial T}{\partial y} = \alpha \frac{\partial^2 T}{\partial x^2} + \alpha \frac{\partial^2 T}{\partial y^2}$$



Derivation of thermal expansion coefficient for ideal gas ($\beta = 1/T$)

Ideal gas law

$$p = \rho RT$$

Thermal expansion coefficient

$$\beta = -\frac{1}{\rho} \left(\frac{\partial \rho}{\partial T} \right)_p = -\frac{1}{\rho} \left(\frac{\partial [p/RT]}{\partial T} \right)_p = \frac{p}{\rho RT^2} = 1/T$$

Note: for other fluids values of the expansion coefficient have been tabulated.



Assumptions in Boussinesq approximation

- Density is assumed to have a well defined mean part and a fluctuation part

$$\rho = \rho_o - \left(\frac{\partial \rho}{\partial T} \right)_p \Delta T$$

or

$$\rho = \rho_o - \beta \rho_o \Delta T$$

Fluctuation part of density contributing to a buoyancy force in the Boussinesq approximation

- Thermodynamic pressure is assumed to be almost constant (often a very good assumption because speed of sound is typically high in comparison to other velocities*)
- Temperature will then be a function of density
- When temperature of a point in space increases, the density decreases
- It leads to a buoyancy force promoting motion against gravity (“hot air balloon effect”)
- we can think that pointwise fluctuations of temperature from the mean ($T' = T - T_{ref}$) promote/drive the flow into motion

*Note: e.g. in a typical flame pressure is almost constant but density and temperature depend very strongly on position (low density in hot parts).



Important numbers

Grashof number

$$Gr = \frac{g\beta(T_s - T_\infty)L^3}{\nu^2} = \frac{\text{Buoyancy force}}{\text{Viscous force}}$$

$L \rightarrow$ characteristic length scale of surface / object

$\beta \rightarrow$ thermal expansion coefficient

Thermal expansion coefficient

$$\beta = -\frac{1}{\rho} \left(\frac{\partial \rho}{\partial T} \right)_p$$

Rayleigh number (Ra and Gr closely related)

$$Ra = \frac{g\beta(T_s - T_\infty)L^3}{\nu\alpha} = \frac{\text{Buoyancy force}}{\text{Viscous force}}$$

$\alpha =$ thermal diffusivity, $\nu =$ kinematic viscosity



Differences in Nusselt number correlations

Note: In forced convection the Reynolds and Prandtl numbers were of very high importance. $Nu=Nu(Re,Pr)$.

Note: In natural convection the Rayleigh (and/or Grashof) number is typically the key driving parameter. $Nu=Nu(Ra,Pr)$ or $Nu=Nu(Gr,Pr)$.

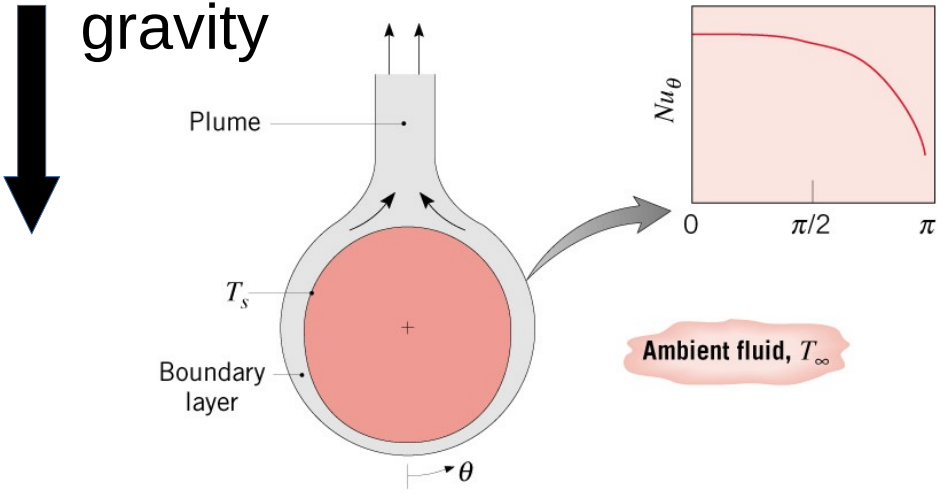
Note: here we do not discuss the mixed convection case.



Nusselt number correlation for a horizontal cylinder



Horizontal cylinder



$$Ra = \frac{g\beta(T_s - T_\infty)L^3}{\nu\alpha} = \frac{\text{Buoyancy force}}{\text{Viscous force}}$$

$$Ra_D < 10^{12}$$

$$\bar{Nu}_D = 0.60 + \frac{0.387 Ra_D^{1/6}}{[1 + (0.559/Pr)^{9/16}]^{8/27}}$$

What happens when $Ra_D \rightarrow 0$?

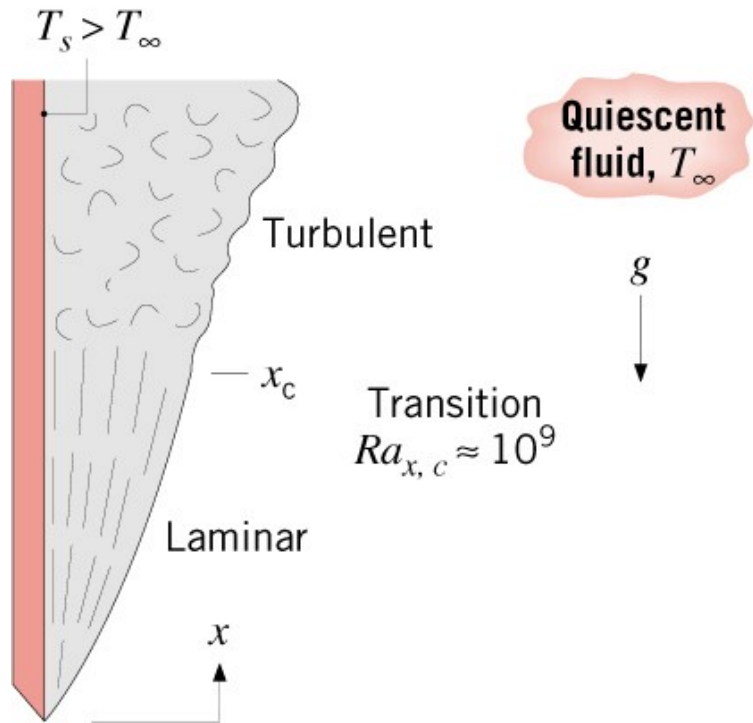
$$\bar{Nu}_D = \frac{\bar{h}D}{k}$$



Nusselt number correlation for a vertical plate



NC creates flow against gravity → near-wall boundary layers → possibility for laminar to turbulence transition → critical Rayleigh number



Critical Rayleigh number where flow becomes turbulent at $x=x_c$

$$Ra_c = 10^9$$

Example: Vertical plate average Nusselt number for laminar conditions ($x < x_c$)

$$\bar{Nu} = 0.68 + \frac{0.670 Ra_L^{1/4}}{[1 + (0.492/Pr)^{9/16}]^{4/9}}$$

Example: Vertical plate average Nusselt number for all conditions (see a few slides ahead)

$$\bar{Nu}_L = \left[0.825 + \frac{0.387 Ra_L^{1/6}}{[1 + (0.492/Pr)^{9/16}]^{8/27}} \right]^2$$

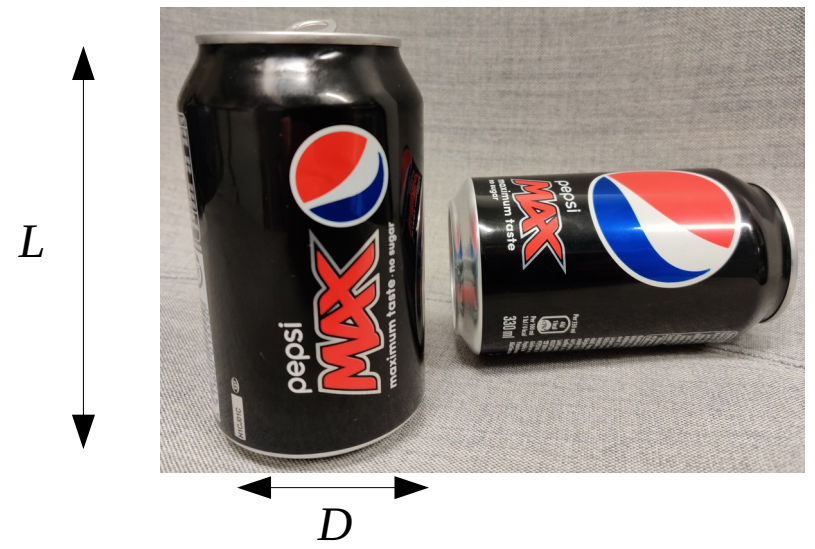


Which way does a can cool faster in the fridge: horizontally or vertically ?

Rayleigh number (general length scale L)

$$Ra = \frac{g\beta(T_s - T_\infty)L^3}{\nu\alpha} = \frac{\text{Buoyancy force}}{\text{Viscous force}}$$

D = 0.06m, L = 0.17m



Horizontal cylinder:

$$\bar{Nu}_D = 0.60 + \frac{0.387 Ra_D^{1/6}}{[1 + (0.559/Pr)^{9/16}]^{8/27}}$$

Vertical cylinder:

$$\bar{Nu}_L = \left[0.825 + \frac{0.387 Ra_L^{1/6}}{[1 + (0.492/Pr)^{9/16}]^{8/27}} \right]^2$$

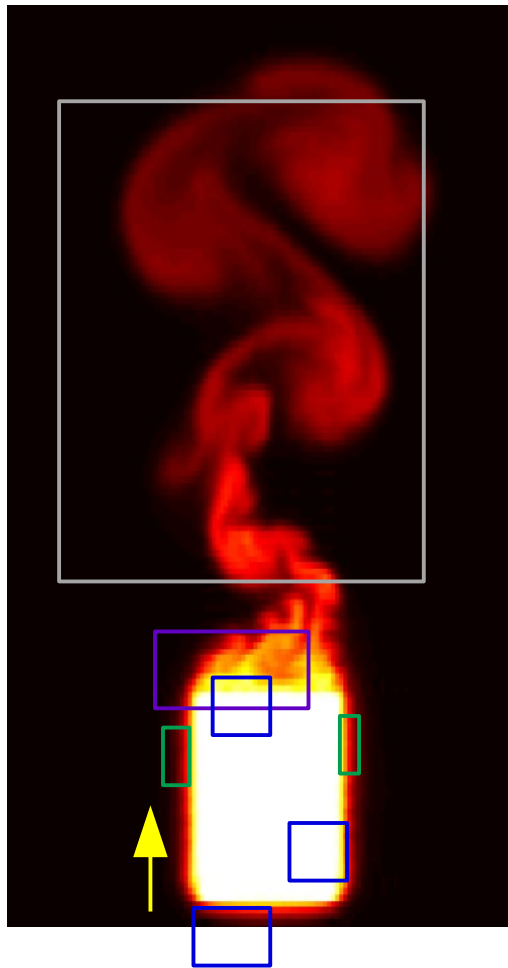


Some physical steps how heat transfer away from a can in natural convection

Step 1: Conduction from the wall to the fluid and conduction in the thermal boundary layer (TBL).

Step 2: Heated fluid starts rising upwards already when conducting in the TBL

Step 3: Accelerated flow forms **viscous and thermal** boundary layers around the can.



Step 5: fluid rises constantly and the hot air is “**self-transported**” away from the object in a plume which poses fluid dynamical structures (e.g. vortices, turbulence)

Step 4: fluid motion becomes 3d and turbulence starts to transport heat from the top surface



Example 9.2: Estimate convective heat rate for glass window of a fireplace – relevance HW5

First, estimate Ra for air rising along glass window:

$$Ra = \frac{g\beta(T_s - T_\infty)L^3}{\nu\alpha} = 1.813 \cdot 10^9 > Ra_c$$

Use the correlation valid at all conditions ($Ra > Ra_c$):

$$\bar{Nu}_L = \left[0.825 + \frac{0.387 Ra_L^{1/6}}{[1 + (0.492/Pr)^{9/16}]^{8/27}} \right]^2 = 147$$

Estimate heat transfer coefficient:

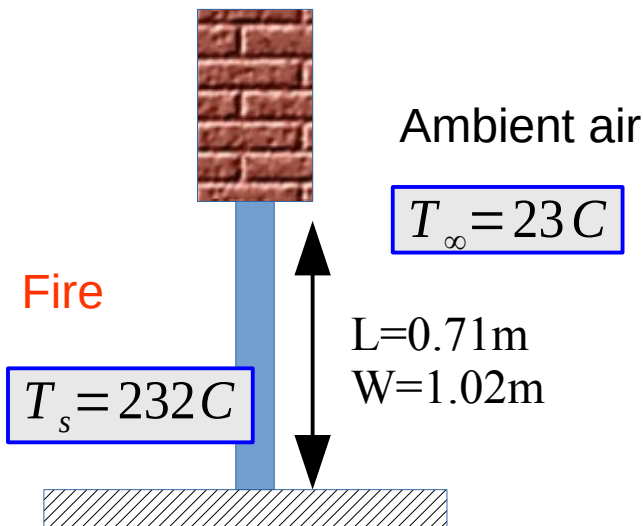
$$\bar{h} = \frac{\bar{Nu}_L k}{L} = 7.0 \text{ W/m}^2 \text{ K}$$

Heat rate from Newton's law of cooling:

$$q = \bar{h} A_s (T_s - T_\infty) = 1060 \text{ W}$$

Note: radiative heat transfer would be essential here:

$$q_{rad} = \epsilon A_s \sigma (T_s^4 - T_\infty^4) = 2355 \text{ W}$$





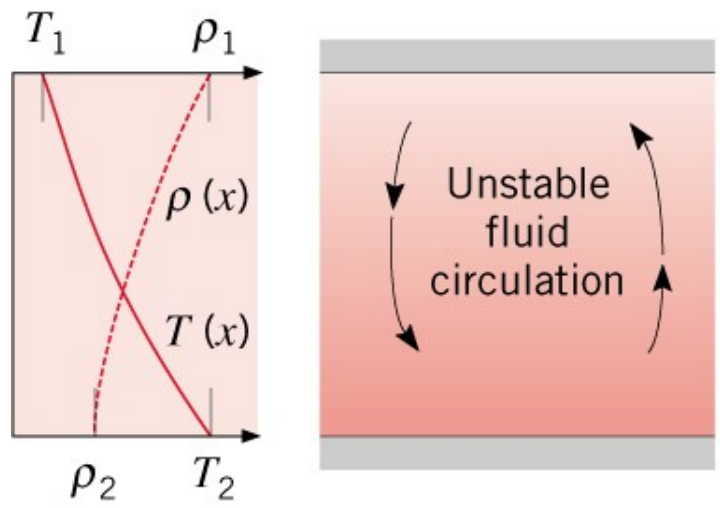
Flow in confinements



Unstable vs stable configurations

cold

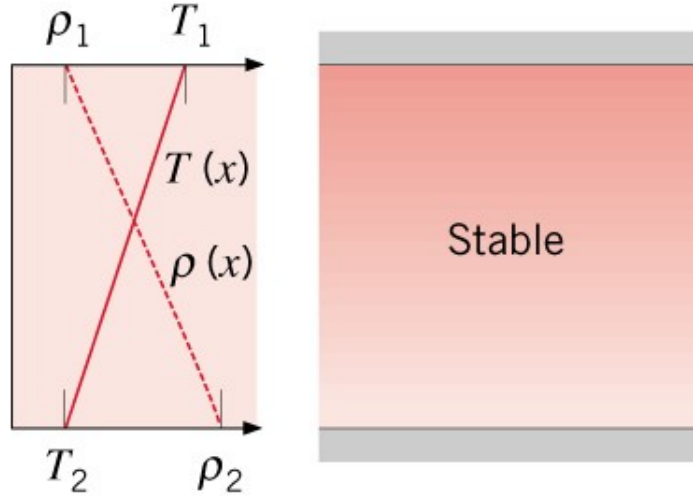
hot



$$\frac{dT}{dx} > 0, \frac{d\rho}{dx} < 0$$

(a)

x
g



$$\frac{dT}{dx} < 0, \frac{d\rho}{dx} > 0$$

(b)

hot

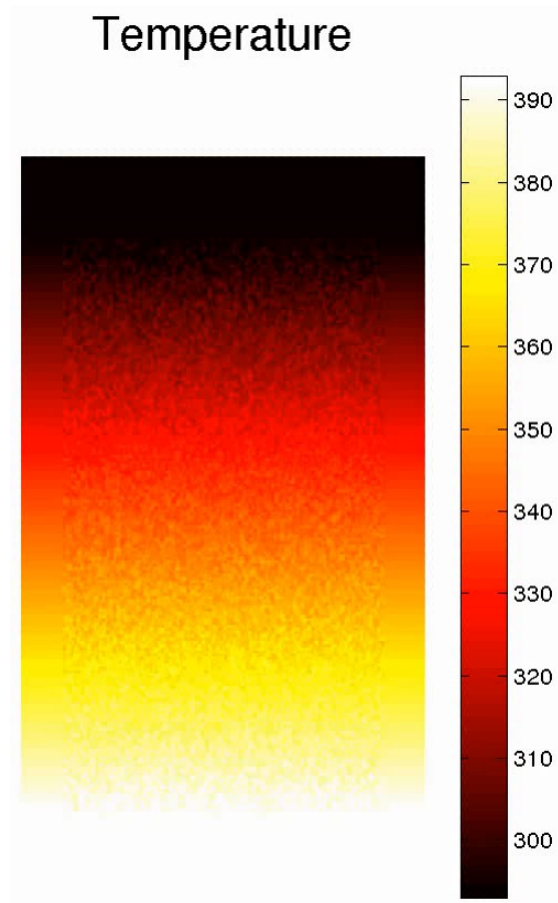
cold

gravity





Case: Enclosed, tight water-filled kettle on the stove



Case: enclosed “kettle” on the stove with space-dependent heating at the walls (linearly decreasing towards the top).

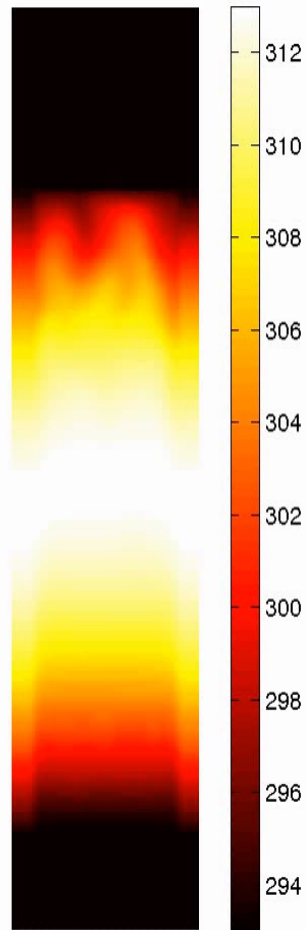
Question 1: Does the schematic on stable vs unstable configuration explain what happens here?

Question 2: Does a steady state solution exist when time \rightarrow infinity?



Case: Enclosed furnace with space-dependent wall heating

Temperature



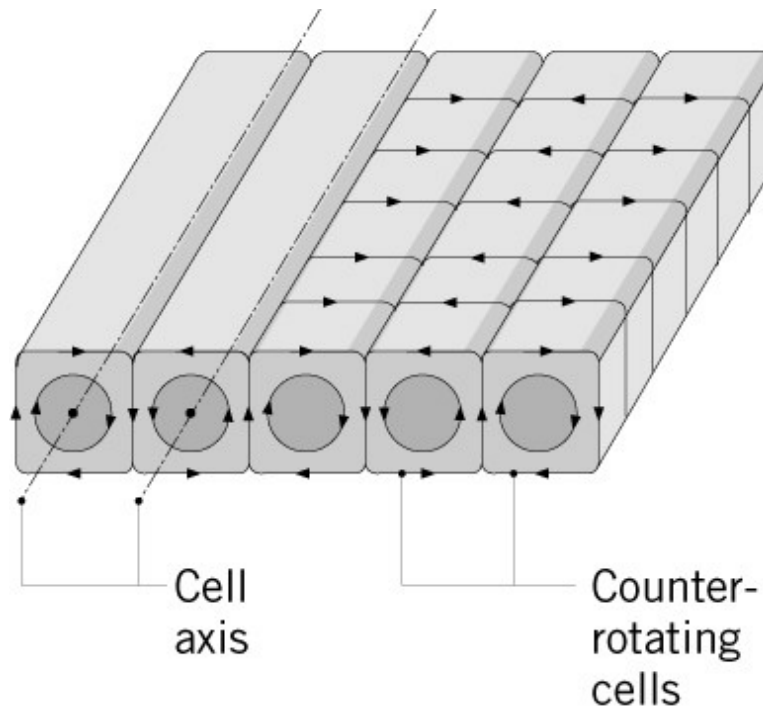
Recall some previous slides:
Stable vs unstable configuration

Case: enclosed “furnace” with space-dependent heating at the walls (cold at top and bottom parts, hot in the center).

Question: Does the schematic picture from the previous slide (stable vs unstable configuration) explain what happens?

Enclosed cavities, heating from below

<https://www.youtube.com/watch?v=OM0I2YPVMf8>
<https://www.youtube.com/watch?v=jFI5KaAqfXI>



$$Ra < Ra_c = 1708$$

$$\bar{Nu}_L = \frac{\bar{h}L}{k} = 1$$

Case 2: Thermally unstable but regular cell patterns

$$1708 < Ra_L < 5 \cdot 10^4$$

Case 3: Flow is turbulent

$$3 \cdot 10^5 < Ra_L < 7 \cdot 10^9$$

<https://www.youtube.com/watch?v=gSTNxS96fRg&t=56s>