



Aalto University  
School of Engineering

# Comfortable and Healthy Indoor Climate

## **EEN-E4001**

Lecture 3: Thermal comfort

Risto Kosonen

# Learning outcomes

- Understanding of factors affecting thermal comfort
- Understanding what is the whole body thermal sensation
- Understanding what is local thermal discomfort

# THERMAL COMFORT

**„state of mind which expresses satisfaction with the thermal environment“**

(ASHRAE)



# Thermal Comfort

- Thermal conditions within living and working environments play a critical role in influencing occupant comfort and wellbeing.
- Research has shown that along with air quality, thermal comfort is one of the critical variables influencing worker productivity.
- **Man is in thermal balance when the internal heat production is equal the heat loss.**

# ANALYSIS OF THERMAL COMFORT

- **Evaluation of thermal sensation in field with surveys**
- **Modelling heat exchange between the human body and the environment**

ISO 7730 & ASHRAE 55/1994

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# Short discussion

How the heat transfer from body happens ?

# Heat Transfer and Thermal Comfort

- Maintenance of thermal balance (heat production = heat loss) is an essential factor of human thermal sensation in all conditions.
- Thermal balance is affected by
  - Sensible heat transfer (dry)
  - Latent heat transfer (wet)





# Globe Temperature (GT)

- **The mean radiant temperature (MRT) can be measured using a black-globe thermometer.**
- The globe can in theory have any diameter but as the formulae used in the calculation of the mean radiant temperature depend on the diameter of the globe, a diameter of 0.15 metres, specified for use with these formula, is generally recommended.
- The surface of the globe shall be darkened, by means of a layer of matte black paint.

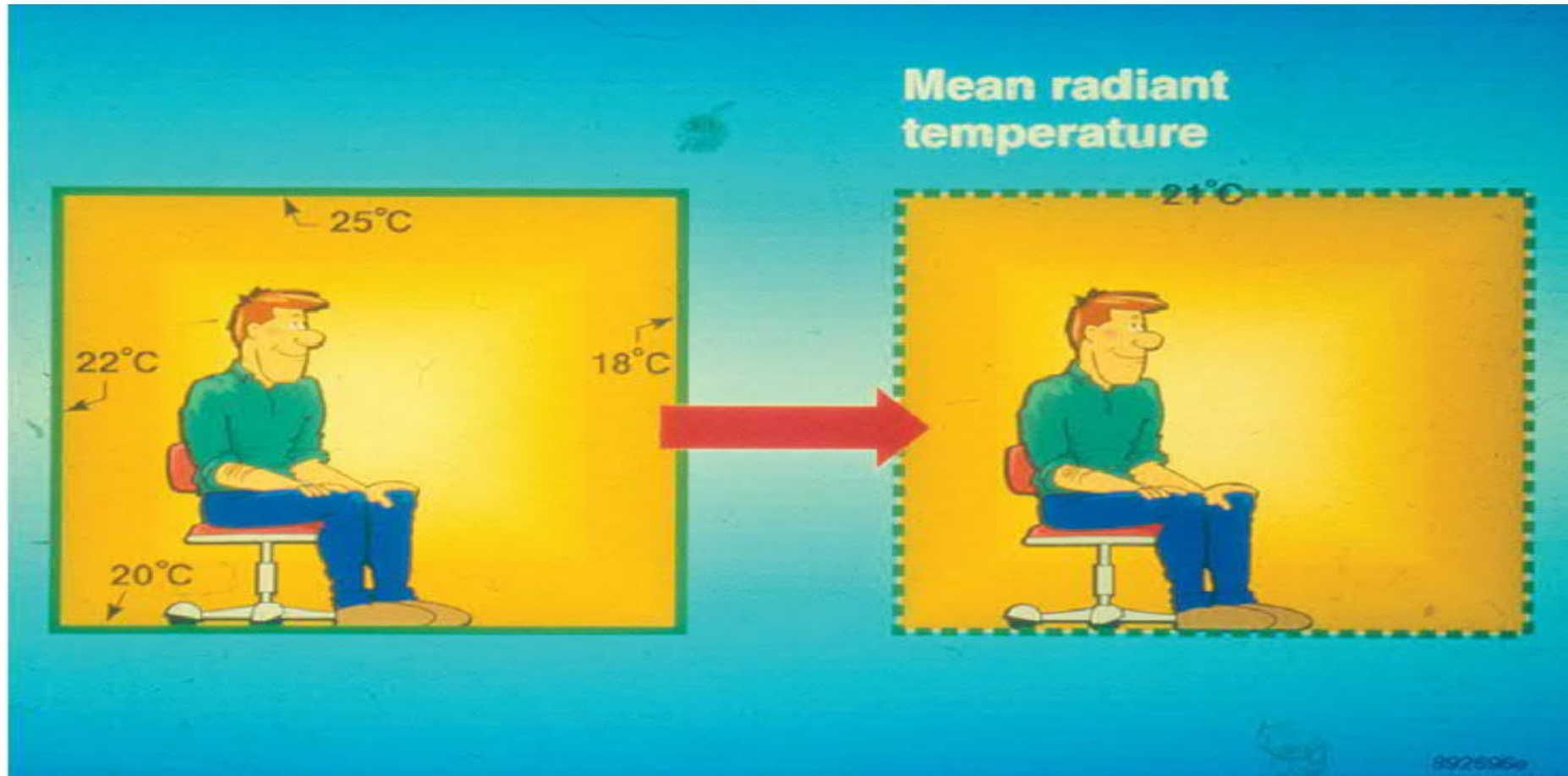


# Mean Radiant Temperature (MRT)

$$MRT = \left[ (GT + 273)^4 + 2,5 \cdot 10^8 \cdot v_a^{0,6} (GT - T_a) \right]^{1/4} - 273$$

- where:
  - MRT is the mean radiant temperature ( $^{\circ}$  C);
  - GT is the globe temperature ( $^{\circ}$  C);
  - $v_a$  is the air velocity at the level of the globe (m/s);
  - $T_a$  is air temperature ( $^{\circ}$  C).

# Mean Radiant Temperature



# Radiant Temperature

Mean radiant temperature ( $t_{mr}$ ) is defined as a uniform surface temperature of an enclosure in which an occupant would exchange the same amount of radiant heat as in the actual non-uniform enclosure.

$$t_{mr} = t_1 F_{p1} + t_2 F_{p2} + \dots + t_n F_{pn} / (F_{p1} + F_{p2} + \dots + F_{pn})$$

where  $F_{pn}$  is an angle factor between a person and a surface  $n$

$$\text{or } t_{mr} = t_1 A_1 + t_2 A_2 + \dots + t_n A_n / (A_1 + A_2 + \dots + A_n)$$

where  $A_n$  is an area of surface  $n$

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# Angle Factors

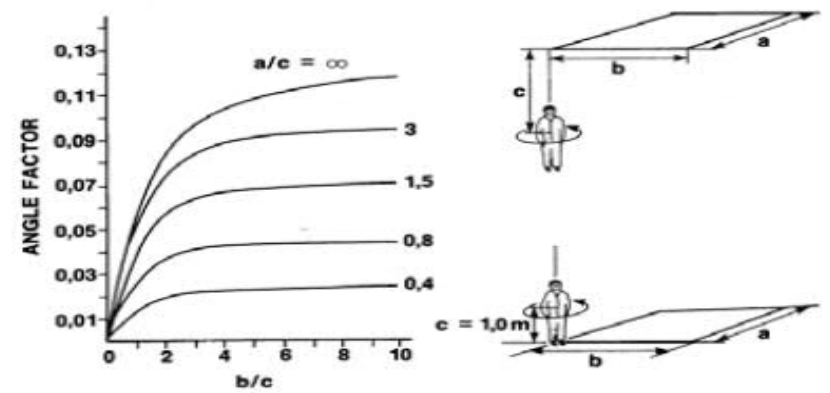
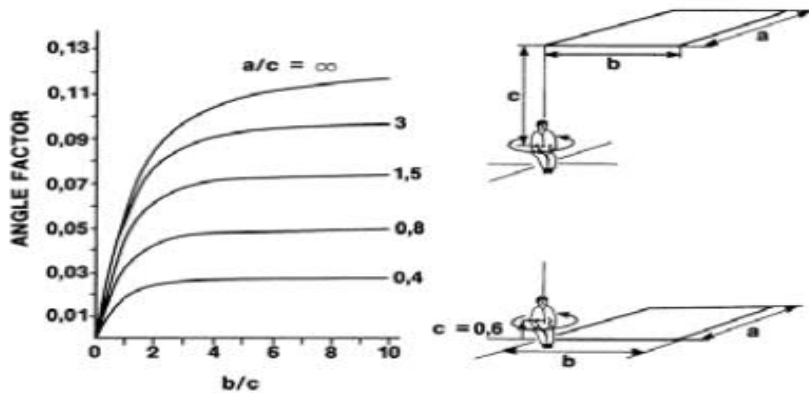
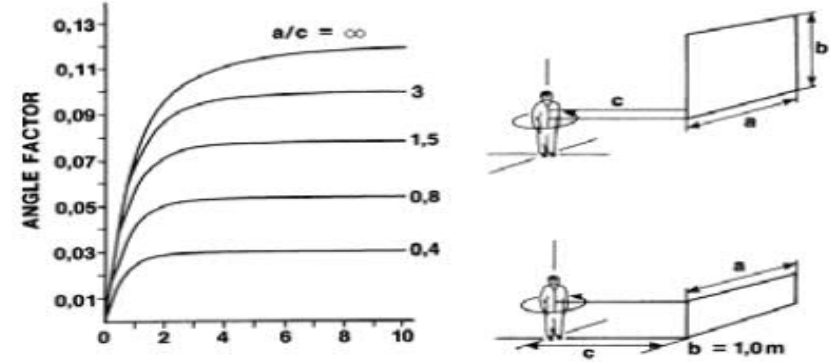
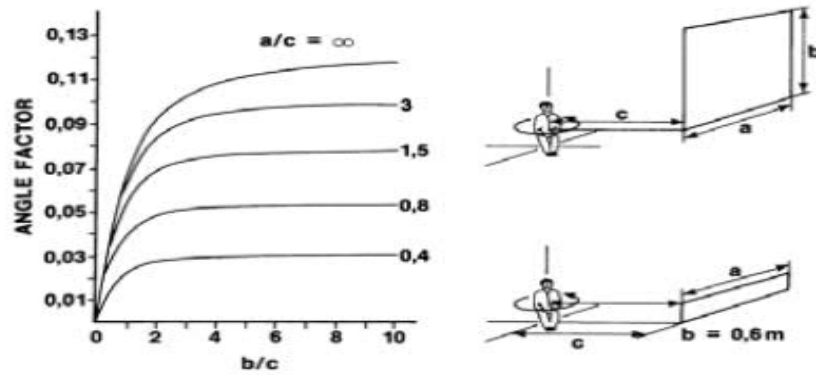


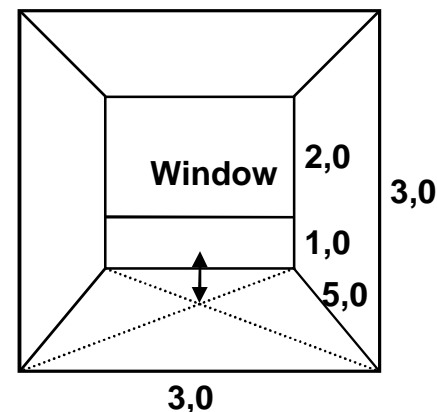
Figure 2.2 Mean value of angle factor between a seated person and a) horizontal rectangle b) vertical rectangle

Figure 2.3 mean value of angle factor between a standing person and a) horizontal rectangle b) vertical rectangle

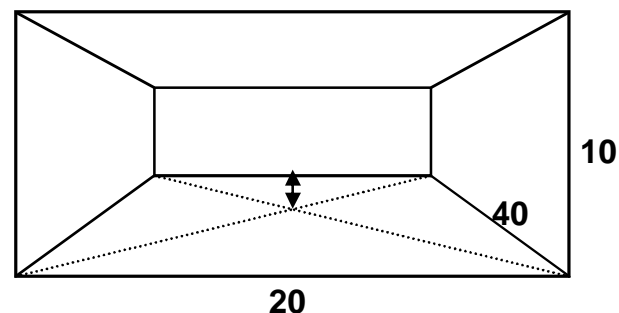
# Angle Factors – Typical Values

Surface	Angle factor $F_{p-N}$			
	office room		industrial room	
	Seated	Standing	Seated	Standing
floor	0,32	0,24	0,48	0,48
ceiling	0,12	0,12	0,22	0,22
front wall (win)	0,03	0,04	0,03	0,03
window	0,06	0,06	-	-
back wall	0,09	0,10	0,03	0,03
right side wall	0,19	0,22	0,12	0,12
left side wall	0,19	0,22	0,12	0,12

Office room



Industrial room



Source: Olesen

# Operative Temperature

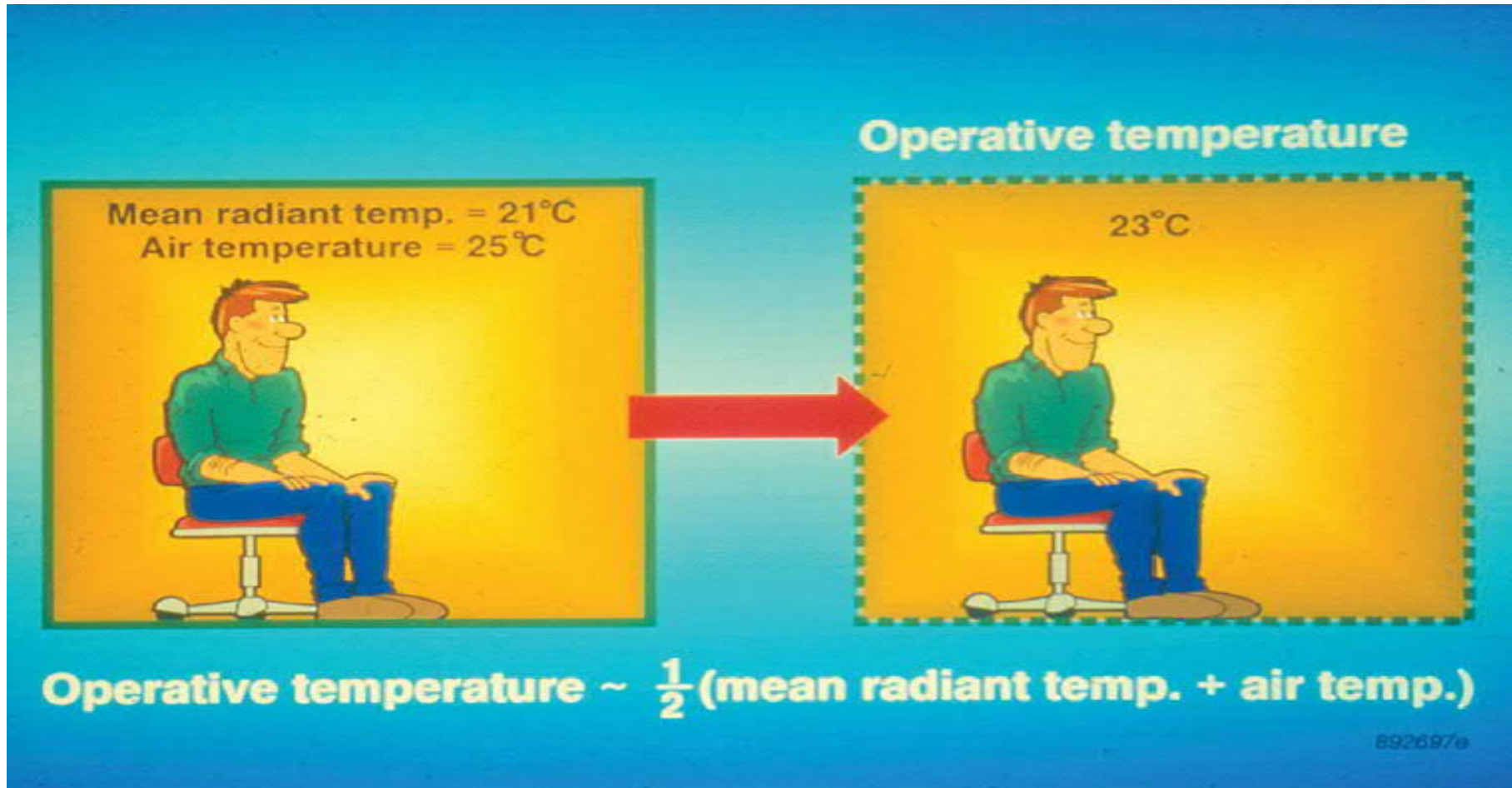
- Operative temperature can be defined as the average of the mean radiant ( $t_{mr}$ ) and dry pulp air ( $t_a$ ) temperatures

$$t_{op} = (t_{mr} + t_a) / 2$$

- Heat release of human body is 50 % of radiation and 50 % of convection.
  - Operative temperature ( $t_{op}$ ) is defined as a uniform temperature of an enclosure in which an occupant would exchange the same amount of heat by radiation plus convection as in the actual non-uniform environment.
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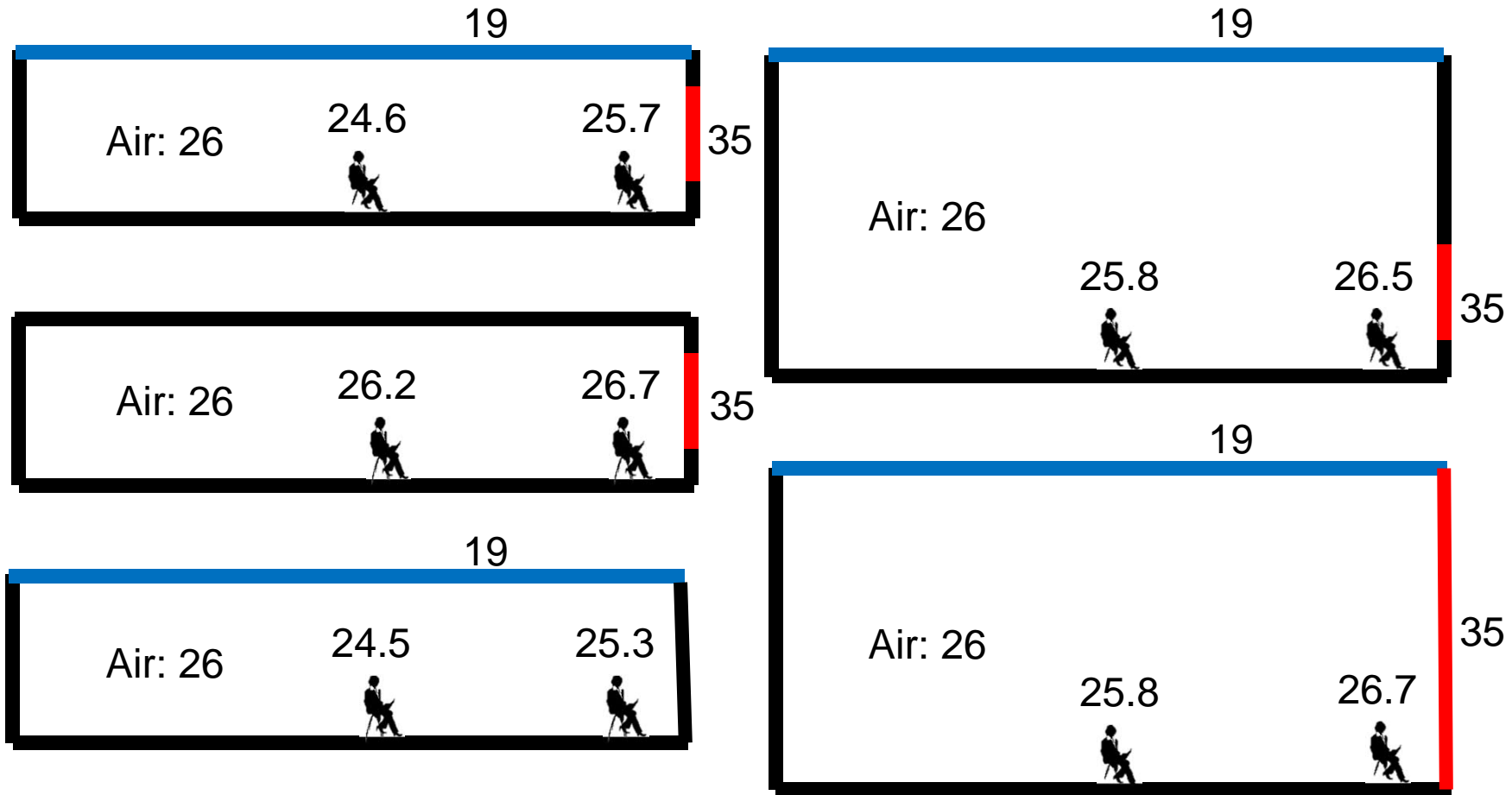


# Operative Temperature

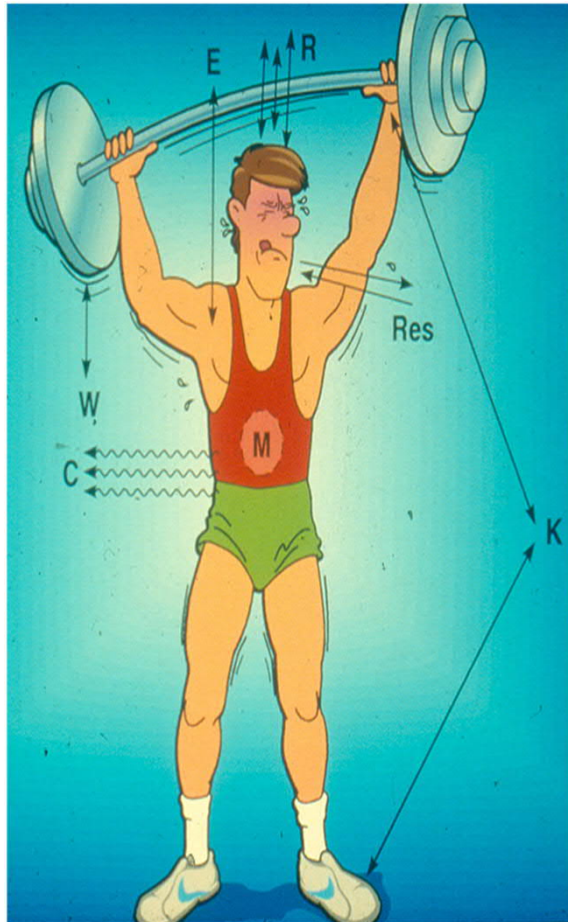




# Operative Temperature: Examples (°C)



# Human body energy balance



$$S = M \pm W \pm R \pm C \pm K - E - RES$$

- S = the rate of heat storage,
- M = the rate of metabolic heat production,
- W = the rate of mechanical work accomplished
- R = the rate of heat exchange by radiation,
- C = the rate of heat exchange by convection, K = the rate of heat exchange by conduction,
- E = the rate of heat exchange by evaporation
- RES = the rate of heat exchange by respiration.

# Short discussion

What you can do to improve your thermal sensation ?

# The Whole Body Thermal Sensation

## Factors Influencing Thermal Comfort

- **Human**
    - **Metabolic Rate**
    - **Clothing Insulation**
  - **Space**
    - **Air Temperature (Dry-Bulb)**
    - **Relative Humidity**
    - **Air Velocity**
    - **Radiation (Mean Radiant Temperature)**
-

# Thermal comfort

## I - Clothing Insulation ( $\text{m}^2 \cdot \text{K}/\text{W}$ )

1 clo =  $0,155 \text{m}^2 \cdot \text{K}/\text{W}$

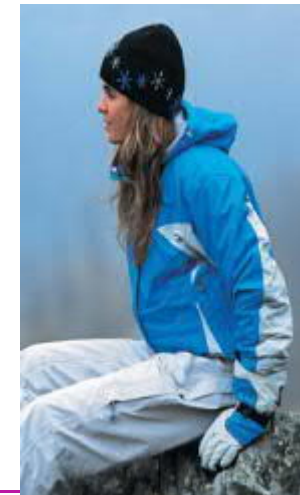


clo < 0,5

0,6-1,2



> 3,5



<b>Work clothing</b>	<b>clo</b>	<b>m<sup>2</sup>KW<sup>-1</sup>.</b>	<b>Daily wear clothing</b>	<b>clo</b>	<b>m<sup>2</sup>KW<sup>-1</sup>.</b>
<b>Underpants, boiler suit, socks, shoes</b>	0.70	0.110	Panties, T-shirt, shorts, light socks, sandals	0.30	<b>0.050</b>
<b>Underpants, shirt, boiler suit, socks, shoes</b>	0.80	0.125	Underpants, shirt with short sleeves, light trousers, light socks, shoes	0.50	<b>0.080</b>
<b>Underpants, shirt, trousers, smock, socks, shoes</b>	0.90	0.140	Panties, petticoat, stockings, dress, shoes	0.70	<b>0.105</b>
<b>Underwear with short sleeves and legs, shirt, trousers, jacket, socks, shoes</b>	1.00	0.155	Underwear, shirt, trousers, socks, shoes	0.70	<b>0.110</b>
<b>Underwear with long legs and sleeves, thermo-jacket, socks, shoes</b>	1.20	0.185	Panties, shirt, trousers, jacket, socks, shoes	1.00	<b>0.155</b>
<b>Underwear with short sleeves and legs, shirt, trousers, jacket, heavy quilted outer jacket and overalls, socks, shoes, cap, gloves</b>	1.40	0.220	Panties, stockings, blouse, long skirt, jacket, shoes	1.10	<b>0.170</b>
<b>Underwear with short sleeves and legs, shirt, trousers, jacket, heavy quilted outer jacket and overalls, socks, shoes</b>	2.00	0.310	Underwear with long sleeves and legs, shirt, trousers, V-neck sweater, jacket, socks, shoes	1.30	<b>0.200</b>
<b>Underwear with long sleeves and legs, thermo-jacket and trousers, Parka with heavy quilting, overalls with heavy quilting, socks, shoes, cap, gloves</b>	2.55	0.395	<b>Underwear with short sleeves and legs, shirt, trousers, vest, jacket, coat, socks,</b>	1.5	<b>0.230</b>

# Thermal comfort

M - Metabolic Rate ( $\text{m}^2 \cdot \text{K} / \text{W}$ )

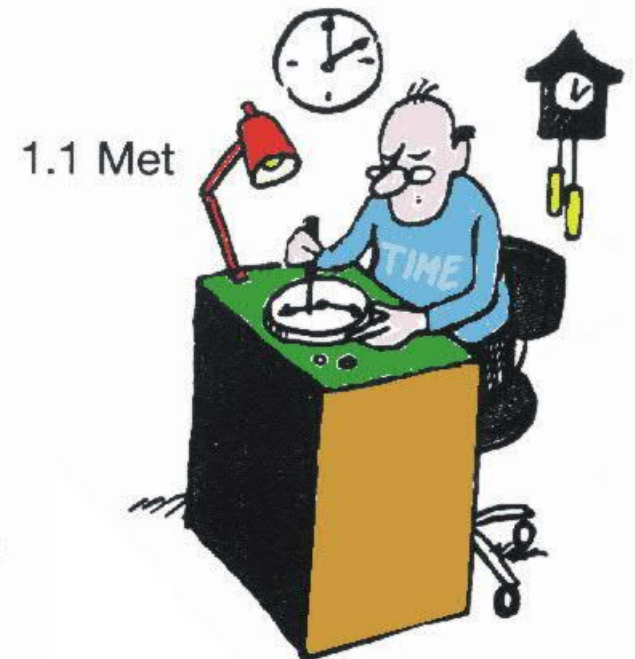
$$1\text{Met} = 58,15 \text{ W/m}^2$$



2.5 Met



6.5 Met



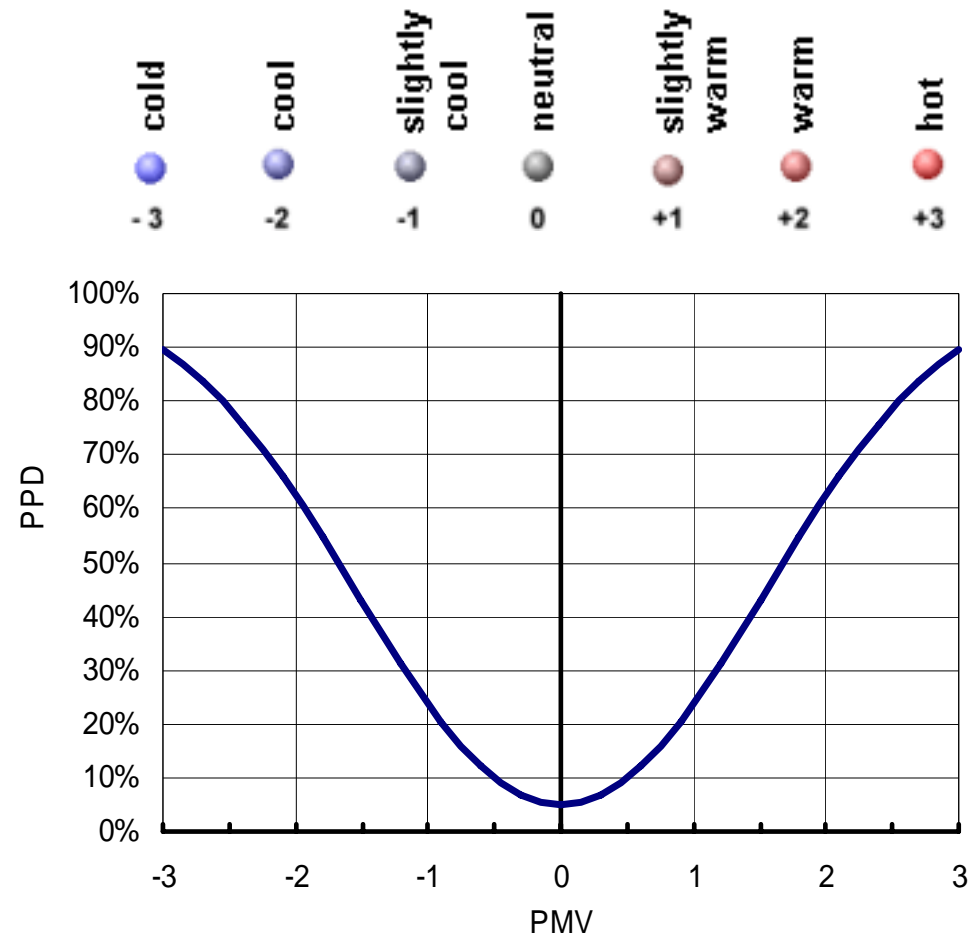
1.1 Met

<b>Activity</b>	<b>Metabolic Rate</b>	
	W/m <sup>2</sup>	met
<b>Reclining</b>	46	<b>0.8</b>
<b>Seated, relaxed</b>	58	<b>1.0</b>
<b>Sedentary activity (office, dwelling, school, laboratory)</b>	70	<b>1.2</b>
<b>Standing, light activity (shopping laboratory , light industry)</b>	93	<b>1.6</b>
<b>Standing, medium activity (Shop assistant, domestic work, machine work)</b>	116	<b>2.0</b>
<b>Walking on level ground</b>		
<b>2 km/h</b>	110	<b>1.9</b>
<b>3 km/h</b>	140	<b>2.4</b>
<b>4 km/h</b>	165	<b>2.8</b>
<b>5 km/h</b>	<b>200</b>	<b>3.4</b>

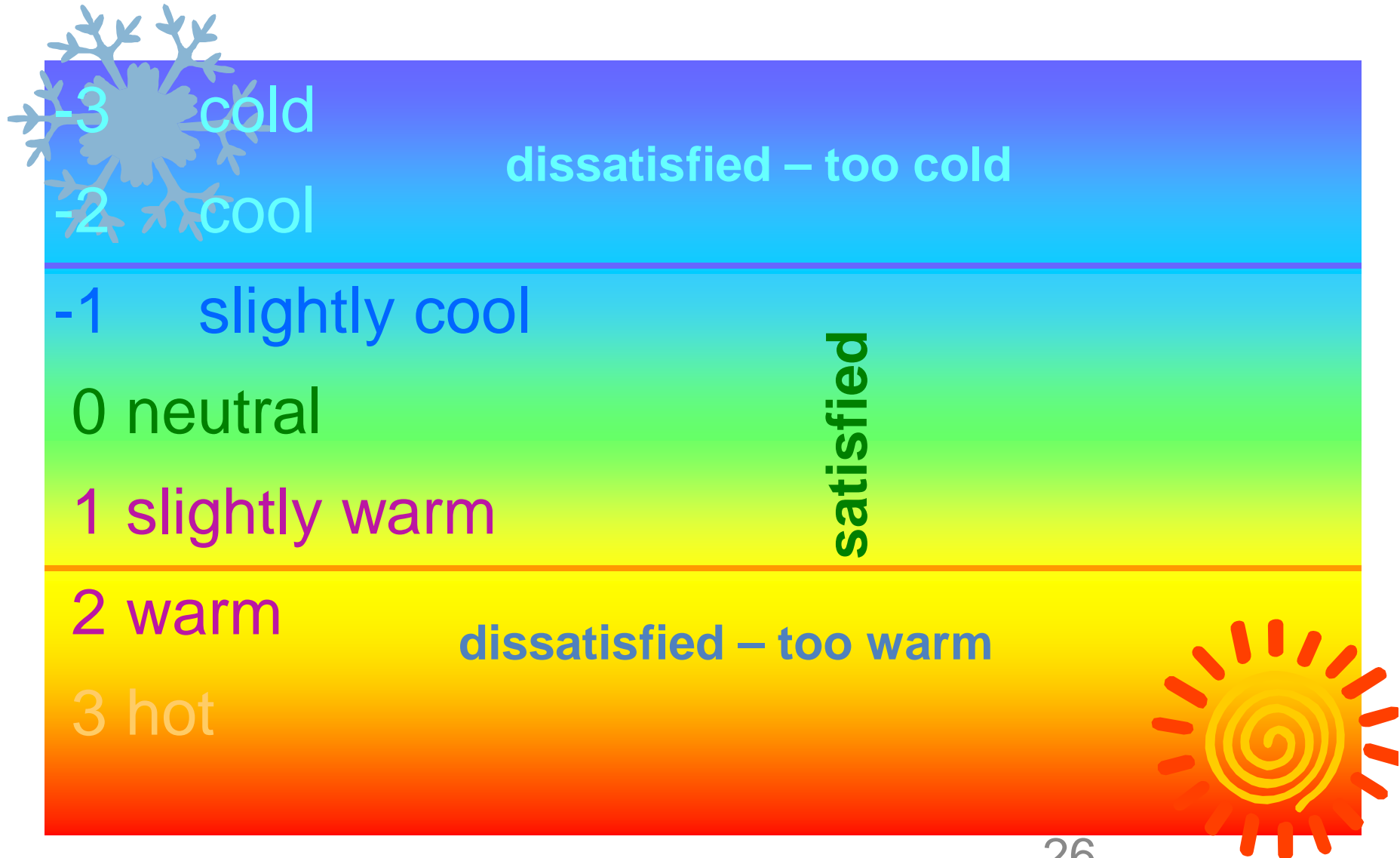


# Thermal comfort evaluation

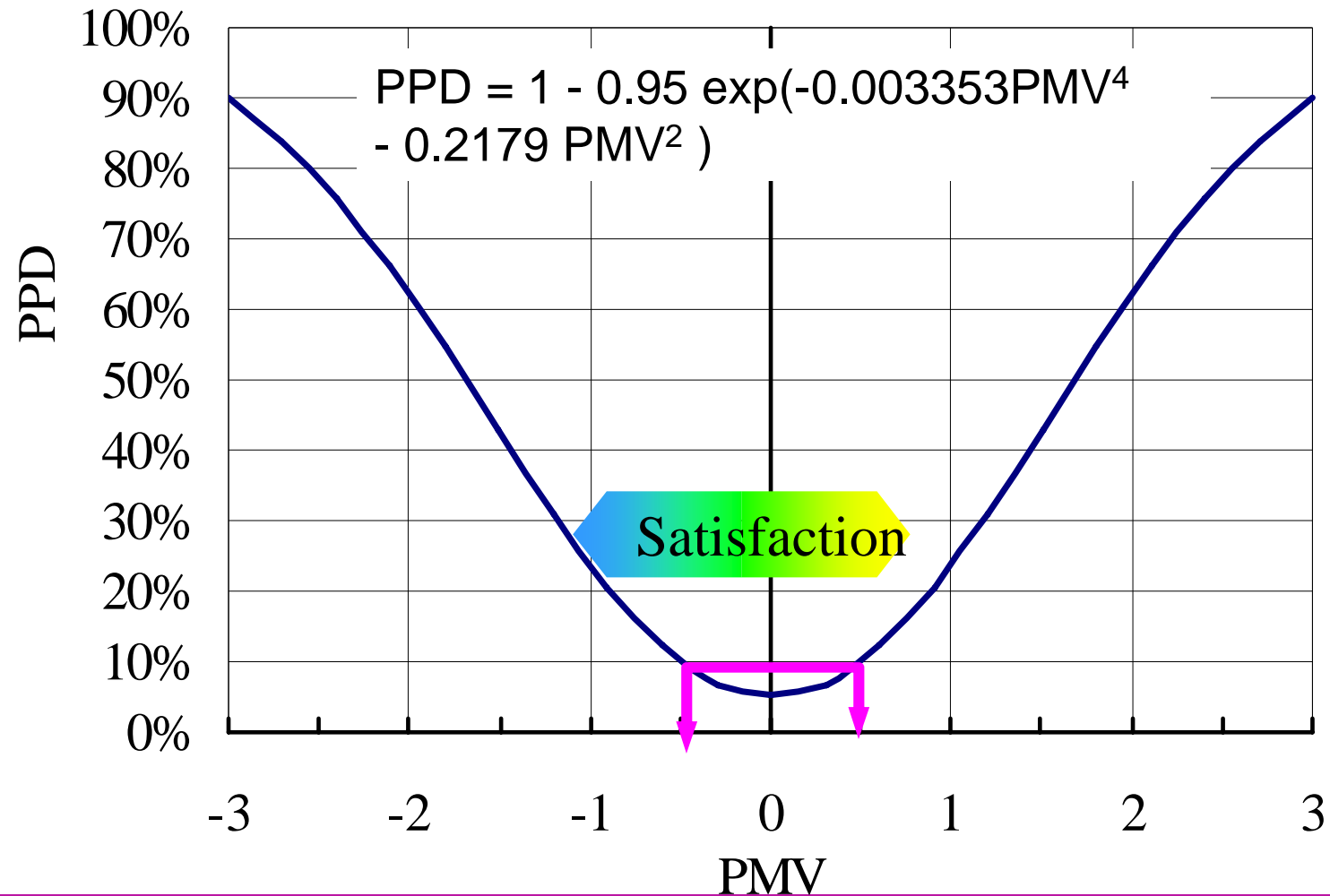
- PMV index  
(Predicted mean vote)
- PPD index  
(Predicted percentage of dissatisfied)



# Comfort measure: Predicted Mean Vote



# PMV and PPD



# Fanger Equation

$$PMV = [0.303 \exp(-0.036m) + 0.028]$$

$$\bullet \left[ \begin{array}{l} m - w - 0.00305(5733 - 6.99(m - w) - p) \\ -0.42(m - w - 58.15) - 0.000017m(5867 - p) \\ -0.0014m(307 - T_a) - F \end{array} \right]$$

$$F = 3.96 \cdot 10^{-8} f(T_{cl}^4 - T_{mrt}^4) + f h(T_{cl} - T_a)$$

$$h = \max \left\{ 2.38(T_{cl} - T_a)^{1/4}; 12.06\sqrt{v} \right\}$$

$$T_{cl} = 308.9 - 0.028(m - w) - R F$$

# Thermal comfort

*1<sup>st</sup> condition : Body heat balance*

## Standard recommendations

**EN ISO 7730 and ASHRAE 55-2004 :**

$$-0.5 < PMV < +0.5 \rightarrow PPD < 10 \%$$

# Range of validity of the model of Fanger

- Valid only in steady-state conditions
- Metabolism from 46 to 230 W/m<sup>2</sup> (0.8 to 4 met);
- Clothing from 0 to 2 clo ;
- Air temperature from 10 to 30 ° C;
- MRT from 10 to 40 ° C;
- Air velocity up to 1 m/s;
- Partial pressure of water vapor from 0 to 2700 Pa.

# Thermal comfort

- EN ISO 7730 – parameters especially for HVAC systems design
- Main parameters of IEQ in Appendix A of EN 12831
- 3 categories of thermal comfort according to PPD and PMV

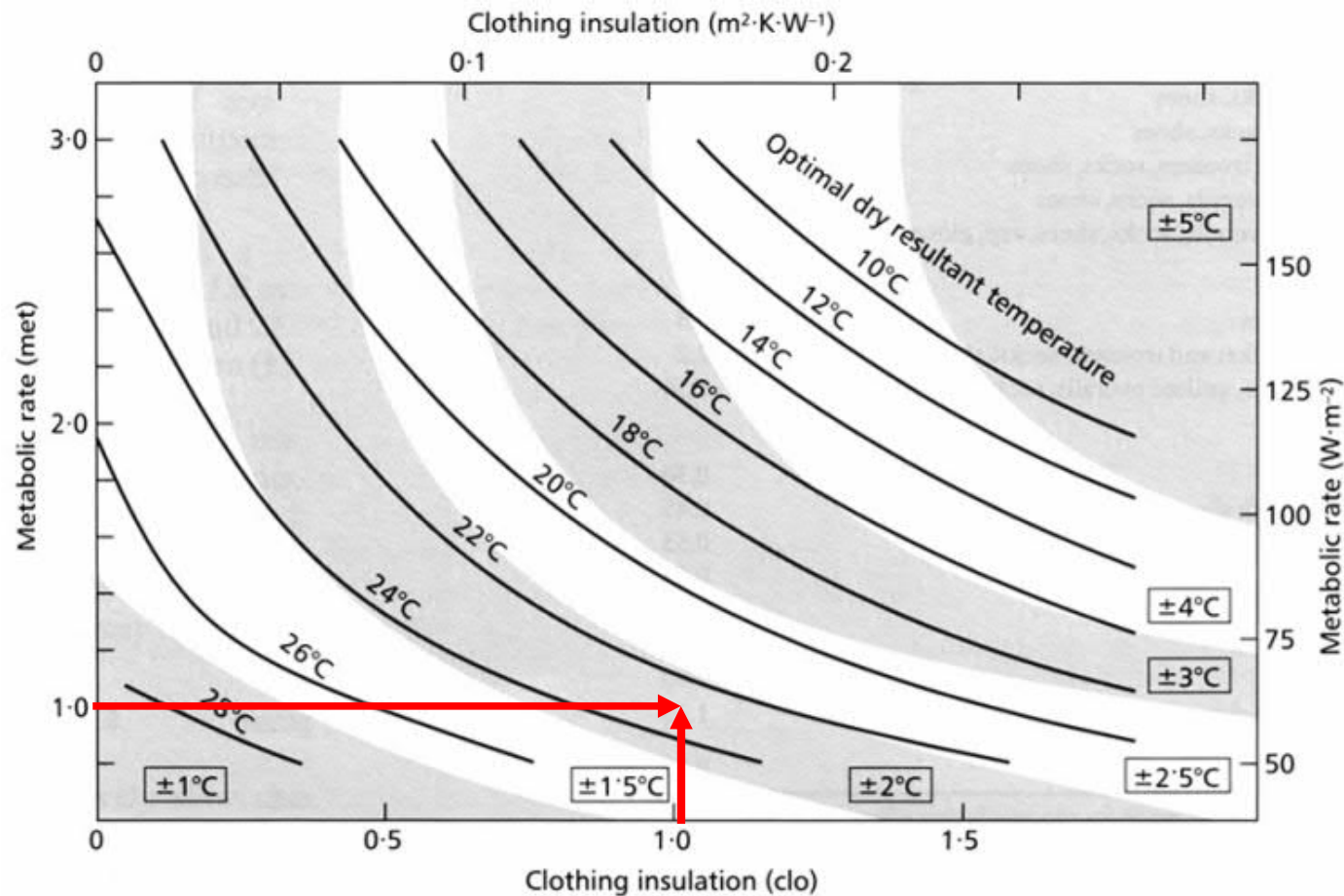
Categories of thermal environment (EN ISO 7730)

Category of indoor thermal environment	Thermal state of the body as a whole	
	PPD	PMV
A	< 6%	$-0,2 < PMV < +0,2$
B	< 10%	$-0,5 < PMV < +0,5$
C	< 15%	$-0,7 < PMV < +0,7$

PMV - predicted mean vote, PPD - predicted percentage of dissatisfied

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# Optimum Air Temperature Depending on Clothing and Metabolic Rate (ASHRAE 55)





# Indoor resultant (operative) temperature

Type of building, Space	Clothing, winter (clo)	Activity (met)	Category of indoor environment	Operative temperature, winter (°C)
Office	1,0	1,2	A	21,0 - 23,0
			B	20,0 - 24,0
			C	19,0 - 25,0
Open space office	1,0	1,2	A	21,0 - 23,0
			B	20,0 - 24,0
			C	19,0 - 25,0
Cafe, restaurant	1,0	1,2	A	21,0 - 23,0
			B	20,0 - 24,0
			C	19,0 - 25,0
Shopping center	1,0	1,6	A	17,5 - 20,5
			B	16,0 - 22,0
			C	15,0 - 23,0
Housing	1,0	1,2	A	21,0 - 23,0
			B	20,0 - 24,0
			C	19,0 - 25,0

# Temperature criteria for the design

Example criteria for operative temperature and mean air velocity for typical spaces<sup>a</sup>

Type of building/space	Clothing cooling season (summer; Clo)	Clothing heating season (winter; Clo)	Activity (met)	Category	Operative temperature cooling season (summer; °C)	Operative temperature heating season (winter; °C)	Mean air velocity cooling season (summer; m s <sup>-1</sup> )	Mean air velocity heating season (winter; m s <sup>-1</sup> )
Office	0.5	1.0	1.2	A	24.5 ± 0.5	22.0 ± 1.0	0.18	0.15
				B	24.5 ± 1.5	22.0 ± 2.0	0.22	0.18
				C	24.5 ± 2.5	22.0 ± 3.0	0.25	0.21
Cafeteria/restaurant	0.5	1.0	1.4	A	23.5 ± 1.0	20.0 ± 1.0	0.16	0.13
				B	23.5 ± 2.0	20.0 ± 2.5	0.20	0.16
				C	23.5 ± 2.5	20.0 ± 3.5	0.24	0.19
Department/store	0.5	1.0	1.6	A	23.0 ± 1.0	19.0 ± 1.5	0.16	0.13
				B	23.0 ± 2.0	19.0 ± 3.0	0.20	0.15
				C	23.0 ± 3.0	19.0 ± 4.0	0.23	0.18

<sup>a</sup> Relative humidity is assumed to be 60% for 'summer' and 40% for 'winter'.

# Thermal comfort

**According to EN ISO 7730 there are two conditions for thermal comfort**

- ① The heat balance of the individual is balanced without overexertion of its self-regulatory mechanisms
- ② There are no local discomforts due to:
  - air velocity/draught
  - radiant assymetry
  - the vertical temperature gradient
  - floor temperature

# Draught Rating, DR

Draught sensation can be estimated using Draught Rating (DR)

$$DR = (34 - t_a)(\bar{v} - 0,05)^{0,62} (0,37 * \bar{v} * Tu + 3,14)$$

DR = share of people, who are dissatisfied due to draught, %

$t_a$  = local air temperature, °C

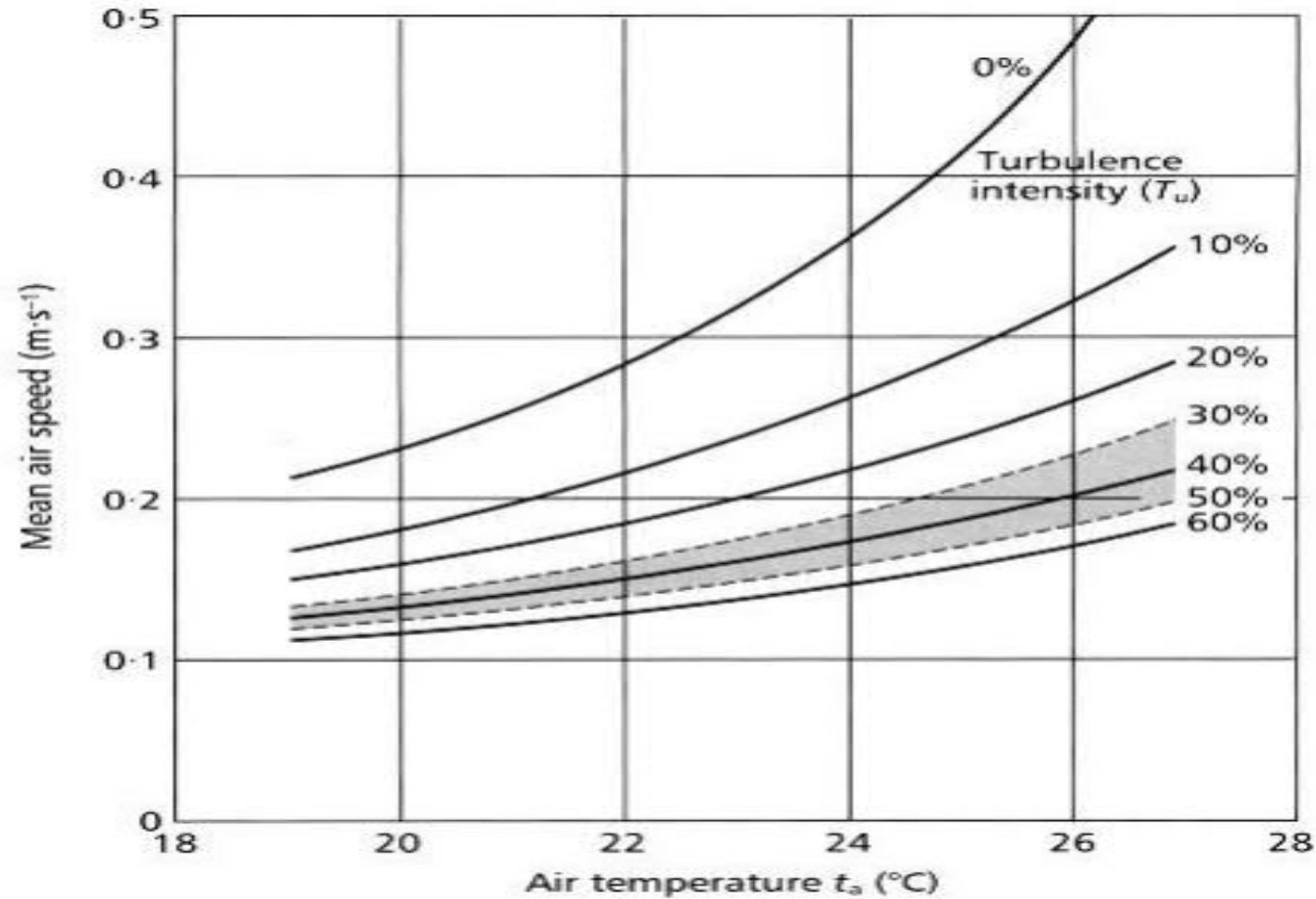
$\bar{v}$  = average air velocity, m/s

$T_u$  = local turbulence intensity, %

$$Tu = 100 * \frac{v_{sd}}{v}$$

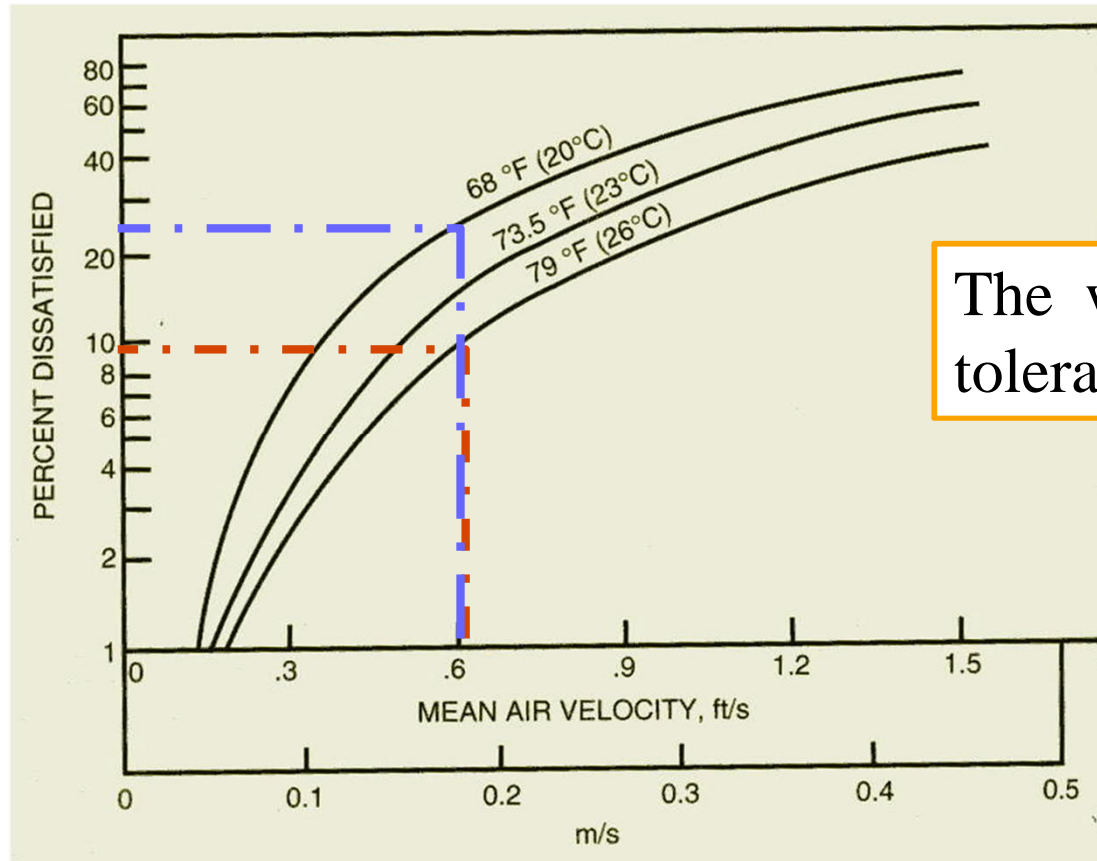
$v_{sd}$  standard deviation of flow velocity, m/s

# Draught Rating DR = 15%



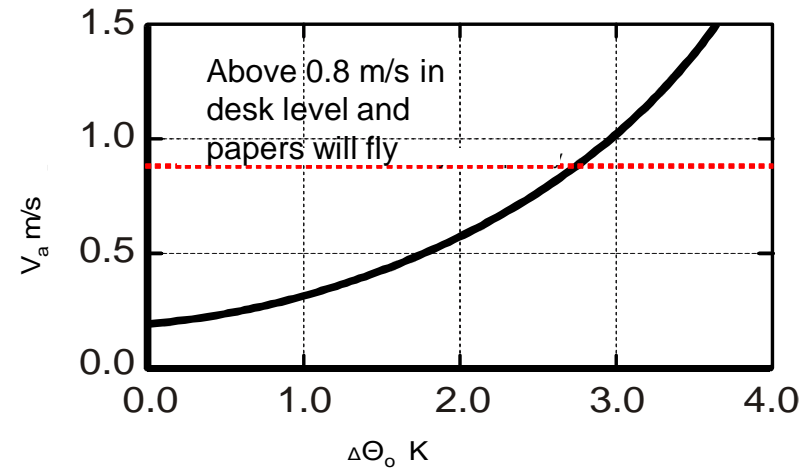
# Local thermal discomfort

## Air velocity



The warmer air is, the larger tolerance is .

# Increased Room Air Velocity

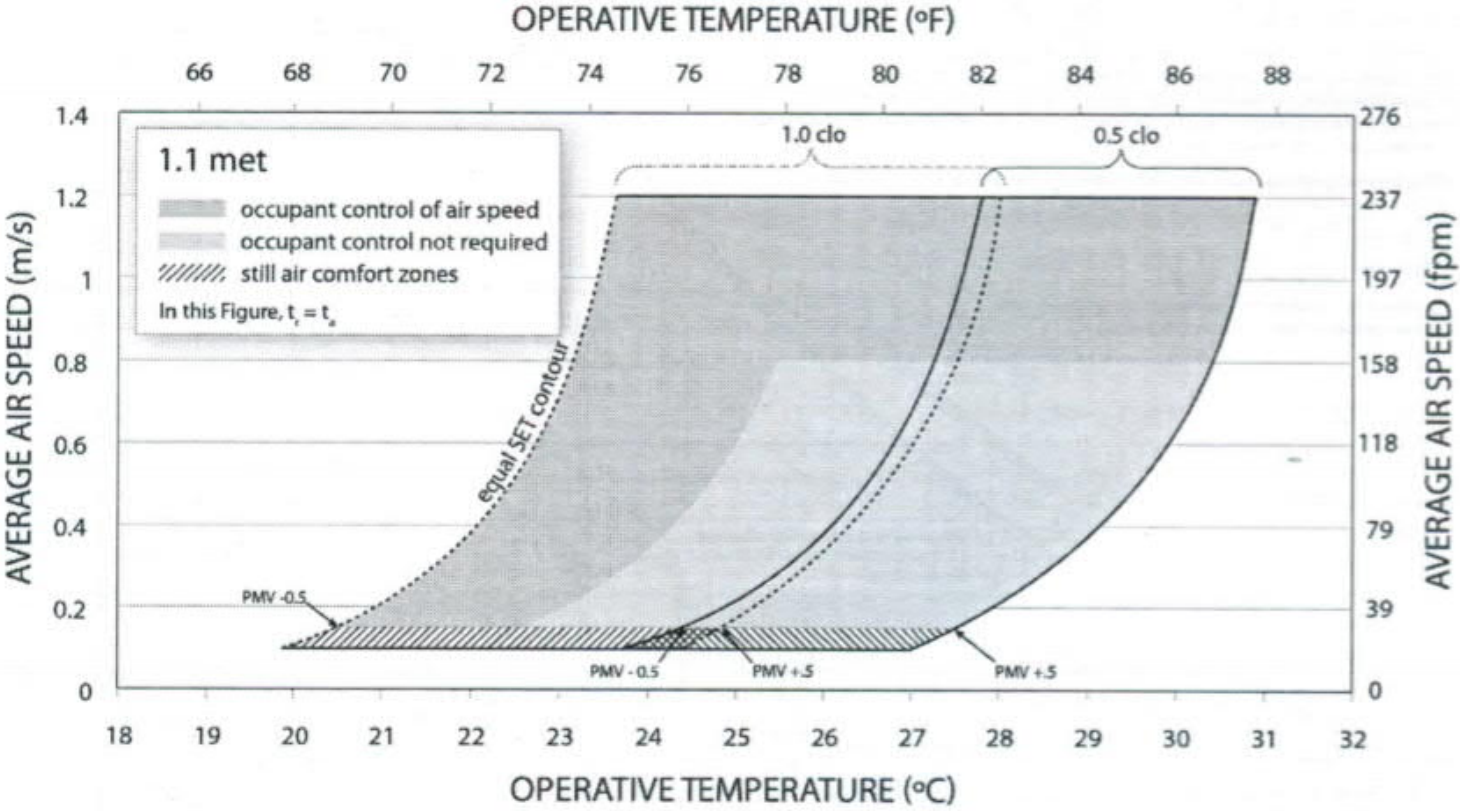


## Personalized ventilation

Air speed required to offset increased temperature ( EN ISO 7730).

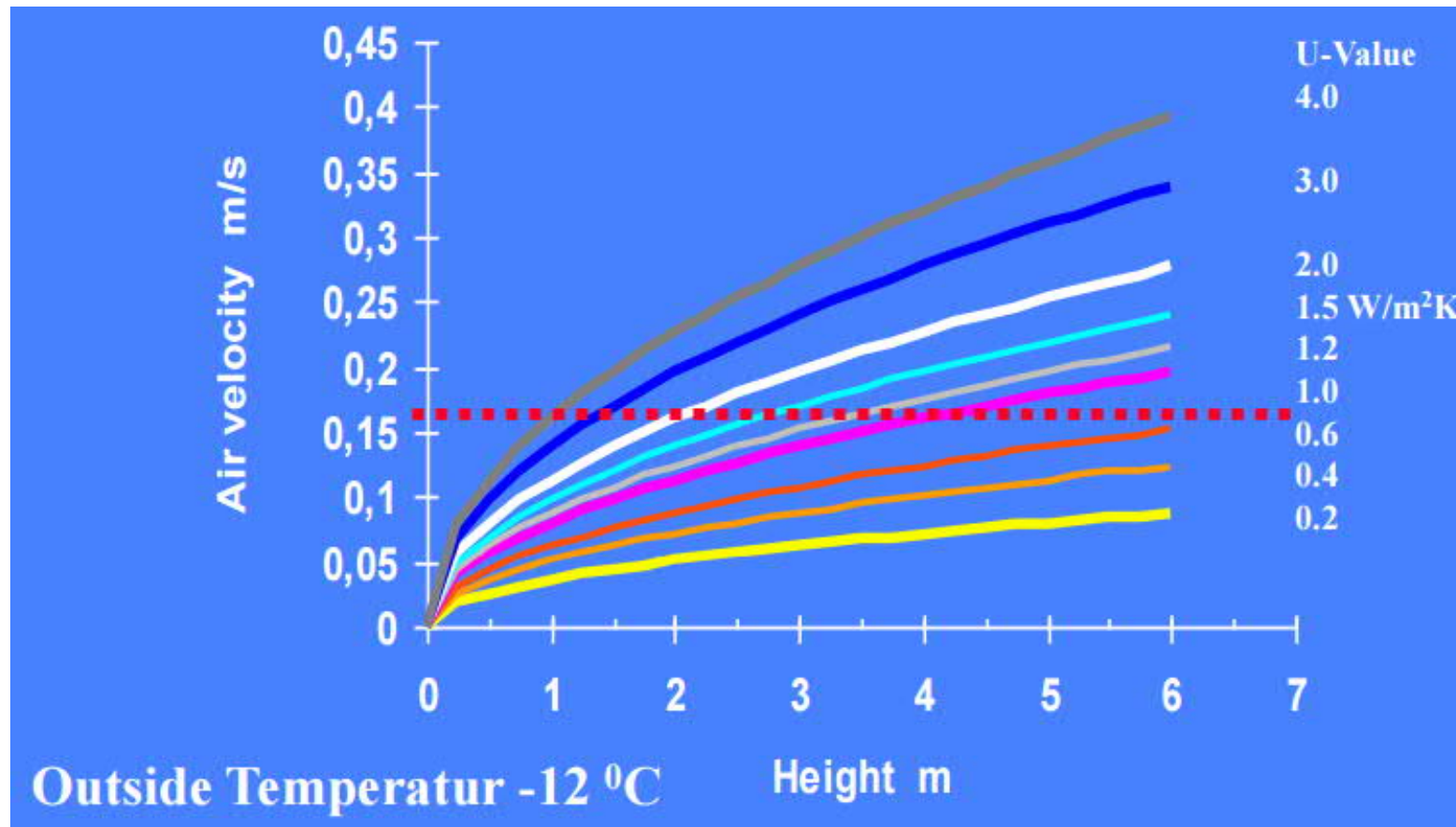
- The air speed increases by the amount necessary to maintain the same total heat transfer from the skin.
- Acceptance of the increased air speed will require occupant control of device creating the local air speed.

# Acceptable Range of Operative Temperature





# Down Draught of Cold Window Surface



Cold surface temperature creates strong convection flow and increases the risk of draught

# Standard Effective Temperature (SET)

- It is a comprehensive comfort index based on heat-balance equations that incorporates the personal factors clothing and metabolic rate as well as skin temperature and skin wetness.
- ASHRAE 55-2010 defines SET as the temperature of an imaginary environment at
  - 50% relative humidity;
  - $<0.1$  m/s average air speed;
  - mean radiant temperature equal to average air temperature;total heat loss from the skin of an imaginary occupant with
  - an activity level of 1.0 met; a clothing level of 0.6 clo;is the same as that from a person in the actual environment, with actual clothing and activity level.

# Local thermal discomfort

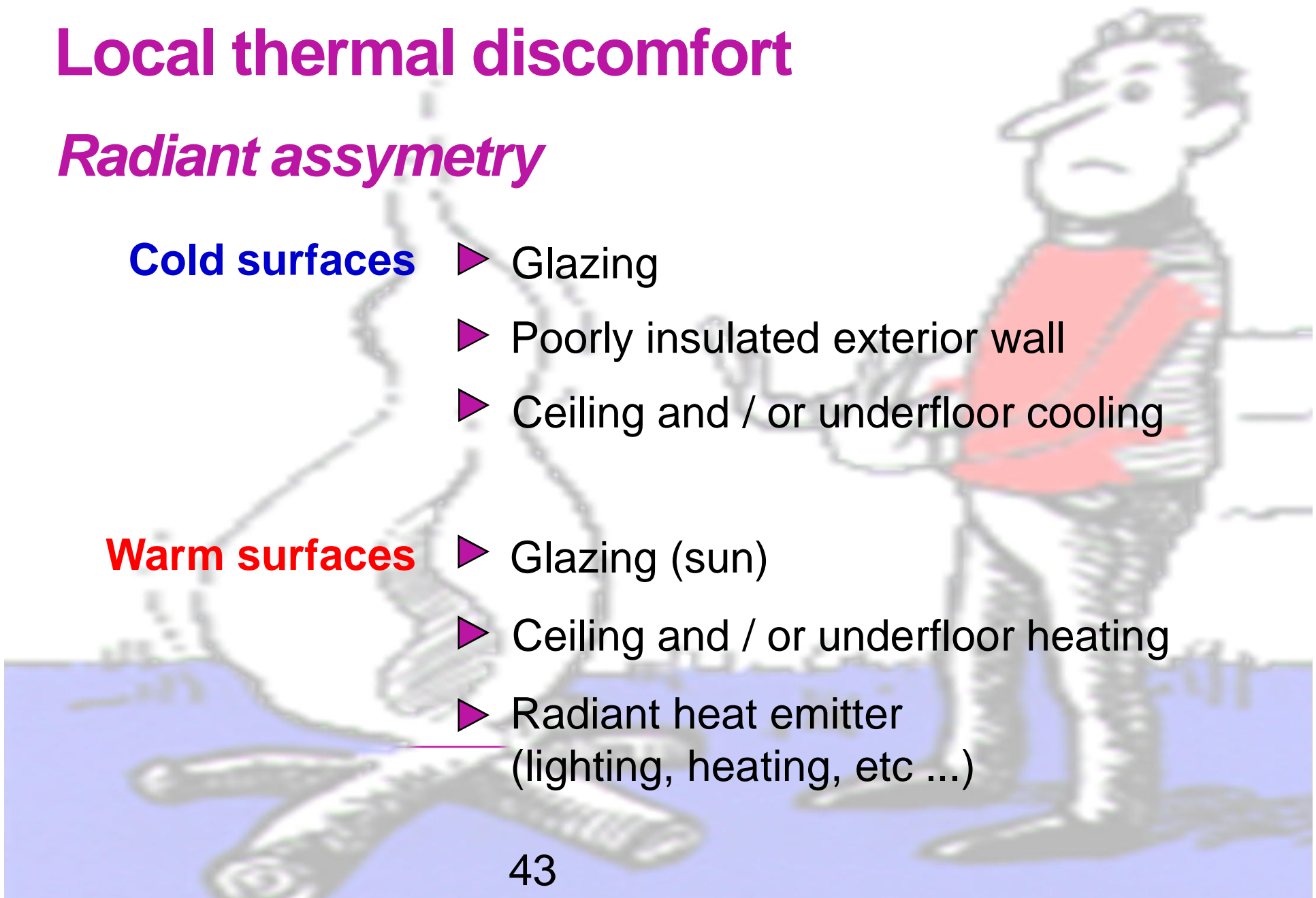
## *Radiant asymmetry*

### **Cold surfaces**

- ▶ Glazing
- ▶ Poorly insulated exterior wall
- ▶ Ceiling and / or underfloor cooling

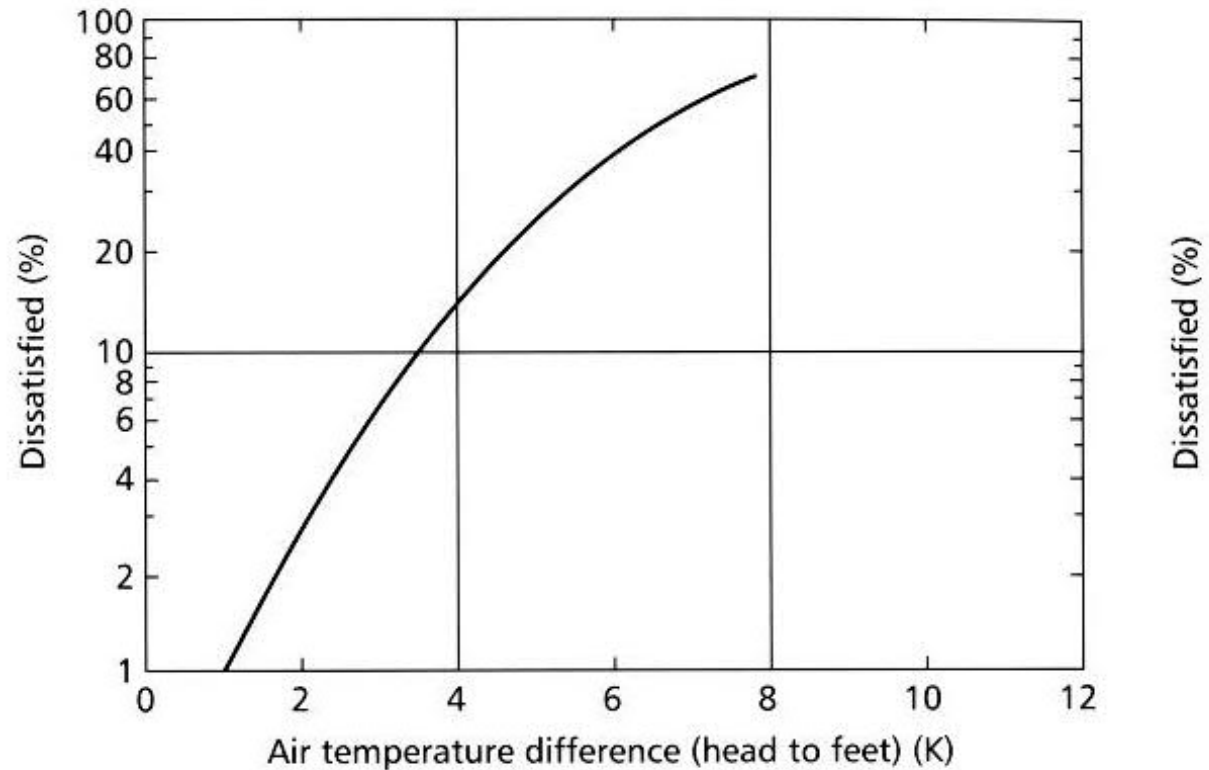
### **Warm surfaces**

- ▶ Glazing (sun)
- ▶ Ceiling and / or underfloor heating
- ▶ Radiant heat emitter  
(lighting, heating, etc ...)

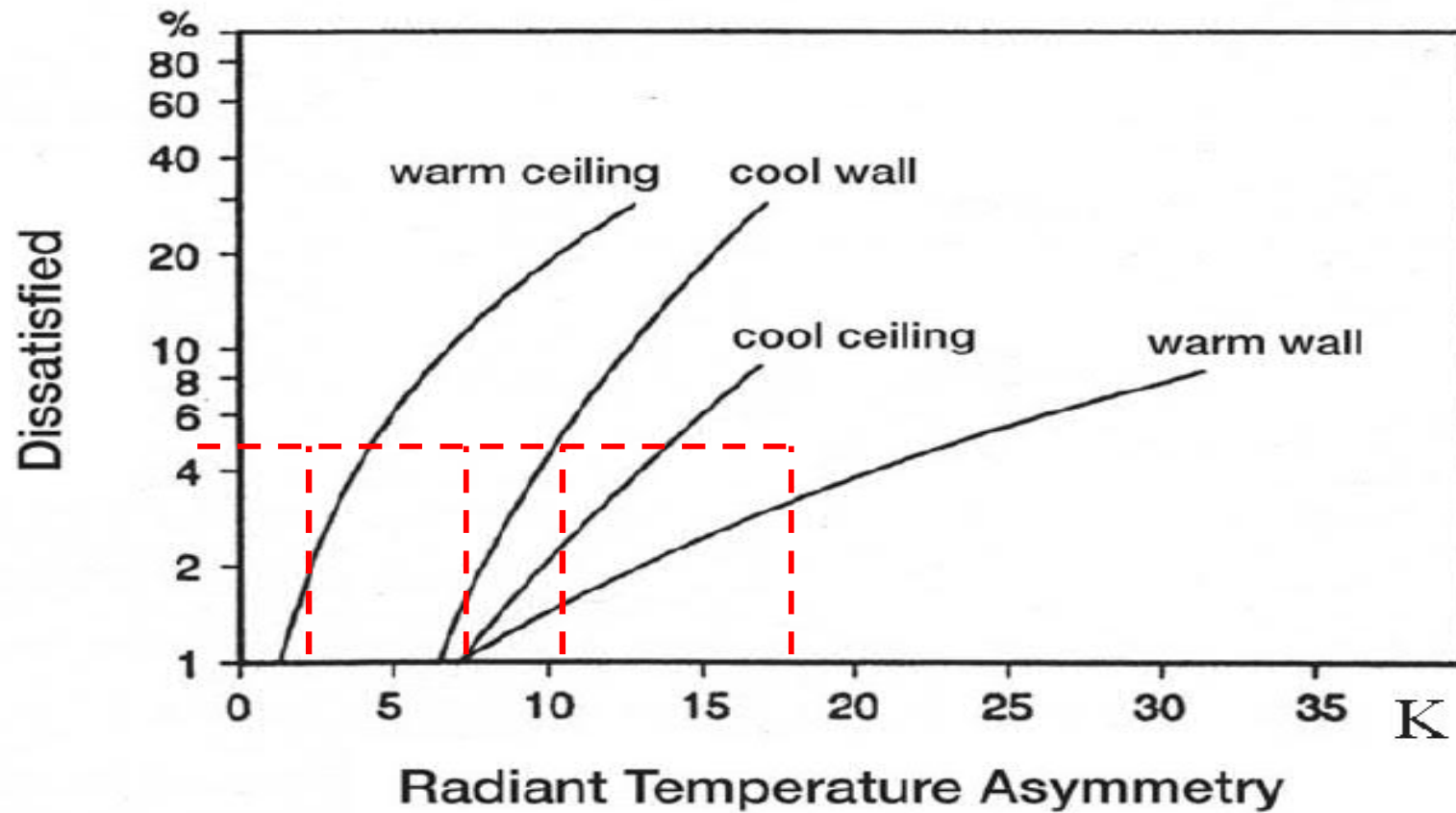


# Vertical Temperature Asymmetry

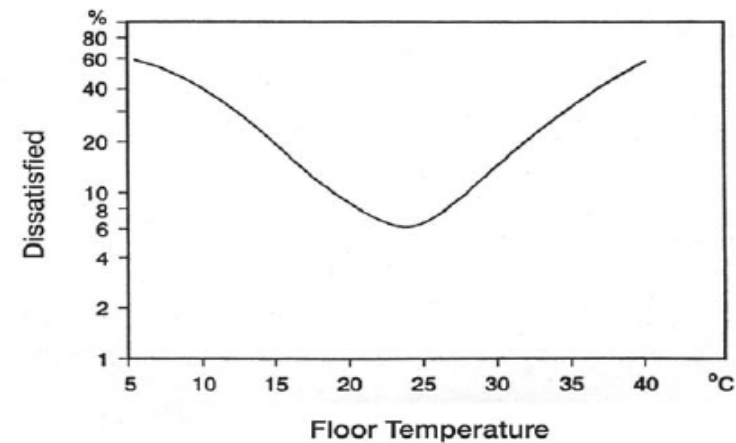
General recommendation is that temperatures between head and feet should not differ by  $>3^{\circ}\text{C}$



# Radiant Temperature Assymmetry



# Floor Temperature



- SEATED/STANDING PERSONS:  
(66.2F)  $19\text{ °C} < t_s < 29\text{ °C}$  (84.2F)
- BY HIGHER ACTIVITY LEVELS A LOWER FLOOR TEMPERATURE IS ACCEPTABLE

# Adaptation to Various Thermal Conditions: Thermal comfort in buildings without mechanical cooling

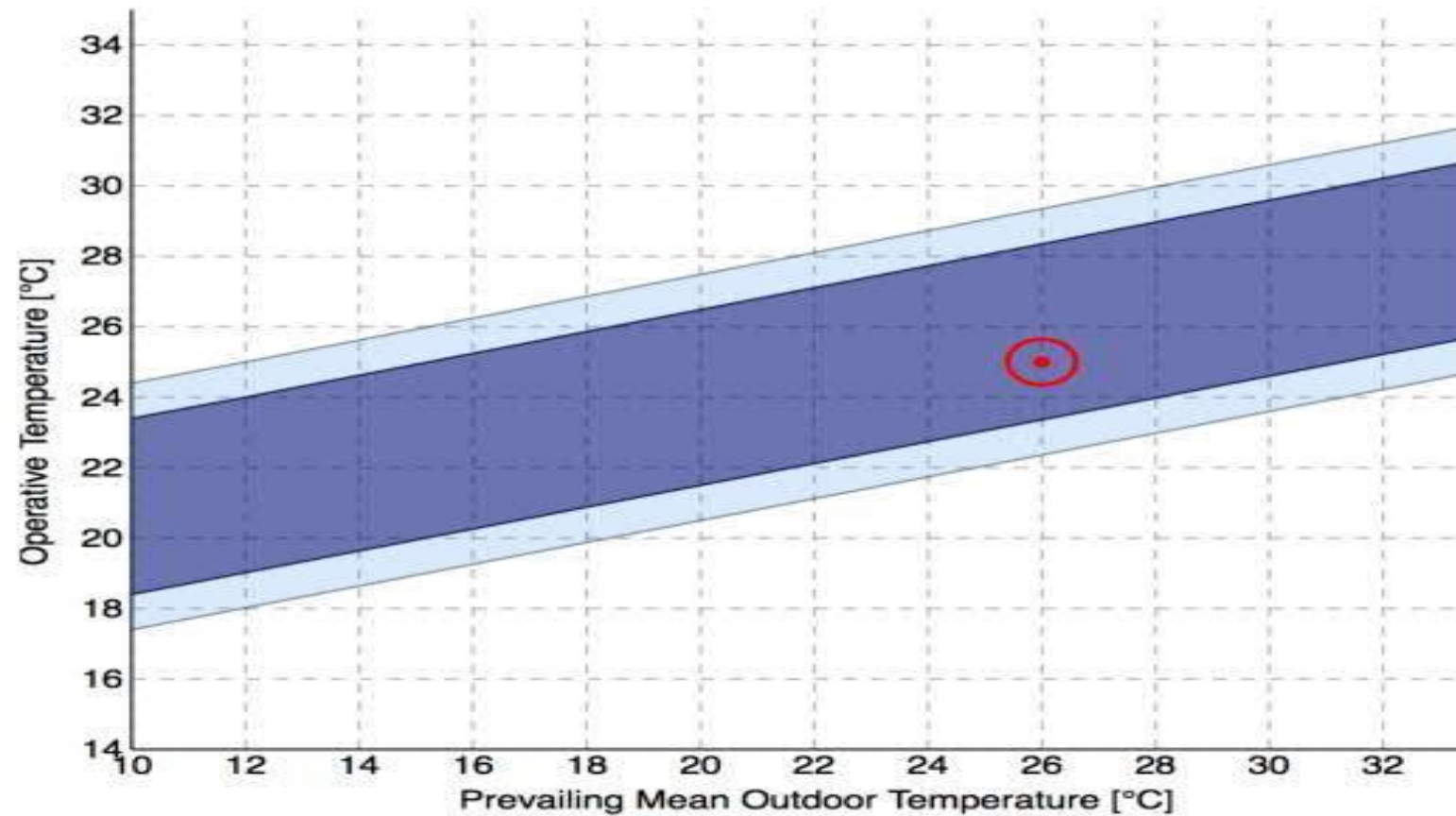
- The adaptive model is based on the idea that outdoor climate influences indoor comfort because humans can adapt to different temperatures during different times of the year.
- There are basically three categories of thermal adaptation to explain the difference between field observations and PMV predictions:
  - **Behavioural** (clothing, activity, personalized control);
  - **Physiological** (acclimatization, genetic adaptation);
  - **Psychological** (expectation, opportunity to adapt).
- The adaptive hypothesis predicts that contextual factors, such as having access to environmental controls, and past thermal history influence building occupants' thermal expectations and preferences.

# Adaptive Thermal Comfort Model

- Adaptive models of thermal comfort are implemented in standards such as ASHRAE 55, European EN 15251 and ISO 7730 standard.
- According ASHRAE in order to apply the adaptive model,
  - there should be no mechanical cooling system for the space,
  - occupants should be engaged in sedentary activities with metabolic rates of 1-1.3 met, and
  - a prevailing mean temperature greater than 10 ° C (50 ° F) and less than 33.5 ° C (92.3 ° F).
- EN15251 can be applied to mixed-mode buildings provided the system is not running.
- The adaptive chart relates indoor comfort temperature to prevailing outdoor temperature and defines zones of 80% and 90% satisfaction.

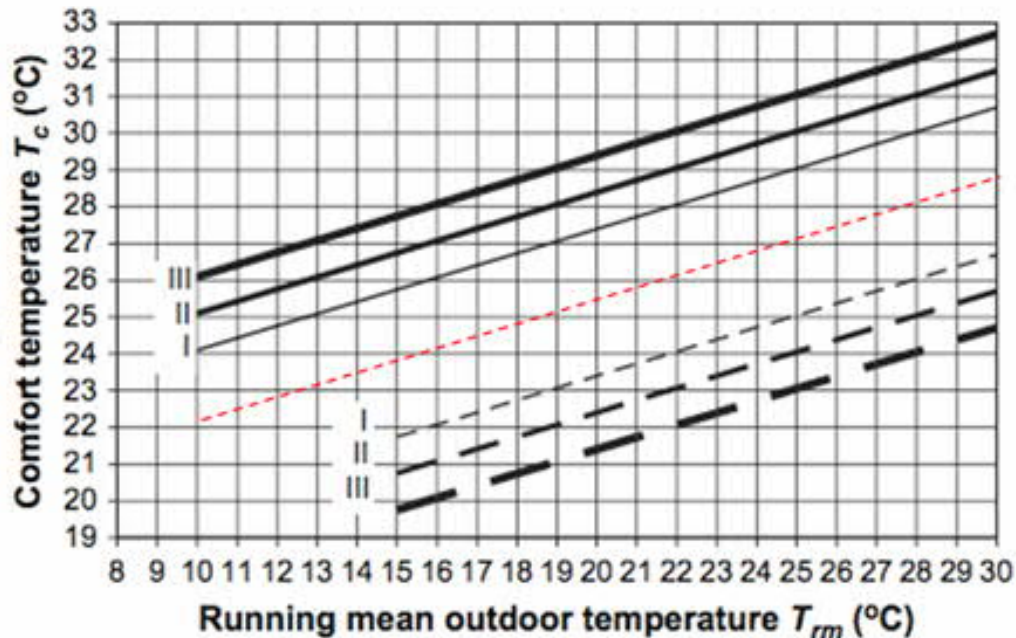


# Adaptive Thermal Comfort Model (ASHRAE 55)



# Adaptive Thermal Comfort Model (EN 15251)

$$T_{\text{comf}} = 0.33 T_{\text{rm}} + 18.8$$



Category Explanation:

I High level of expectation only used for spaces occupied by very sensitive and fragile persons

II Normal expectation for new buildings and renovations

III A moderate expectation (used for existing buildings)

IV Values outside the criteria for the above categories (only acceptable for a limited periods)

The allowable maximum difference between this comfort temperature and the actual indoor **operative** temperature ( $T_{\text{diff}}$ ) is given in terms of the categories

- Category I:  $\pm 2\text{K}$
- Category II:  $\pm 3\text{K}$
- Category III:  $\pm 4\text{K}$

# Thermal Comfort Indicators

Index	Dry-bulb Air Temperature	Radiant Temperature	Air Velocity	Turbulence Intensity	Relative Humidity	MET (Activity)	Clothing	Outdoor Air Temperature
Air Temperature	X							
Operative Temperature	X	X						
Draught Rating (local)	X		X	X				
PMV & PPD – Index (whole body)	X	X	X		X	X	X	
Standard Effective Temperature	X	X	X		X	X	X	
Adaptive Thermal Comfort Model	X	X						X

# Thank you