



Aalto University

# Basic oscillating systems

ELEC-E5610 Acoustics and the Physics of Sound

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# 1

# Basic concepts

# 1 Definition of degrees of freedom

## DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

“The smallest number of independent variables required for describing the motion of a system”.



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## DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

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Examples:



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## DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

“The smallest number of independent variables required for describing the motion of a system”.

Examples:

- electrical LC-circuit  $\Rightarrow$  one degree of freedom (1DOF)



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## DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

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Examples:

- electrical LC-circuit  $\Rightarrow$  one degree of freedom (1DOF)
- rectilinear motion + rotation around axis  $\Rightarrow$  2DOF



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## DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

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Examples:

- electrical LC-circuit  $\Rightarrow$  one degree of freedom (1DOF)
- rectilinear motion + rotation around axis  $\Rightarrow$  2DOF
- free motion + rotation in 3D  $\Rightarrow$  6DOF



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## DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

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Examples:

- electrical LC-circuit  $\Rightarrow$  one degree of freedom (1DOF)
- rectilinear motion + rotation around axis  $\Rightarrow$  2DOF
- free motion + rotation in 3D  $\Rightarrow$  6DOF

A finite number of DOFs a simplification of real-world phenomena.





# 1 Systems With multiple degrees of freedom (MDOF)

DOFs

MDOF systems

MDOF systems are more complex to analyze

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study



# 1 Systems With multiple degrees of freedom (MDOF)

DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

MDOF systems are more complex to analyze

- motion not restricted to a path representable by a single quantity



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DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

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- motion not restricted to a path representable by a single quantity
- multiple interconnected masses



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DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

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- number of DOFs = number of eigenfrequencies (or resonance peaks)



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DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

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DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

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- multiple interconnected masses
- number of DOFs = number of eigenfrequencies (or resonance peaks)
- antiresonance notches between resonance peaks
- example: the double pendulum  
<http://www.youtube.com/watch?v=d2E5oojoXjk>
  - (two or more DOFs & nonlinearity  $\Rightarrow$  chaotic behavior!)



# 1 Continuums

DOFs

MDOF systems

**Continuums**

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

In reality, physical objects are not point-like, but distributed systems (at least in classical mechanics), i. e. their coordinate systems are continuous functions.



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DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

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- fluids, bars, plates, membranes, strings ...





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DOFs

MDOF systems

**Continuums**

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

In reality, physical objects are not point-like, but distributed systems (at least in classical mechanics), i. e. their coordinate systems are continuous functions.

- fluids, bars, plates, membranes, strings ...
- finite systems (e. g. a finite string) have countably infinite degrees of freedom



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DOFs

MDOF systems

**Continuums**

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

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- finite systems (e. g. a finite string) have countably infinite degrees of freedom
- infinite systems have non-countably infinite degrees of freedom



# 1 Practical simplifications

DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

Typically, some practical simplifications are made:

**Number of DOFs** : 1DOF systems are sufficiently accurate approximations of real systems, if

- the bandwidth is limited
- the eigenfrequencies are well separated in frequency

**Linearity** : it is assumed that the frequency and waveform of the vibration do not depend on amplitude

# 1 Practical simplifications II

DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

**Deterministic** : it is possible to determine the future state of a system using a “snapshot” of a previous state



# 1 A simple pendulum

DOFs

MDOF systems

Continuums

Simplifications

**Pendulum**

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

## A simple pendulum

- small angles: period is  $t = \sqrt{l/g}$ ,  $l$  is string length,  $g$  is acceleration of gravity



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DOFs

MDOF systems

Continuums

Simplifications

**Pendulum**

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

## A simple pendulum

- small angles: period is  $t = \sqrt{l/g}$ ,  $l$  is string length,  $g$  is acceleration of gravity
- planar motion: easily predictable motion as a function of time



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DOFs

MDOF systems

Continuums

Simplifications

**Pendulum**

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

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DOFs

MDOF systems

Continuums

Simplifications

**Pendulum**

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

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- planar motion: easily predictable motion as a function of time
- free motion: difficult to control the transversal motion, external excitation  $\Rightarrow$  chaotic motion
- large angles: period depends on amplitude (nonlinearity)





# 1 Forced vibration at resonance frequency

DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

**Forced vibration**

Eigenfrequencies

Eigenmodes

Case study

Forced vibration at the resonance frequency (R&F p.3-21):

- the relation between the magnitudes of response and excitation is in its local frequency maximum



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DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

**Forced vibration**

Eigenfrequencies

Eigenmodes

Case study

Forced vibration at the resonance frequency (R&F p.3-21):

- the relation between the magnitudes of response and excitation is in its local frequency maximum
- displacement, velocity, and acceleration typically are in different phases



# 1 Eigenfrequencies

- DOFs
- MDOF systems
- Continuums
- Simplifications
- Pendulum
- Resonance
- Forced vibration
- Eigenfrequencies**
- Eigenmodes
- Case study

The set of frequencies that the system can freely vibrate in are called **eigenfrequencies** of the system (Germ. “*eigen*”, own)

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- DOFs
- MDOF systems
- Continuums
- Simplifications
- Pendulum
- Resonance
- Forced vibration
- Eigenfrequencies**
- Eigenmodes
- Case study

The set of frequencies that the system can freely vibrate in are called **eigenfrequencies** of the system (Germ. “*eigen*”, own)

- corresponds to the eigenvalues of the set of equations that determine the system's behavior

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DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

**Eigenfrequencies**

Eigenmodes

Case study

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- eigenfrequency  $\neq$  resonance frequency !

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DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

**Eigenfrequencies**

Eigenmodes

Case study

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DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

**Eigenfrequencies**

Eigenmodes

Case study

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After a transient excitation, a system will vibrate at its eigenfrequencies.

# 1 Eigenmodes

- DOFs
- MDOF systems
- Continuums
- Simplifications
- Pendulum
- Resonance
- Forced vibration
- Eigenfrequencies
- Eigenmodes**
- Case study

Each eigenfrequency corresponds to a certain shape of vibration, called **eigenmode**.

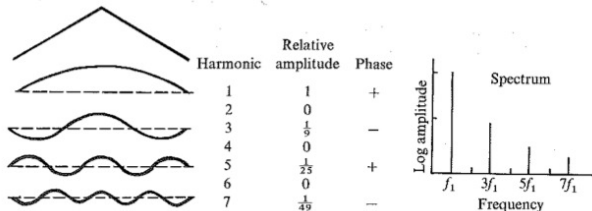


Fig. 2.5. Frequency analysis of a string plucked at its center. Odd-numbered modes of vibration add up in appropriate amplitude and phase to give the shape of the string.

**Figure:** Vibrational modes of a plucked string, R&F p. 39



# 1 Case study: 1DOF system

DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

Let's study a mass-spring oscillator.  
Two forces acting on the mass are:



# 1 Case study: 1DOF system

DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

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DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

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where  $K$  is the spring constant,  $x$  is displacement, and  $\ddot{x}$  is acceleration.

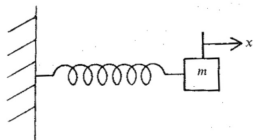


Fig. 1.1. Simple mass-spring vibrating system.

# 1 Case study: 1DOF system

DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

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$$m\ddot{x} + Kx = 0$$

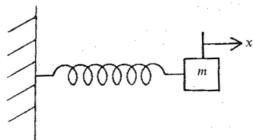


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DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

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$$m\ddot{x} + Kx = 0 \quad \Rightarrow \quad \ddot{x} + \omega_0^2 x = 0, \quad \text{where } \omega_0 = \sqrt{K/m}. \quad (1)$$

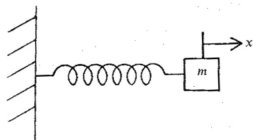


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DOFs

MDOF systems

Continuums

Simplifications

Pendulum

Resonance

Forced vibration

Eigenfrequencies

Eigenmodes

Case study

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$$m\ddot{x} + Kx = 0 \Rightarrow \ddot{x} + \omega_0^2 x = 0, \text{ where } \omega_0 = \sqrt{K/m}. \quad (1)$$

A general solution to the motion equation (1) is  
 $x = A \cos(\omega_0 t + \phi)$ , where  $\omega_0$  is the eigenfrequency (rad/s).

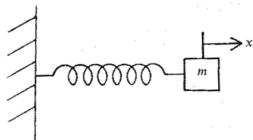


Fig. 1.1. Simple mass-spring vibrating system.

# 2

## Complex representation



## 2 Complex exponential representation

### FF appendix 1

Complex  
representation

1DOF

Why complex  
numbers?

Harmonic vibration has the general form:

$$f(t) = A \cos(\omega t + \phi), \quad (2)$$

where  $A$  is amplitude,  $t$  is time,  $\omega$  is angular frequency, and  $\phi$  is angle.





## 2 Complex exponential representation

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1DOF

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$$e^{ix} = \cos x + i \sin x,$$



## 2 Complex exponential representation

### FF appendix 1

#### Complex representation

1DOF

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where  $A$  is amplitude,  $t$  is time,  $\omega$  is angular frequency, and  $\phi$  is angle. Let's remind us of Euler's formula:

$$e^{ix} = \cos x + i \sin x,$$

and interpret Eq. (2) as the real part of an exponential function:

$$f(t) = \operatorname{Re}\{Ae^{i(\omega t + \phi)}\} = \operatorname{Re}\{Ae^{i\phi} e^{i\omega t}\}. \quad (3)$$

Next, we will define a complex amplitude  $\tilde{A} = Ae^{i\phi}$

Complex  
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1DOF

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Next, we will define a complex amplitude  $\tilde{A} = Ae^{i\phi}$ , so that harmonic vibration can be given as

$$f(t) = \text{Re}\{\tilde{A}e^{i(\omega t)}\}. \quad (4)$$

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Graphic representation is a rotating phasor:

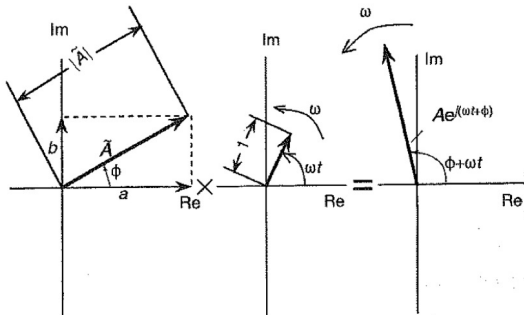


Fig. A1.1 Complex exponential representation of harmonic signals by phasors.

## Interpretation:

- the projection of this rotating vector on the real axis denotes the state at each time instant
- Java-applet: [https://ngsir.netfirms.com/j/Eng/springSHM/springSHM\\_js.htm](https://ngsir.netfirms.com/j/Eng/springSHM/springSHM_js.htm)

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- superposition of harmonic signals by summing the phasors (<http://tinyurl.com/2bo7bcj>):

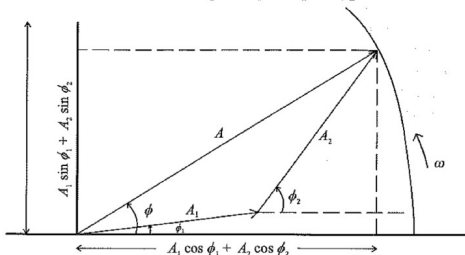


Fig. 1.4. Phasor representation of two simple harmonic motions having the same frequency.

## 2 Complex representation of a 1DOF oscillator

Complex  
representation

1DOF

Why complex  
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For the 1DOF mass-spring oscillator, the solution for the motion equation can be given using the complex notation:

$$\tilde{x} = \tilde{A}e^{i\omega_0 t} \quad (5)$$

for the displacement.



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for the displacement. By differentiating Eq. (5) w. r. t. time, we obtain the complex velocity

$$\tilde{v} = \dot{\tilde{x}} = i\omega_0 \tilde{A}e^{i\omega_0 t}$$



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representation

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$$\tilde{v} = \dot{\tilde{x}} = i\omega_0 \tilde{A}e^{i\omega_0 t}$$

and acceleration

$$\tilde{a} = \dot{\tilde{v}} = \ddot{\tilde{x}} = -\omega_0^2 \tilde{A}e^{i\omega_0 t}$$

## 2 Why complex numbers?

Complex  
representation

1DOF

Why complex  
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“What do you mean? How can velocity be complex?”



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1DOF

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- remember: the physical values are obtained as the real parts of these complex numbers



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1DOF

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- it's more convenient to calculate using the complex notation (compared to trigonometry)



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1DOF

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“What do you mean? How can velocity be complex?”

- remember: the physical values are obtained as the real parts of these complex numbers
- it's more convenient to calculate using the complex notation (compared to trigonometry)
- if only linear operations are used, the real part may be taken only from the final result
  - otherwise the real parts should be taken at each step



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1DOF

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“What do you mean? How can velocity be complex?”

- remember: the physical values are obtained as the real parts of these complex numbers
- it's more convenient to calculate using the complex notation (compared to trigonometry)
- if only linear operations are used, the real part may be taken only from the final result
  - otherwise the real parts should be taken at each step
- the  $\text{Re}\{\}$ -operator is often left unwritten in the literature



# 3

## Lossy 1DOF systems





# 3 Modelling of losses

## Modelling of losses

Solution

Plot of the solution

Time constant and Q

Forced vibration in  
1DOF system

Graphic interpretation

Combinations of  
springs and masses

Accurate modelling of real losses is difficult.



# 3 Modelling of losses

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- simplification: consider only viscous losses



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Accurate modelling of real losses is difficult.

- simplification: consider only viscous losses
- remember the motion equation (1) for the mass-spring oscillator

$$m\ddot{x} + Kx = 0 \tag{6}$$

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Accurate modelling of real losses is difficult.

- simplification: consider only viscous losses
- remember the motion equation (1) for the mass-spring oscillator
- viscous losses result in an additional velocity-dependent term in the motion equation

$$m\ddot{x} + R_m\dot{x} + Kx = 0 \tag{6}$$

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- simplification: consider only viscous losses
- remember the motion equation (1) for the mass-spring oscillator
- viscous losses result in an additional velocity-dependent term in the motion equation
- next, define  $\alpha = \frac{R_m}{2m}$  (in addition to  $\omega_0 = \sqrt{K/m}$ )

$$\begin{aligned} m\ddot{x} + R_m\dot{x} + Kx &= 0 \\ \Rightarrow \ddot{x} + 2\alpha\dot{x} + \omega_0^2x &= 0 \end{aligned} \tag{6}$$

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- viscous losses result in an additional velocity-dependent term in the motion equation
- next, define  $\alpha = \frac{R_m}{2m}$  (in addition to  $\omega_0 = \sqrt{K/m}$ )
- $\Rightarrow$  the motion equation of a damped 1DOF oscillator

$$\begin{aligned} m\ddot{x} + R_m\dot{x} + Kx &= 0 \\ \Rightarrow \ddot{x} + 2\alpha\dot{x} + \omega_0^2x &= 0 \end{aligned} \tag{6}$$

# 3 Solution to the lossy equation of motion

Modelling of losses

**Solution**

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The solution to Eq. (6) for displacement (R&F p.10-11):

$$x = e^{-\alpha t} \cos(\omega_d t + \phi) \quad (7)$$



# 3 Solution to the lossy equation of motion

Modelling of losses

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1DOF system

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The solution to Eq. (6) for displacement (R&F p.10-11):

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- $e^{-\alpha t}$  denotes the damping oscillation





# 3 Solution to the lossy equation of motion

Modelling of losses

**Solution**

Plot of the solution

Time constant and Q

Forced vibration in  
1DOF system

Graphic interpretation

Combinations of  
springs and masses

The solution to Eq. (6) for displacement (R&F p.10-11):

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1DOF system

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1DOF system

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### 3 Plot of the solution

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Solution

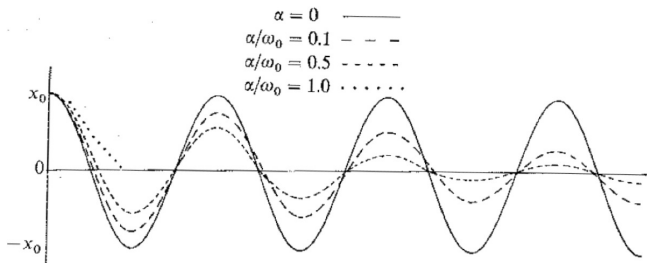
Plot of the solution

Time constant and Q

Forced vibration in 1DOF system

Graphic interpretation

Combinations of springs and masses



**Figure:** Plot of the damped oscillator vibration with different values of  $\alpha$  R&F p.11.

### 3 Plot of the solution

Modelling of losses

Solution

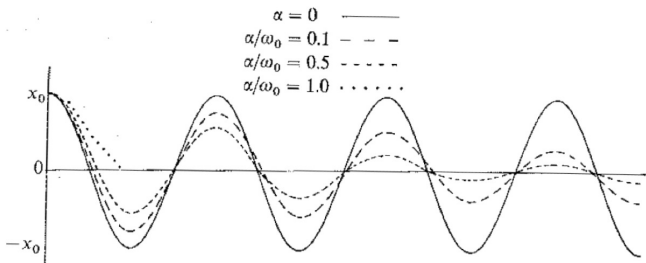
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Time constant and Q

Forced vibration in  
1DOF system

Graphic interpretation

Combinations of  
springs and masses



**Figure:** Plot of the damped oscillator vibration with different values of  $\alpha$  R&F p.11.

■  $\alpha = 0 \Rightarrow$  eternal vibration

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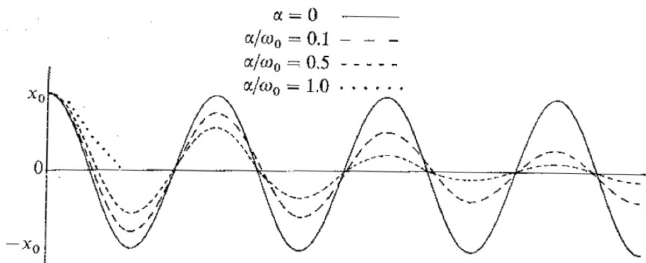
Plot of the solution

Time constant and Q

Forced vibration in 1DOF system

Graphic interpretation

Combinations of springs and masses



**Figure:** Plot of the damped oscillator vibration with different values of  $\alpha$  R&F p.11.

- $\alpha = 0 \Rightarrow$  eternal vibration
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Modelling of losses

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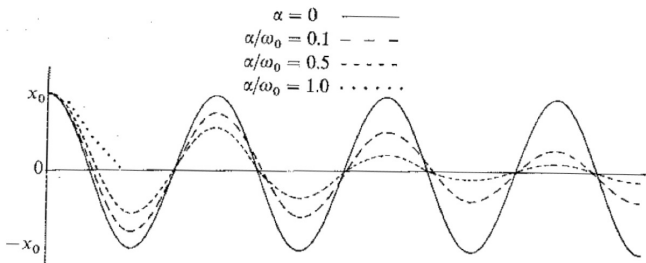
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Time constant and Q

Forced vibration in  
1DOF system

Graphic interpretation

Combinations of  
springs and masses



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- $\alpha = 0 \Rightarrow$  eternal vibration
- $0 < \alpha/\omega_0 < 1 \Rightarrow$  attenuating vibration
- $\alpha/\omega_0 = 1 \Rightarrow$  critical attenuation (no vibration)

# 3 Time constant and quality factor

Modelling of losses  
Solution  
Plot of the solution

Two important numbers for damped oscillators:

## Time constant and Q

Forced vibration in  
1DOF system  
Graphic interpretation

Combinations of  
springs and masses





### 3 Time constant and quality factor

Modelling of losses  
Solution  
Plot of the solution

#### Time constant and Q

Forced vibration in  
1DOF system  
Graphic interpretation  
Combinations of  
springs and masses

Two important numbers for damped oscillators:

**time constant**  $\tau = 1/\alpha = 2m/R_m$  is the time it takes for the oscillation to attenuate to  $1/e$  relative to the initial state



# 3 Time constant and quality factor

Modelling of losses  
Solution  
Plot of the solution

## Time constant and Q

Forced vibration in  
1DOF system  
Graphic interpretation  
Combinations of  
springs and masses

Two important numbers for damped oscillators:

**time constant**  $\tau = 1/\alpha = 2m/R_m$  is the time it takes for the oscillation to attenuate to  $1/e$  relative to the initial state

**quality factor**  $Q = \frac{K}{R_m\omega_0} = \frac{\omega_0}{2\alpha}$  denotes the sharpness of the resonance peak. The higher the  $Q$ , the sharper the resonance.



# 3 Forced vibration in 1DOF system

Modelling of losses

Solution

Plot of the solution

Time constant and Q

**Forced vibration in  
1DOF system**

Graphic interpretation

Combinations of  
springs and masses

Let's add an external excitation force to the motion equation of the oscillator and study the response.



# 3 Forced vibration in 1DOF system

Modelling of losses

Solution

Plot of the solution

Time constant and Q

**Forced vibration in 1DOF system**

Graphic interpretation

Combinations of springs and masses

Let's add an external excitation force to the motion equation of the oscillator and study the response. Recall Eq. (6)

$$m\ddot{x} + R_m\dot{x} + Kx = 0$$

## 3 Forced vibration in 1DOF system

Modelling of losses

Solution

Plot of the solution

Time constant and Q

Forced vibration in  
1DOF system

Graphic interpretation

Combinations of  
springs and masses

Let's add an external excitation force to the motion equation of the oscillator and study the response. Recall Eq. (6) and add  $f(t)$  to the RHS.

$$m\ddot{x} + R_m\dot{x} + Kx = f(t)$$



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Modelling of losses

Solution

Plot of the solution

Time constant and Q

Forced vibration in 1DOF system

Graphic interpretation

Combinations of springs and masses

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$$m\ddot{x} + R_m\dot{x} + Kx = f(t)$$

if the excitation is sinusoidal  $f(t) = \text{Re}\{\tilde{F}\} = \text{Re}\{Fe^{i\omega t}\}$ :

$$\tilde{x} = \frac{\tilde{F}/m}{\omega_0^2 - \omega^2 + i\omega 2\alpha} \quad (\text{R\&F:(1.60)})$$

$$\tilde{v} = \frac{\tilde{F}\omega/m}{2\omega\alpha + i(\omega^2 - \omega_0^2)} \quad (\text{R\&F:(1.61)})$$



By dividing Eqs. (R&F:(1.60) and (1.61)) with  $\tilde{F}$  and taking the absolute value, one obtains the response of displacement and velocity for a constant force excitation as a function of frequency:

$$\frac{|\tilde{x}|}{|\tilde{F}|} = \frac{1}{\sqrt{(K - \omega^2 m)^2 + (\omega R)^2}}$$

$$\frac{|\tilde{v}|}{|\tilde{F}|} = \frac{1}{\sqrt{(\omega m - K/\omega)^2 + R^2}}$$

Modelling of losses

Solution

Plot of the solution

Time constant and Q

Forced vibration in  
1DOF system

Graphic interpretation

Combinations of  
springs and masses

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...these may be interpreted as **the transfer functions between input force and resulting displacement (or velocity)!**

Modelling of losses

Solution

Plot of the solution

Time constant and Q

Forced vibration in 1DOF system

Graphic interpretation

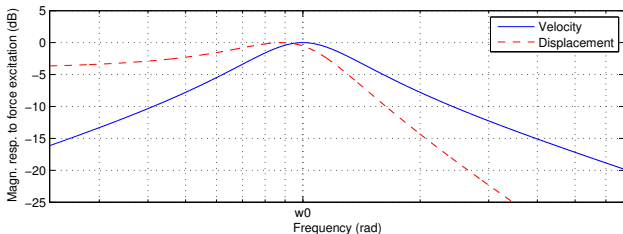
Combinations of springs and masses





# 3 Graphic interpretation

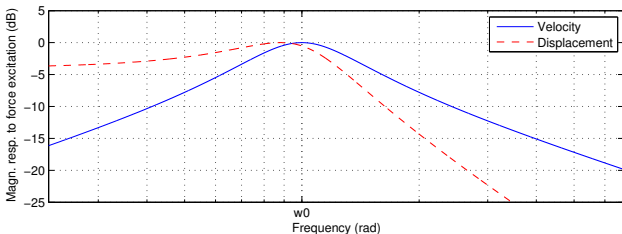
Transfer functions for force input as a function of frequency:



- Modelling of losses
- Solution
- Plot of the solution
- Time constant and Q
- Forced vibration in 1DOF system
- Graphic interpretation**
- Combinations of springs and masses

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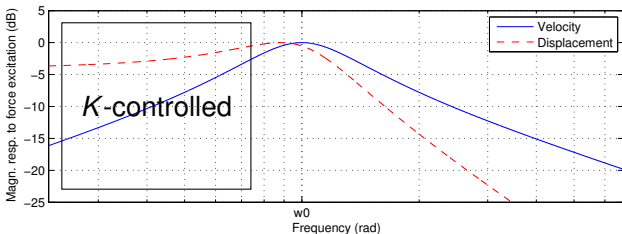
Transfer functions for force input as a function of frequency:



$$\Rightarrow \frac{|\tilde{X}|}{|\tilde{F}|} = \frac{1}{\sqrt{(\omega_0^2 m - \omega^2 m)^2 + (\omega R)^2}},$$

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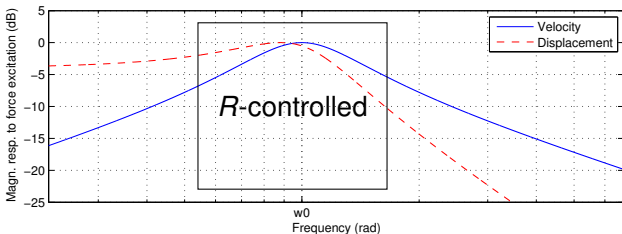
Transfer functions for force input as a function of frequency:



$$\Rightarrow \frac{|\tilde{x}|}{|\tilde{F}|} = \frac{1}{\sqrt{(\omega_0^2 m - \omega^2 m)^2 + (\omega R)^2}}, \quad \frac{|\tilde{x}|}{|\tilde{F}|} \approx \begin{cases} \frac{1}{K} & \text{if } \omega \ll \omega_0, \\ \frac{1}{\omega R} & \text{if } \omega \approx \omega_0, \\ \frac{1}{\omega^2 m} & \text{if } \omega \gg \omega_0 \end{cases}$$

### 3 Graphic interpretation

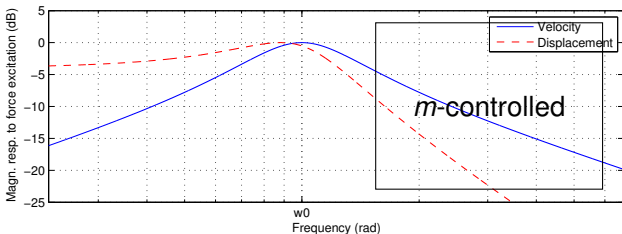
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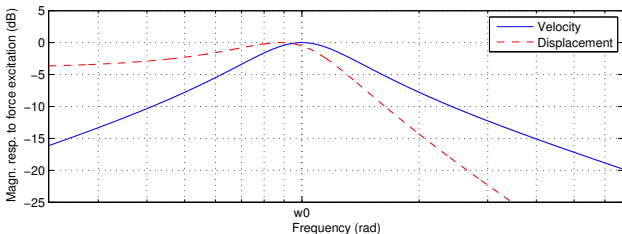
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# 3 Combinations of springs and masses

Modelling of losses

Solution

Plot of the solution

Time constant and Q

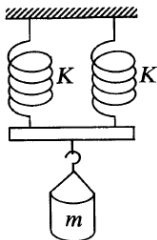
Forced vibration in 1DOF system

Graphic interpretation

Combinations of springs and masses



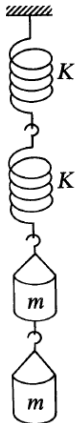
(a)



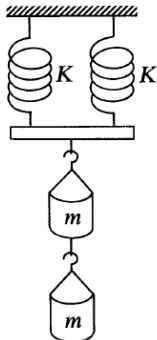
(b)



(c)



(d)



(e)