



Aalto University
School of Engineering

Geo-E2010 Advanced Soil Mechanics L

Wojciech Sołowski

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Aalto University
School of Engineering

Tutorial 1

Mohr - Coulomb model

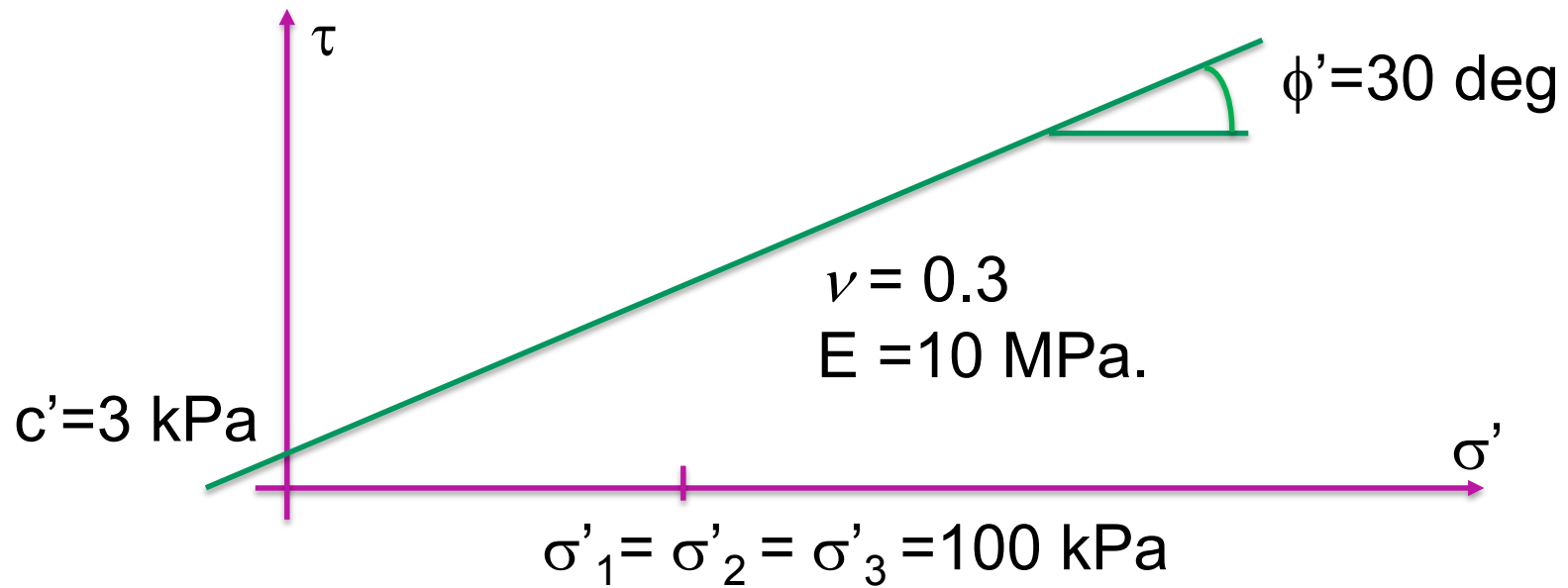
Tutorial 1

Simulate standard triaxial drained and undrained tests, assuming that soil is behaving as a Mohr-Coulomb material.

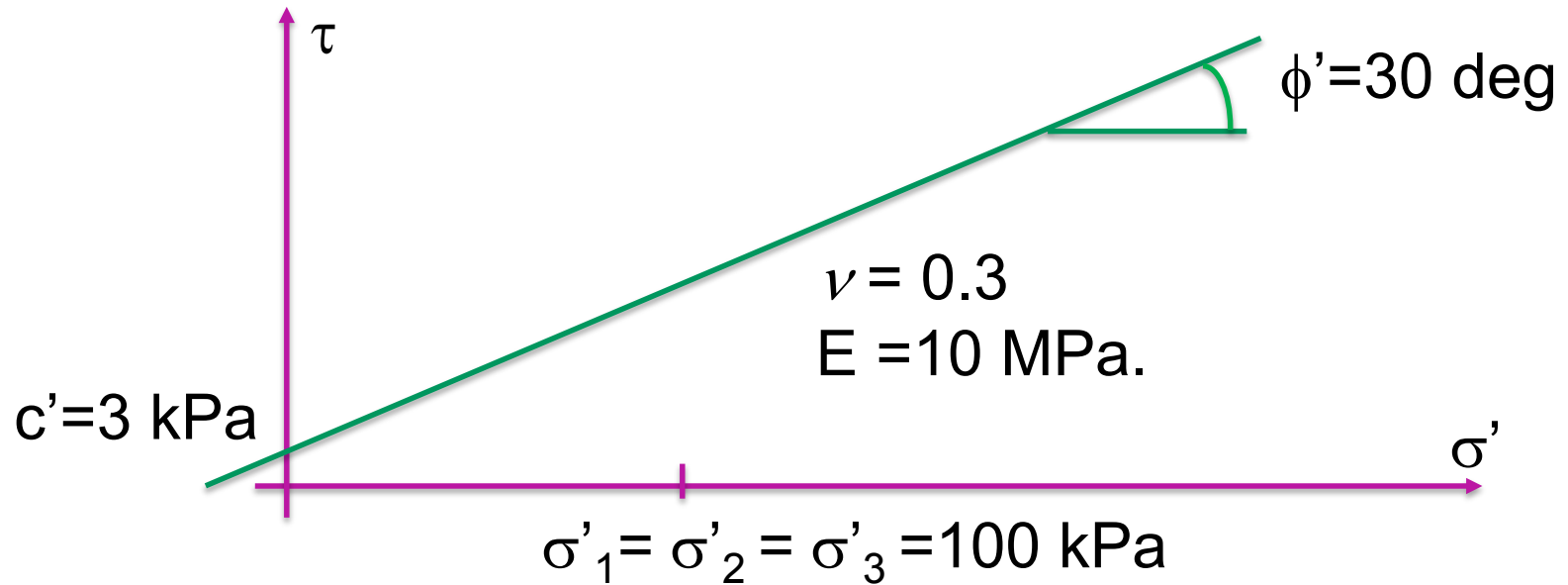
Assume initial condition $p=100$ kPa, $q=0$.

Assume Mohr-Coulomb soil parameters:

- friction angle 30 degrees
- dilation angle: 0 degrees, 3 degrees, 30 degrees
- cohesion c' equal to 3 kPa
- Poisson's ratio 0.3
- Young's modulus 10 MPa.

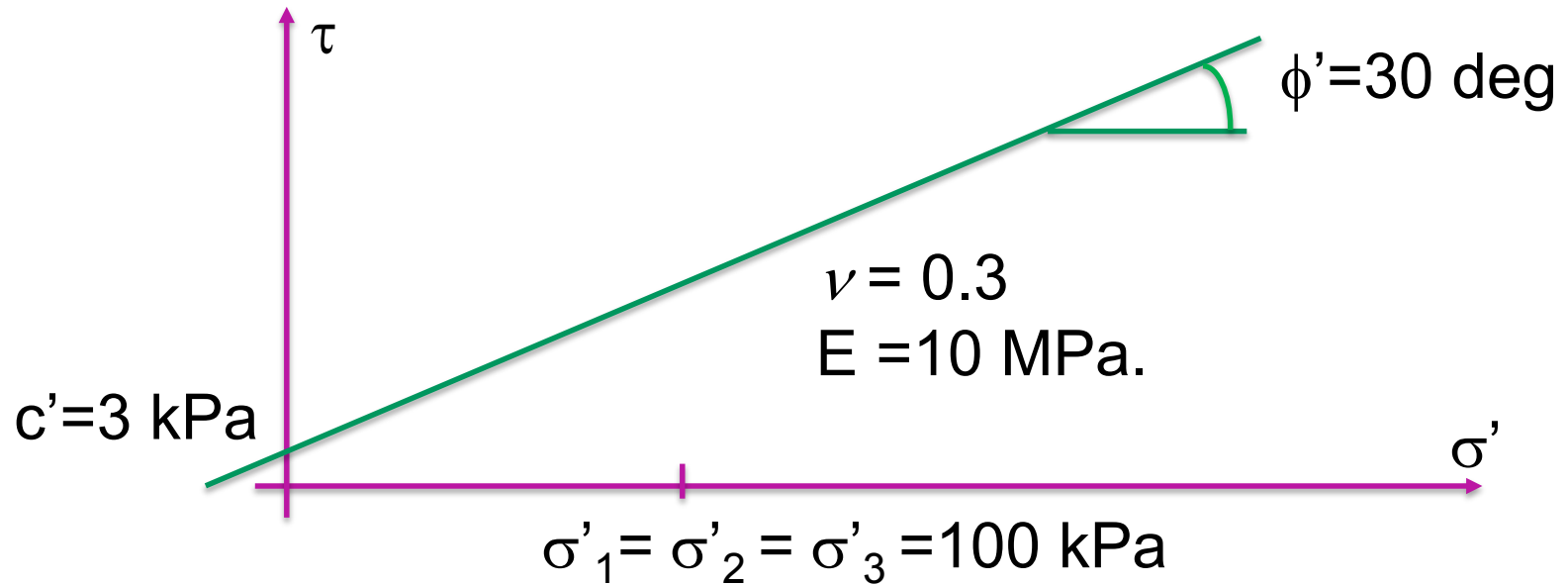


Drained test



σ'_1 – increases, $\sigma'_2 = \sigma'_3 = \text{const.}$

Drained test



$$F = (\sigma'_1 - \sigma'_3) - (\sigma'_1 + \sigma'_3) \sin \phi' - 2c' \cos \phi' = 0$$

Drained...

$p'=100$ kPa and $q=0$ kPa. Hence $\sigma_1'=\sigma_3'=100$ kPa

In triaxial test cell pressure is constant, hence $\sigma_3'=\text{const.}=100$ kPa

How high σ_1' needs to be to reach yielding?

$$\sigma_1' - 100 - (\sigma_1' + 100)0.5 - 2 \cdot 3 \cdot 0.5 \sqrt{3} = 0$$

$$0.5 \sigma_1' = 150 + 5,2 = 155.2 \quad \sigma_1' = 310.4 \text{ [kPa]}$$

$$p' = (100 + 100 + 310.4) / 3 = 170.1 \text{ kPa} \quad q = 310.4 - 100 = 210.4 \text{ kPa}$$

$$F = (\sigma_1' - \sigma_3') - (\sigma_1' + \sigma_3') \sin \phi' - 2c' \cos \phi' = 0$$

Drained...

$\Delta p' = 170,1 - 100 = 70,1$ kPa and $\Delta q = 210,4$ kPa.

Strains:

$$\begin{Bmatrix} \Delta \varepsilon_{11} \\ \Delta \varepsilon_{22} \\ \Delta \varepsilon_{33} \\ \Delta \varepsilon_{12} \\ \Delta \varepsilon_{13} \\ \Delta \varepsilon_{23} \end{Bmatrix} = \frac{1}{E} \overbrace{\begin{bmatrix} 1 & -\nu & -\nu & 0 & 0 & 0 \\ -\nu & 1 & -\nu & 0 & 0 & 0 \\ -\nu & -\nu & 1 & 0 & 0 & 0 \\ & & & 1+\nu & 0 & 0 \\ & & & & 1+\nu & 0 \\ & & & & & 1+\nu \end{bmatrix}}^{\mathbf{D}^{el^{-1}}} \begin{Bmatrix} \Delta \sigma_{11} \\ \Delta \sigma_{22} \\ \Delta \sigma_{33} \\ \Delta \sigma_{12} \\ \Delta \sigma_{13} \\ \Delta \sigma_{23} \end{Bmatrix}$$

$$F = (\sigma'_1 - \sigma'_3) - (\sigma'_1 + \sigma'_3) \sin \phi' - 2c' \cos \phi' = 0$$

Drained...

$\Delta p' = 170,1 - 100 = 70,1$ kPa and $\Delta q = 210,4$ kPa.

Strains:

$$\begin{Bmatrix} \Delta \varepsilon_{11} \\ \Delta \varepsilon_{22} \\ \Delta \varepsilon_{33} \\ \Delta \varepsilon_{12} \\ \Delta \varepsilon_{13} \\ \Delta \varepsilon_{23} \end{Bmatrix} = \frac{1}{10000} \overbrace{\begin{bmatrix} 1 & -\nu & -\nu & 0 & 0 & 0 \\ -\nu & 1 & -\nu & 0 & 0 & 0 \\ -\nu & -\nu & 1 & 0 & 0 & 0 \\ & & & 1+\nu & 0 & 0 \\ & & & & 1+\nu & 0 \\ & & & & & 1+\nu \end{bmatrix}}^{\mathbf{D}^{el^{-1}}} \begin{Bmatrix} 210,4 \\ 0 \\ 0 \\ 0 \\ 0 \\ 0 \end{Bmatrix}$$

Drained...

$\Delta p' = 170,1 - 100 = 70,1$ kPa and $\Delta q = 210,4$ kPa.

Strains:

$$\begin{Bmatrix} \Delta \varepsilon_{11} \\ \Delta \varepsilon_{22} \\ \Delta \varepsilon_{33} \\ \Delta \varepsilon_{12} \\ \Delta \varepsilon_{13} \\ \Delta \varepsilon_{23} \end{Bmatrix} = \frac{1}{E} \begin{matrix} \overbrace{\begin{bmatrix} 1 & -0.3 & -0.3 & 0 & 0 & 0 \\ -0.3 & 1 & -0.3 & 0 & 0 & 0 \\ -0.3 & -0.3 & 1 & 0 & 0 & 0 \\ & & & 1+0.3 & 0 & 0 \\ & & & & 1+0.3 & 0 \\ & & & & & 1+0.3 \end{bmatrix}}^{\mathbf{D}^{el^{-1}}} \end{matrix} \begin{Bmatrix} \Delta \sigma \\ 210.4 \\ 0 \\ 0 \\ 0 \\ 0 \end{Bmatrix}$$

$$F = (\sigma'_1 - \sigma'_3) - (\sigma'_1 + \sigma'_3) \sin \phi' - 2c' \cos \phi' = 0$$

Drained...

$$\begin{Bmatrix} \Delta \varepsilon_{11} \\ \Delta \varepsilon_{22} \\ \Delta \varepsilon_{33} \\ \Delta \varepsilon_{12} \\ \Delta \varepsilon_{13} \\ \Delta \varepsilon_{23} \end{Bmatrix} = \frac{1}{10000} \overbrace{\begin{bmatrix} 1 & -\nu & -\nu & 0 & 0 & 0 \\ -\nu & 1 & -\nu & 0 & 0 & 0 \\ -\nu & -\nu & 1 & 0 & 0 & 0 \\ & & & 1+\nu & 0 & 0 \\ & & & & 1+\nu & 0 \\ & & & & & 1+\nu \end{bmatrix}}^{\mathbf{D}^{el^{-1}}} \begin{Bmatrix} \Delta \sigma \\ 210.4 \\ 0 \\ 0 \\ 0 \\ 0 \end{Bmatrix}$$

$$\Delta \varepsilon_{11} = 210.4 / 10000 = 0,02104 = 2.104\%$$

$$\Delta \varepsilon_{22} = -0.3 * 210.4 / 10000 = -0.006312 = -0.631\%$$

$$\Delta \varepsilon_{33} = -0.3 * 210.4 / 10000 = -0.006312 = -0.631\%$$

$$\Delta \varepsilon_v = \Delta \varepsilon_{11} + \Delta \varepsilon_{22} + \Delta \varepsilon_{33} = 0.842\%$$

$$\Delta \varepsilon_q = 2/3(\Delta \varepsilon_{11} - \Delta \varepsilon_{33}) = 1,823\%$$

Drained...

$$\left\{ \begin{array}{c} \Delta\sigma \\ p \\ q \end{array} \right\} = \overbrace{\begin{bmatrix} K & 0 \\ 0 & 3G \end{bmatrix}}^{\mathbf{D}^{el}} \left\{ \begin{array}{c} \Delta\varepsilon \\ \Delta\varepsilon_v \\ \Delta\varepsilon_q \end{array} \right\}$$

$$K = \frac{E}{3(1-2\nu)} = \frac{10000}{3(1-0.6)} = 8333,33$$

$$G = \frac{E}{2(1+\nu)} = \frac{10000}{2(1+0.3)} = 3846,15$$

$$\Delta\varepsilon_v = \frac{1}{K} \Delta p = 70,1 / 8333,33 = 0,841\%$$

$$\Delta\varepsilon_q = \frac{1}{3G} \Delta q = 210,4 / 3846,15 = 1,82\%$$

Let's check in Excel

Driver:

Strain increment $d\varepsilon_{11}$

We know that:

$$p/q = 1/3 = K / 3G * d\varepsilon_v / d\varepsilon_q \rightarrow G / K = d\varepsilon_v / d\varepsilon_q$$

$$\Delta\varepsilon_v = \Delta\varepsilon_{11} + 2\Delta\varepsilon_{33}$$

$$\Delta\varepsilon_q = 2/3(\Delta\varepsilon_{11} - \Delta\varepsilon_{33})$$

$$\begin{matrix} \Delta\sigma \\ \left[\begin{matrix} p \\ q \end{matrix} \right] \\ \Delta\varepsilon \end{matrix} = \begin{matrix} \mathbf{D}^{el} \\ \left[\begin{matrix} K & 0 \\ 0 & 3G \end{matrix} \right] \\ \left[\begin{matrix} \Delta\varepsilon_v \\ \Delta\varepsilon_q \end{matrix} \right] \end{matrix}$$

-- we have 1 eq + 2 eq connecting strains and stress+ 2 eq defining strains

So – 5 unknowns – (p, q), $d\varepsilon_q$, $d\varepsilon_v$, $d\varepsilon_{33}$

Stop condition:

$$F = (\sigma'_1 - \sigma'_3) - (\sigma'_1 + \sigma'_3) \sin \phi' - 2c' \cos \phi' = 0$$

MC model p' - q - space

$$F = (\sigma'_1 - \sigma'_3) - (\sigma'_1 + \sigma'_3) \sin \phi' - 2c' \cos \phi' = 0$$

$$\sigma'_1 = 3p' - 2\sigma'_3 \quad \sigma'_3 = \sigma'_1 - q$$

$$\sigma'_1 = 3p' - 2\sigma'_1 + 2q = \frac{3p' + 2q}{3}$$

$$\sigma'_3 = 3p' - 2\sigma'_3 - q = \frac{3p' - q}{3}$$

$$\sigma'_1 + \sigma'_3 = \frac{6p' + q}{3}$$

MC model p' - q - space

$$\text{or } q = \sin \phi \left(\frac{6p' + q}{3} \right) + 2c \cos \phi$$

$$3q = 6p' \sin \phi + q \sin \phi + 6c \cos \phi$$

$$q = \frac{6 \sin \phi'}{3 - \sin \phi'} p' + \frac{6c \cos \phi'}{3 - \sin \phi'}$$

$$q = \eta p' + c^*$$

$$\text{where } \eta = \frac{6 \sin \phi'}{3 - \sin \phi'}, c^* = \frac{6c \cos \phi'}{3 - \sin \phi'}$$

$$F = q - \eta p' - c^* = 0 \quad \rightarrow \quad \text{MC - Model formulated in p' - q}$$

MC model p'-q- space

$$\begin{Bmatrix} \Delta p' \\ \Delta q \end{Bmatrix} = \begin{bmatrix} K' & 0 \\ 0 & 3G' \end{bmatrix} \begin{Bmatrix} \Delta \varepsilon_v^e \\ \Delta \varepsilon_q^e \end{Bmatrix}$$

Assuming associated flow rule and ideal plasticity

$$F(p', q) = q - \eta p' - c^* = 0$$

$$\frac{\partial F}{\partial p'} dp' + \frac{\partial F}{\partial q} dq = 0 \quad : \text{ consistency condition}$$

Formulation of D^{ep} for MC

$$dp' = K (d\varepsilon_v - d\varepsilon_v^p)$$

$$dq = 3G (d\varepsilon_q - d\varepsilon_q^p)$$

$$d\varepsilon_v^p = d\lambda \frac{\partial F}{\partial p'}$$

$$d\varepsilon_q^p = d\lambda \frac{\partial F}{\partial q}$$

Substituting into consistency condition leads to:

$$\frac{\partial F}{\partial p'} K d\varepsilon_v - \frac{\partial F}{\partial p'} K d\lambda \frac{\partial F}{\partial p'} + \frac{\partial F}{\partial Q} 3G d\varepsilon_q - \frac{\partial F}{\partial q} 3G d\lambda \frac{\partial F}{\partial q} = 0$$

Formulation of D^{ep} for MC

$$d\lambda = \frac{\frac{\partial F}{\partial p'} K d\varepsilon_v + \frac{\partial F}{\partial q'} 3G d\varepsilon_q}{\frac{\partial F}{\partial p'} K \frac{\partial F}{\partial p'} + \frac{\partial F}{\partial q'} 3G \frac{\partial F}{\partial q'}} = \frac{\begin{bmatrix} \frac{\partial F}{\partial p'} & \frac{\partial F}{\partial q'} \end{bmatrix} \begin{bmatrix} K & 0 \\ 0 & 3G \end{bmatrix} \begin{Bmatrix} d\varepsilon_v \\ d\varepsilon_q \end{Bmatrix}}{\begin{bmatrix} \frac{\partial F}{\partial p'} & \frac{\partial F}{\partial q'} \end{bmatrix} \begin{bmatrix} K & 0 \\ 0 & 3G \end{bmatrix} \begin{Bmatrix} \frac{\partial F}{\partial p'} \\ \frac{\partial F}{\partial q'} \end{Bmatrix}}$$

Formulation of D^{ep} for MC

$$\frac{\partial F}{\partial p'} = -\eta, \quad \frac{\partial F}{\partial q} = 1, \quad d\lambda = \frac{-\eta K d\varepsilon_v + 3G d\varepsilon_q}{\eta^2 K + 3G}$$

$$d\varepsilon_v^p = -d\lambda\eta, \quad d\varepsilon_q^p = d\lambda$$

$$F = q - \eta p' - c^* = 0$$

$$\begin{aligned} \begin{Bmatrix} dp' \\ dq \end{Bmatrix} &= \begin{bmatrix} K & 0 \\ 0 & 3G \end{bmatrix} \begin{Bmatrix} d\varepsilon_v - d\varepsilon_v^p \\ d\varepsilon_q - d\varepsilon_q^p \end{Bmatrix} \\ &= \begin{bmatrix} K & 0 \\ 0 & 3G \end{bmatrix} \begin{Bmatrix} d\varepsilon_v \\ d\varepsilon_q \end{Bmatrix} - \begin{bmatrix} K & 0 \\ 0 & 3G \end{bmatrix} d\lambda \begin{Bmatrix} -\eta \\ 1 \end{Bmatrix} \\ &= \begin{bmatrix} K & 0 \\ 0 & 3G \end{bmatrix} \begin{Bmatrix} d\varepsilon_v \\ d\varepsilon_q \end{Bmatrix} - \begin{bmatrix} K & 0 \\ 0 & 3G \end{bmatrix} \begin{Bmatrix} -\eta \\ 1 \end{Bmatrix} \frac{[-\eta K \quad 3G]}{\eta^2 K + 3G} \begin{Bmatrix} d\varepsilon_v \\ d\varepsilon_q \end{Bmatrix} \end{aligned}$$

Formulation of D^{ep} for MC

$$= \left[\begin{bmatrix} K & 0 \\ 0 & 3G \end{bmatrix} - \frac{1}{\eta^2 K + 3G} \begin{bmatrix} K & 0 \\ 0 & 3G \end{bmatrix} \begin{bmatrix} \eta^2 K & -3G\eta \\ -\eta K & 3G \end{bmatrix} \right] \begin{Bmatrix} d\varepsilon_v \\ d\varepsilon_q \end{Bmatrix}$$

$$= \left[\begin{bmatrix} K & 0 \\ 0 & 3G \end{bmatrix} - \frac{1}{\eta^2 K + 3G} \begin{bmatrix} \eta^2 K^2 & -3GK\eta \\ -3GK\eta & 9G^2 \end{bmatrix} \right] \begin{Bmatrix} d\varepsilon_v \\ d\varepsilon_q \end{Bmatrix}$$

$$= \begin{bmatrix} K - \frac{\eta^2 K^2}{\eta^2 K + 3G} & \frac{3GK\eta}{\eta^2 K + 3G} \\ \frac{3GK\eta}{\eta^2 K + 3G} & 3G - \frac{9G^2}{\eta^2 K + 3G} \end{bmatrix} \begin{Bmatrix} d\varepsilon_v \\ d\varepsilon_q \end{Bmatrix}$$

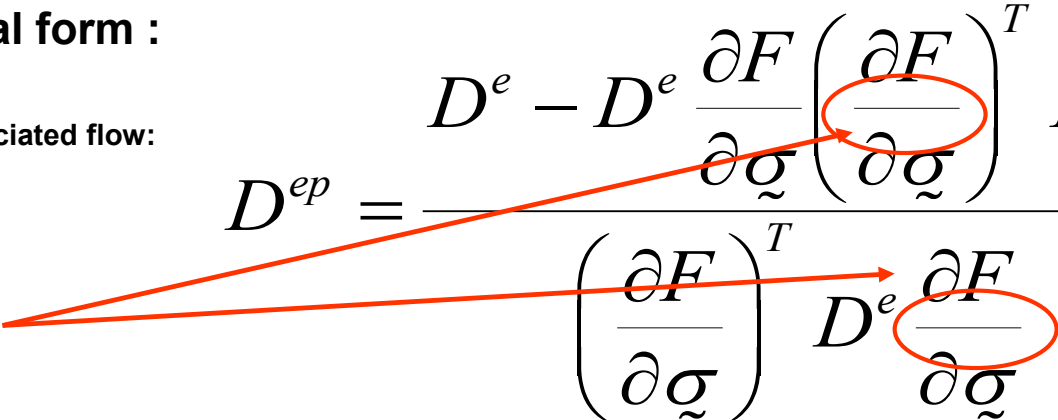
Formulation of D^{ep} for MC

$$D^{ep} = \begin{bmatrix} K - \frac{\eta^2 K^2}{\eta^2 K + 3G} & \frac{3GK\eta}{\eta^2 K + 3G} \\ \frac{3GK\eta}{\eta^2 K + 3G} & 3G - \frac{9G^2}{\eta^2 K + 3G} \end{bmatrix}$$

$\det |D^{ep}| = 0$  perfect plasticity

In general form :

for non associated flow:

$$\frac{\partial Q}{\partial \sigma} D^{ep} = \frac{D^e - D^e \frac{\partial F}{\partial \tilde{\sigma}} \left(\frac{\partial F}{\partial \tilde{\sigma}} \right)^T D^{eT}}{\left(\frac{\partial F}{\partial \tilde{\sigma}} \right)^T D^e \frac{\partial F}{\partial \tilde{\sigma}}}$$


MC model p'-q- space

$$\begin{Bmatrix} \Delta p' \\ \Delta q \end{Bmatrix} = \begin{bmatrix} K' & 0 \\ 0 & 3G' \end{bmatrix} \begin{Bmatrix} \Delta \varepsilon_v^e \\ \Delta \varepsilon_q^e \end{Bmatrix}$$

Assuming associated flow rule and ideal plasticity

$$F(p', q) = q - \eta p' - c^* = 0$$

$$\frac{\partial F}{\partial p'} dp' + \frac{\partial F}{\partial q} dq = 0 \quad : \text{ consistency condition}$$

Formulation of D^{ep} for MC

$$dp' = K (d\varepsilon_v - d\varepsilon_v^p)$$

$$dq = 3G (d\varepsilon_q - d\varepsilon_q^p)$$

$$d\varepsilon_v^{pl} = \lambda \frac{\partial Q}{\partial p'}$$

$$d\varepsilon_q^{pl} = \lambda \frac{\partial Q}{\partial q'}$$

Substituting into consistency condition leads to:

$$dF = \frac{\partial F}{\partial p'} dp' + \frac{\partial F}{\partial q} dq = 0$$

Formulation of D^{ep} for MC

Substituting into consistency condition leads to:

$$dp' = K(d\varepsilon_v - d\varepsilon_v^p)$$

$$dq = 3G(d\varepsilon_q - d\varepsilon_q^p)$$

$$dF = \frac{\partial F}{\partial p'} dp' + \frac{\partial F}{\partial q} dq = 0$$

$$d\varepsilon_v^{pl} = \lambda \frac{\partial Q}{\partial p'}$$

$$dF = \frac{\partial F}{\partial p'} K(d\varepsilon_v - d\varepsilon_v^{pl}) + \frac{\partial F}{\partial q} 3G(d\varepsilon_q - d\varepsilon_q^{pl}) = 0$$

$$d\varepsilon_q^{pl} = \lambda \frac{\partial Q}{\partial q'}$$

$$dF = \frac{\partial F}{\partial p'} K\left(d\varepsilon_v - \lambda \frac{\partial Q}{\partial p'}\right) + \frac{\partial F}{\partial q} 3G\left(d\varepsilon_q - \lambda \frac{\partial Q}{\partial q'}\right) = 0$$

$$\frac{\partial F}{\partial p'} K d\varepsilon_v - \frac{\partial F}{\partial p'} K \lambda \frac{\partial Q}{\partial p'} + \frac{\partial F}{\partial q} 3G d\varepsilon_q - \frac{\partial F}{\partial q} 3G \lambda \frac{\partial Q}{\partial q'} = 0$$

Formulation of D^{ep} for MC

Substituting into consistency condition leads to:

$$dp' = K(d\varepsilon_v - d\varepsilon_v^p)$$

$$dq = 3G(d\varepsilon_q - d\varepsilon_q^p)$$

$$dF = \frac{\partial F}{\partial p'} dp' + \frac{\partial F}{\partial q} dq = 0$$

$$d\varepsilon_v^{pl} = \lambda \frac{\partial Q}{\partial p'}$$

$$\frac{\partial F}{\partial p'} K d\varepsilon_v - \frac{\partial F}{\partial p'} K \lambda \frac{\partial Q}{\partial p'} + \frac{\partial F}{\partial q} 3G d\varepsilon_q - \frac{\partial F}{\partial q} 3G \lambda \frac{\partial Q}{\partial q'} = 0$$

$$d\varepsilon_q^{pl} = \lambda \frac{\partial Q}{\partial q'}$$

$$\frac{\partial F}{\partial p'} K d\varepsilon_v + \frac{\partial F}{\partial q} 3G d\varepsilon_q - \lambda \left(\frac{\partial F}{\partial p'} K \frac{\partial Q}{\partial p'} + \frac{\partial F}{\partial q} 3G \frac{\partial Q}{\partial q'} \right) = 0$$

$$\lambda = \frac{\frac{\partial F}{\partial p'} K d\varepsilon_v + \frac{\partial F}{\partial q} 3G d\varepsilon_q}{\left(\frac{\partial F}{\partial p'} K \frac{\partial Q}{\partial p'} + \frac{\partial F}{\partial q} 3G \frac{\partial Q}{\partial q'} \right)}$$

Formulation of D^{ep} for MC

$$F = q - \eta p' - c^*$$

$$\eta = \frac{6 \sin \phi'}{3 - \sin \phi'}$$

$$\lambda = \frac{\frac{\partial F}{\partial p'} K d\varepsilon_v + \frac{\partial F}{\partial q} 3G d\varepsilon_q}{\left(\frac{\partial F}{\partial p'} K \frac{\partial Q}{\partial p'} + \frac{\partial F}{\partial q} 3G \frac{\partial Q}{\partial q'} \right)}$$

$$Q = q - \xi p'$$

$$\frac{\partial F}{\partial p'} = -\eta$$

$$\frac{\partial F}{\partial q} = 1$$

$$\xi = \frac{6 \sin \psi}{3 - \sin \psi}$$

$$\frac{\partial Q}{\partial p'} = -\xi$$

$$\frac{\partial Q}{\partial q} = 1$$

Formulation of D^{ep} for MC

$$\frac{\partial F}{\partial p'} = -\eta \quad \frac{\partial F}{\partial q} = 1$$

$$\frac{\partial Q}{\partial p'} = -\xi \quad \frac{\partial Q}{\partial q} = 1$$

$$\lambda = \frac{\frac{\partial F}{\partial p'} K d\varepsilon_v + \frac{\partial F}{\partial q} 3G d\varepsilon_q}{\left(\frac{\partial F}{\partial p'} K \frac{\partial Q}{\partial p'} + \frac{\partial F}{\partial q} 3G \frac{\partial Q}{\partial q'} \right)}$$

$$\lambda = \frac{\frac{\partial F}{\partial p'} K d\varepsilon_v + \frac{\partial F}{\partial q} 3G d\varepsilon_q}{\left(\frac{\partial F}{\partial p'} K \frac{\partial Q}{\partial p'} + \frac{\partial F}{\partial q} 3G \frac{\partial Q}{\partial q'} \right)} = \frac{-\eta K d\varepsilon_v + 3G d\varepsilon_q}{(\eta K \xi + 3G)}$$

Formulation of D^{ep} for MC

$$\lambda = \frac{\frac{\partial F}{\partial p'} K d\varepsilon_v + \frac{\partial F}{\partial q} 3G d\varepsilon_q}{\left(\frac{\partial F}{\partial p'} K \frac{\partial Q}{\partial p'} + \frac{\partial F}{\partial q} 3G \frac{\partial Q}{\partial q} \right)} = \frac{-\eta K d\varepsilon_v + 3G d\varepsilon_q}{(\eta K \xi + 3G)}$$

$$\eta = \frac{6 \sin \phi'}{3 - \sin \phi'}$$

$$dp' = K (d\varepsilon_v - d\varepsilon_v^p)$$

$$\xi = \frac{6 \sin \psi}{3 - \sin \psi}$$

$$dq = 3G (d\varepsilon_q - d\varepsilon_q^p)$$

Task for the PhD students (MSc students: 5% extra at the Lecture Test 1 for each case)

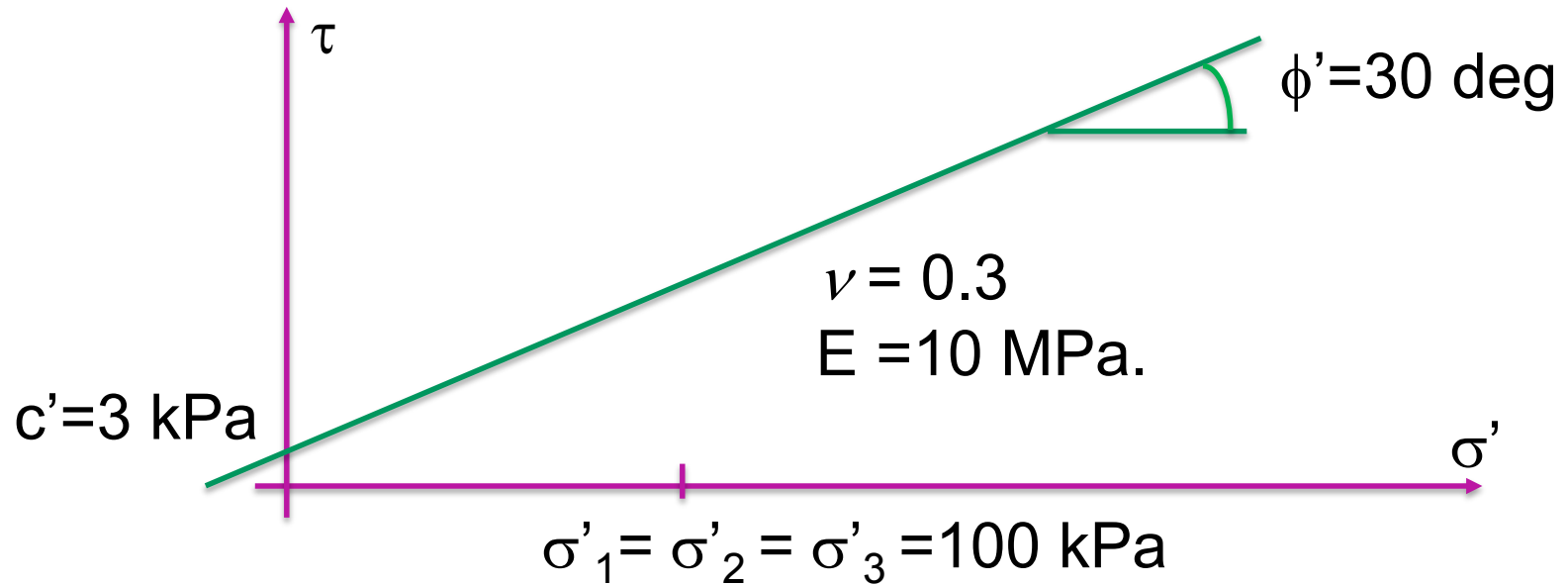
Simulate standard triaxial drained and **undrained tests**, assuming that soil is behaving as a Mohr-Coulomb material.

Assume initial condition $p=100$ kPa, $q=0$.

Assume Mohr-Coulomb soil parameters:

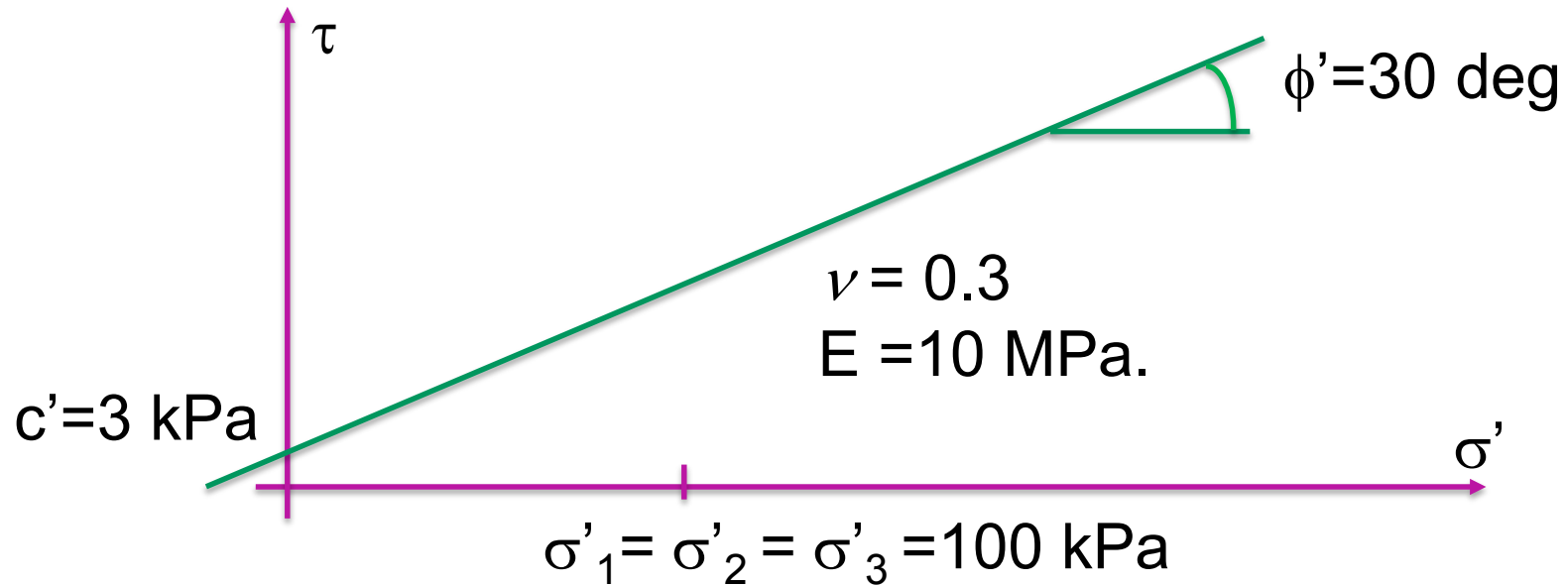
- friction angle 30 degrees
- dilation angle: 0 degrees, 3 degrees, 30 degrees
- cohesion c' equal to 3 kPa
- Poisson's ratio 0.3
- Young's modulus 10 MPa.

Undrained Test



In undrained test, volume is constant

Undrained Test

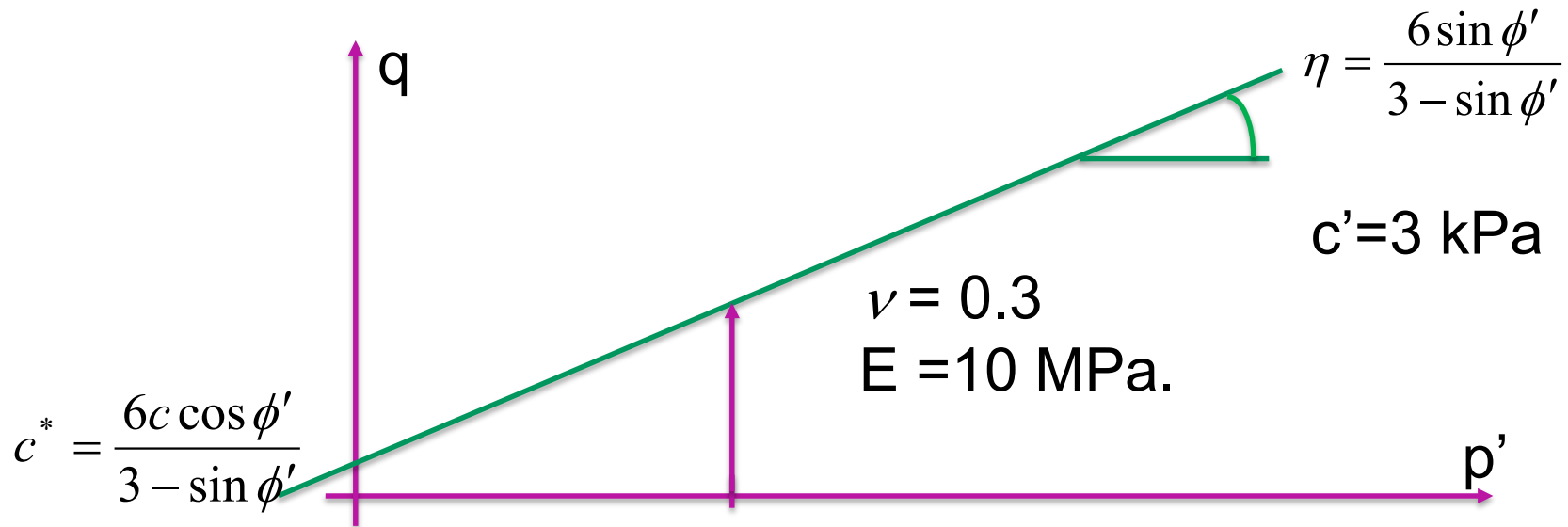


In elasticity no plastic strain, but

$$dp' = K (d\varepsilon_v - d\varepsilon_v^p)$$

$$dq = 3G (d\varepsilon_q - d\varepsilon_q^p)$$

Undrained Test



$$F = q - \eta p' - c^*$$

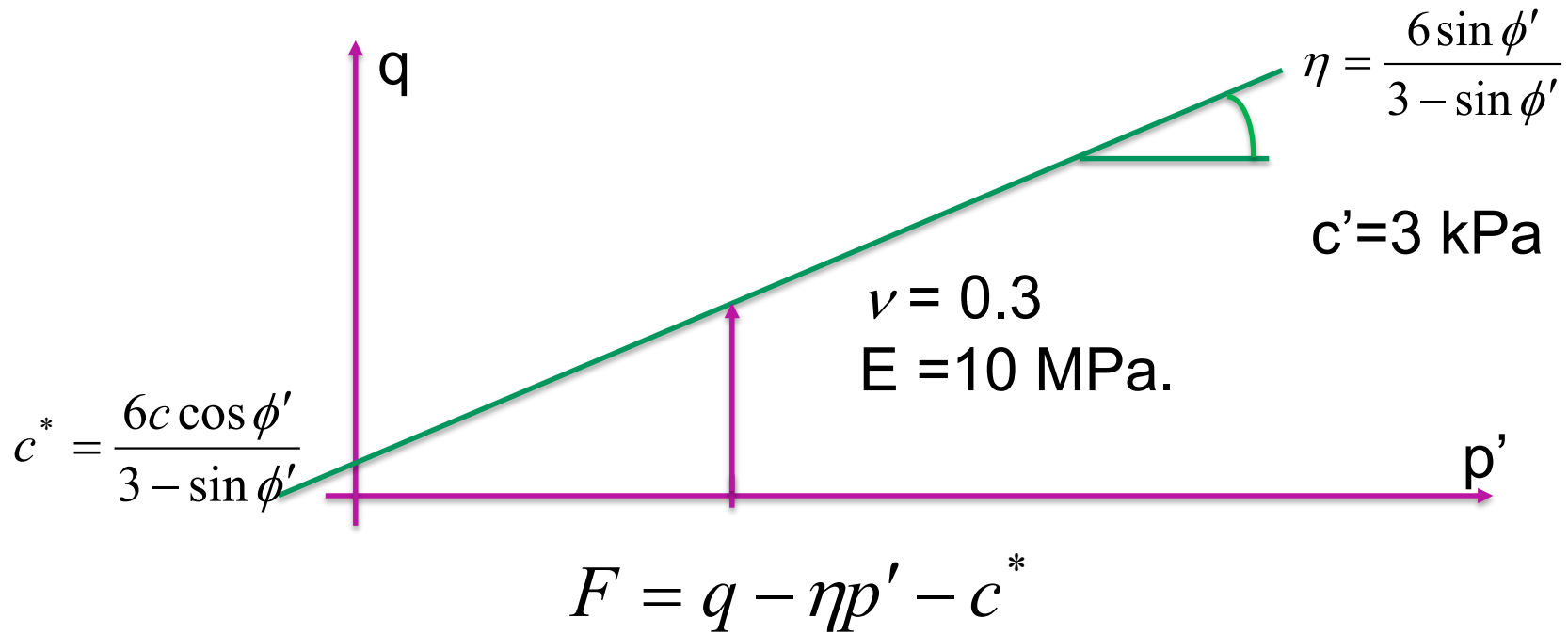
So, dp' must be zero...

All the change in p , must be turned into u

$$dp' = K (d\varepsilon_v - d\varepsilon_v^p)$$

$$dq = 3G (d\varepsilon_q - d\varepsilon_q^p)$$

Undrained Test



So, at yield, $p' = 100 \text{ kPa}$, $q = \eta p' + c^*$

Undrained Test

After yield, same equations, but we demand that

$$d\varepsilon_v = 0 = d\varepsilon_v^{el} + d\varepsilon_v^{pl}$$

Instead of having $q/p'=3$

Undrained Test

After yield, same equations, but we demand that

$$d\varepsilon_v = 0 = d\varepsilon_v^{el} + d\varepsilon_v^{pl}$$

$$\eta = \frac{6 \sin \phi'}{3 - \sin \phi'}$$

$$\xi = \frac{6 \sin \psi}{3 - \sin \psi}$$

$$\lambda = \frac{-\eta K d\varepsilon_v + 3G d\varepsilon_q}{(\eta K \xi + 3G)}$$

$$dp' = K (d\varepsilon_v - d\varepsilon_v^p)$$

$$dq = 3G (d\varepsilon_q - d\varepsilon_q^p)$$

we also know that $u=p-p'$ and $q/p=3$

Thank you