

Lecture 5 - AAE-E3030:

A Model of Premixed Combustion

March 25th Ville Vuorinen



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B

A

Q1) Why and how 'premixed' ?

Q2) Typical flow velocities ?

Q3) Are the flames rotationally symmetric ?

Q4) Shape and structure of the flame ?

Q5) Where is the rate of highest heat release ?

Q6) Pressure/density/velocity/temperature/ C_p at points A and B ?

Lecture 5 in the Multiphase Course Timetable

- Lectures 1-2 → Fuel drops/multiphase flows
- Lectures 3-4 → Premixed 0d chemistry Warnatz
Ch. 8, 10, 15
- **Lecture 5 → Premixed combustion 1d & 2d**
- Lectures 6-7 → Premixed 1d chemistry
- Lecture 8 → Non-premixed combustion

Motivation

Combustor (partially premixed ?)

<https://www.youtube.com/watch?v=B7OajNkGp80>

Acoustics and flames (acoustic modulation)

https://www.youtube.com/watch?v=EQXcOqH_Drs&list=PLxAI1X0qwonL1OyfLgfjonQSVFH8AdXnT

Flame blowoff and flashback (influence of inflow rate)

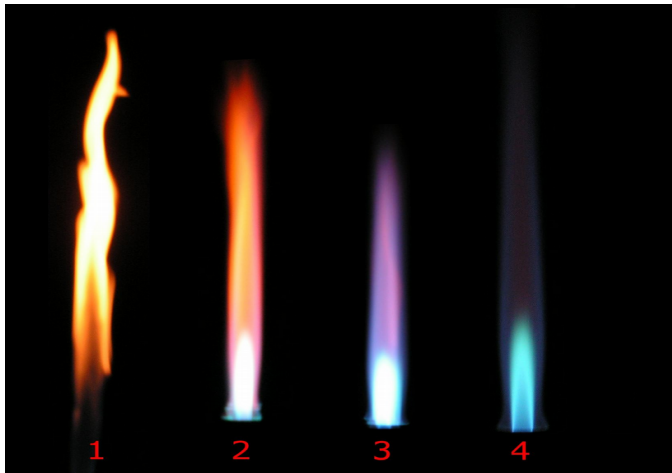
<https://www.youtube.com/watch?v=KmyGR6mSPe0&list=PLxAI1X0qwonL1OyfLgfjonQSVFH8AdXnT&index=2>

LES of premixed combustor (influence of swirl and recirculation techniques)

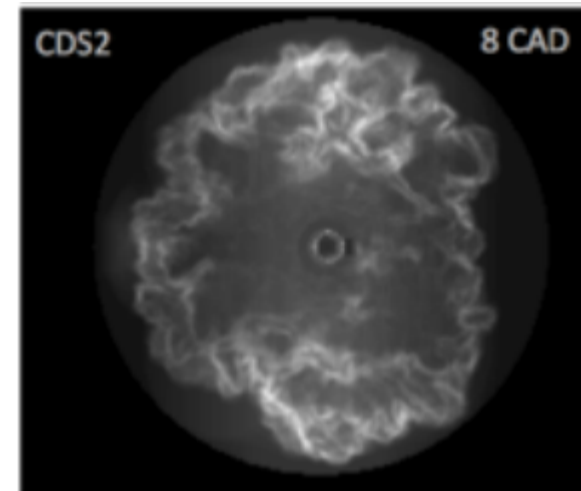
<https://www.youtube.com/watch?v=Mim33CvQTUQ>

Spark ignition of premixed gas (advantages of mixture uniformity thanks to premixing)

<https://www.youtube.com/watch?v=xg3Ri1-1rCE>

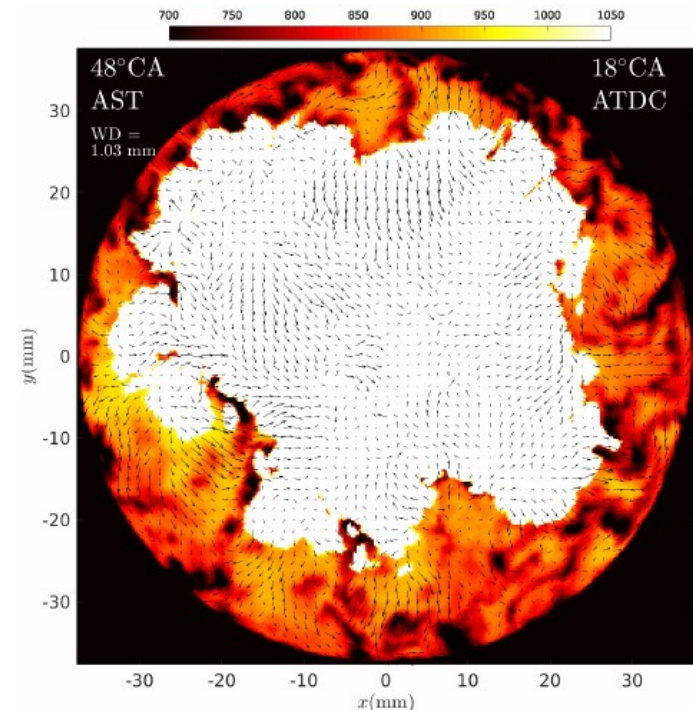
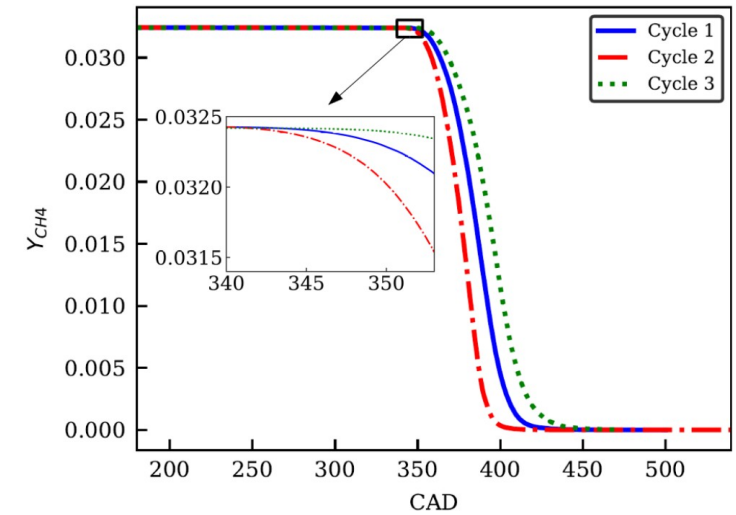
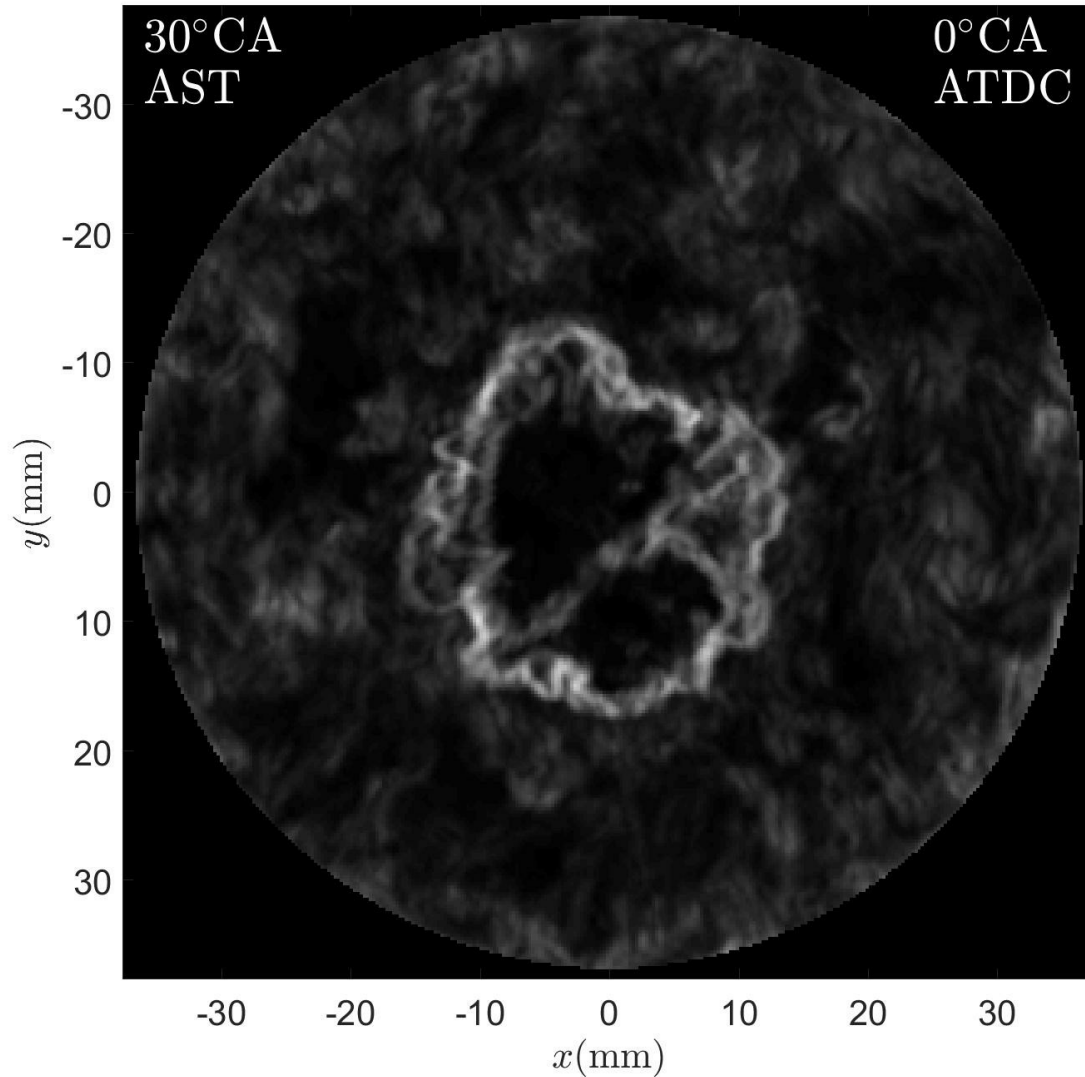


LES simulation of spark ignited fuel

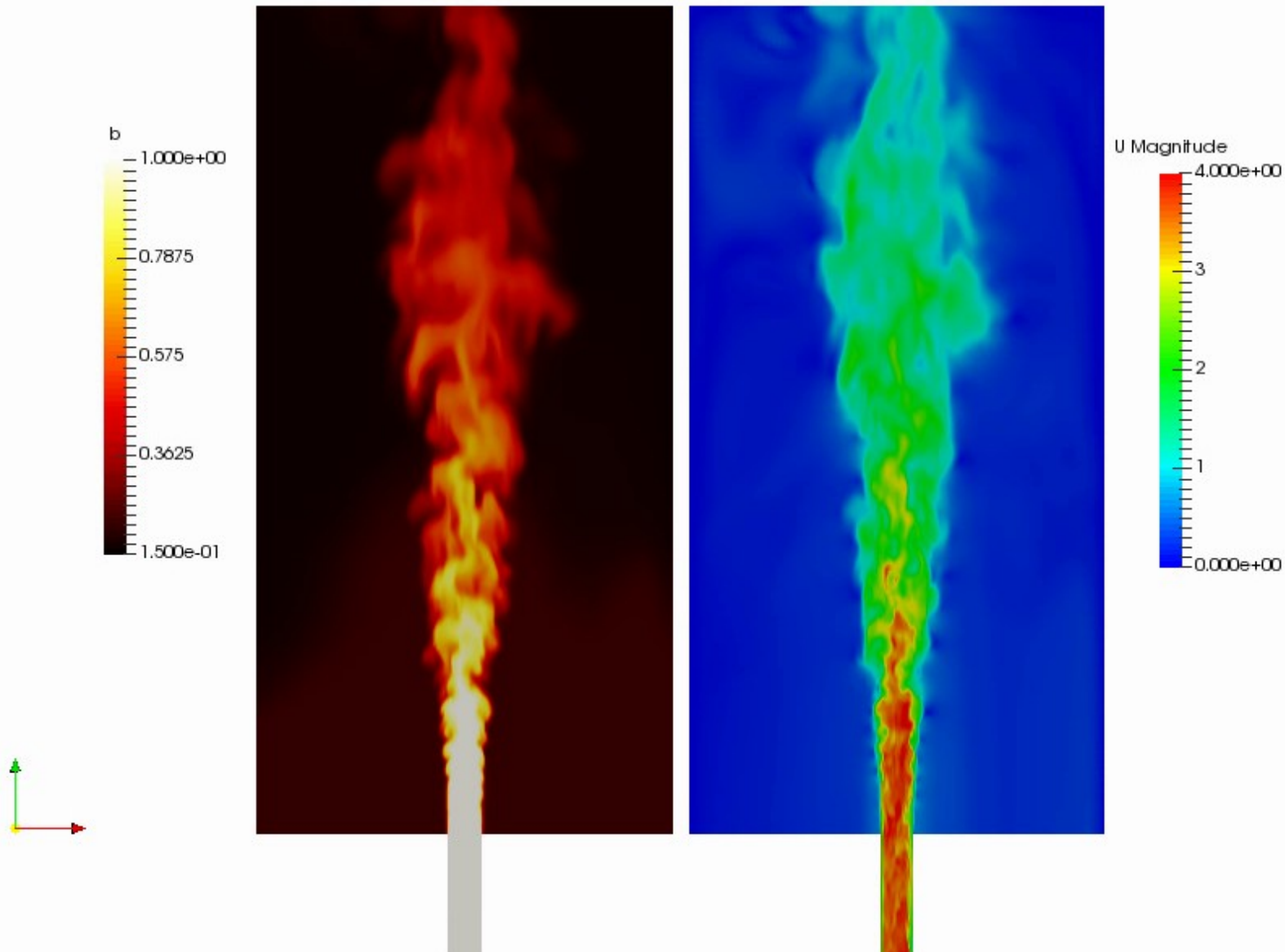


Courtesy of: Nguyen and Kempf, LES4ICE conference (2016)

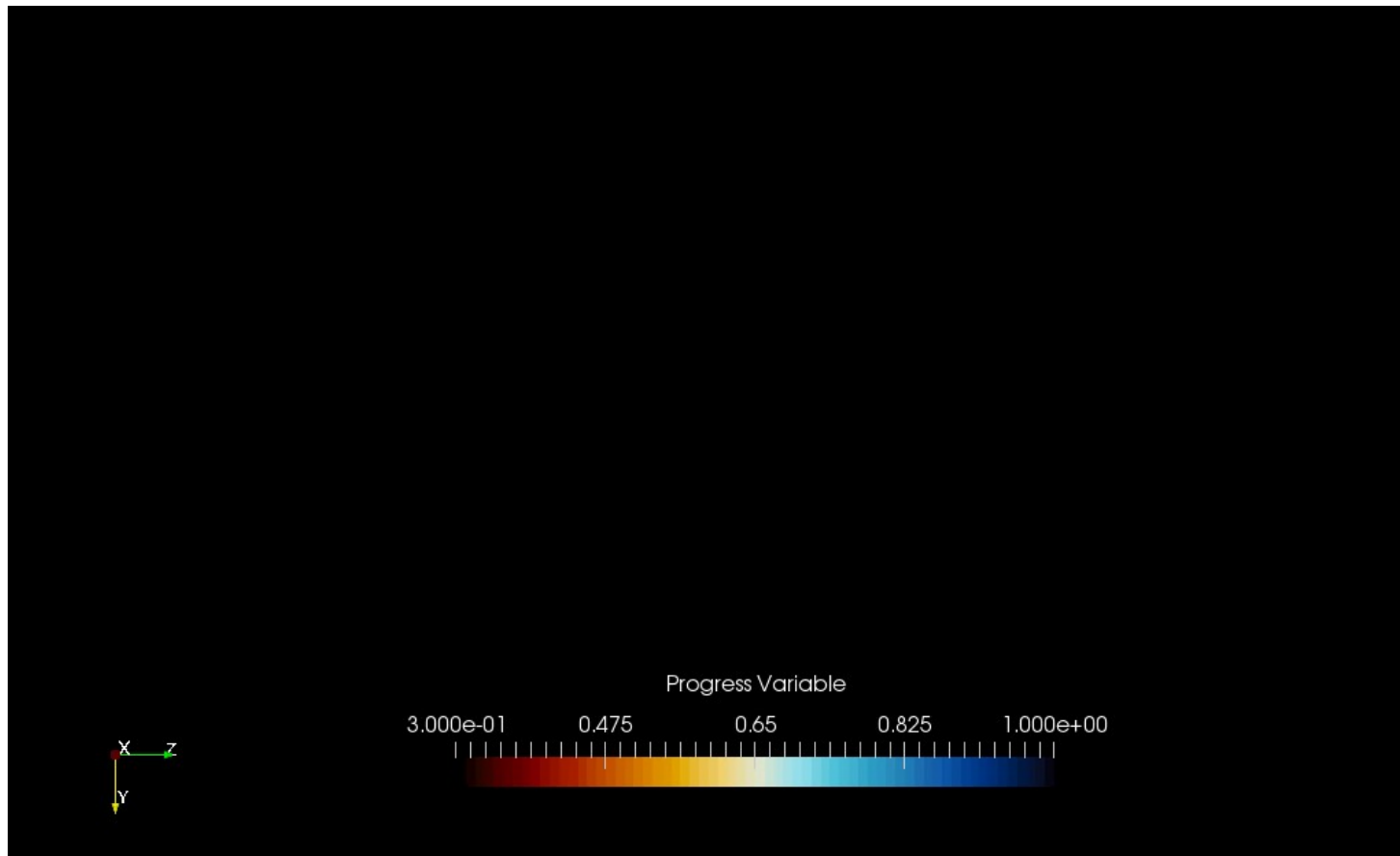
Large-Eddy Simulation (LES CFD method) on Spark-Ignited (SI), Premixed Methane-Air Combustion



Typical scalar (e.g. concentration of incoming gas A) and velocity fields in a turbulent jet

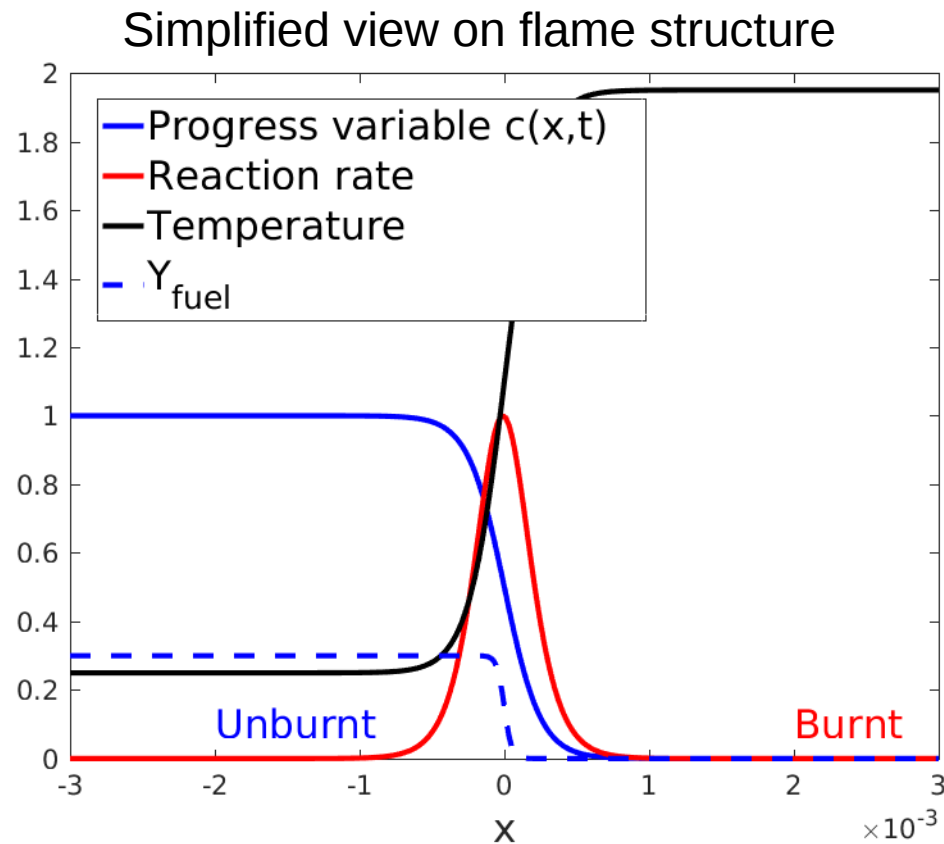


Simulation of premixed flame for different flame speeds

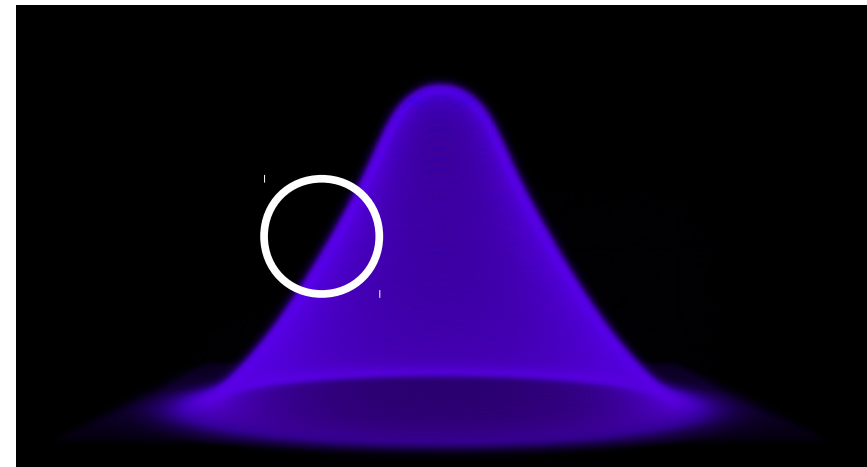


Courtesy of B.Tekgul (2017)

We look next on a simplified model on premixed flame and imagine how the flame would look like locally



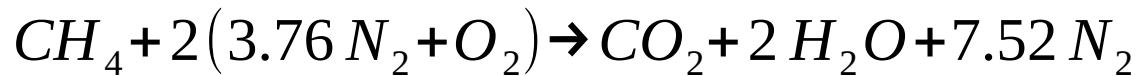
Locally, flame is considered to be 1 dimensional in the direction of flame surface normal



Important concept: S_L = laminar flame speed

Some assumptions

Single step reaction of premixed fuel and air either lean, stoichiometric or rich. For example:



The deflagration type flame front thickness is thin, simple scaling estimates:

$$\delta = \frac{\lambda_{therm}}{\rho c_p S_L} = \frac{D_{therm}}{S_L} \quad \text{Re}_{flame} = \frac{S_L \delta}{D_{therm}} = 1$$

A progress variable describes flame evolution:

$$c = \frac{Y_f^b - Y_f}{Y_f^b - Y_f^u} \quad \begin{array}{l} c=1 \rightarrow \text{unburnt} \\ c=0 \rightarrow \text{burnt} \end{array} \quad T \approx (1-c) T_b + c T_u$$

1d Convection-Reaction Equation for c i.e. c-equation

$$\frac{\partial \rho c}{\partial t} + \frac{\partial \rho c u}{\partial x} = -\rho_u S_L \left| \frac{\partial c}{\partial x} \right|$$

Progress variable Velocity Unburnt density Laminar flame speed

Time derivative Convection term Reaction source term

High at burnt/unburnt interface

Progress variable approach in general (1D, 2D and 3D)

$$\frac{\partial \rho c}{\partial t} + \nabla \cdot \rho c \mathbf{u} = -S_d \rho_u |\nabla c|$$

Interplay of thermal diffusion and global reaction rate consumes fuel

$S_d = \text{displacement speed}$

$$S_d = S_L (1 - L_M \kappa - S)$$

Correction terms for curved and strained plane fronts (deviation from plane flame, uniform ambient flow Assumption).

Markstein length

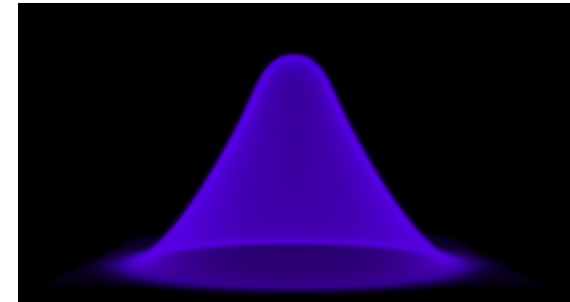
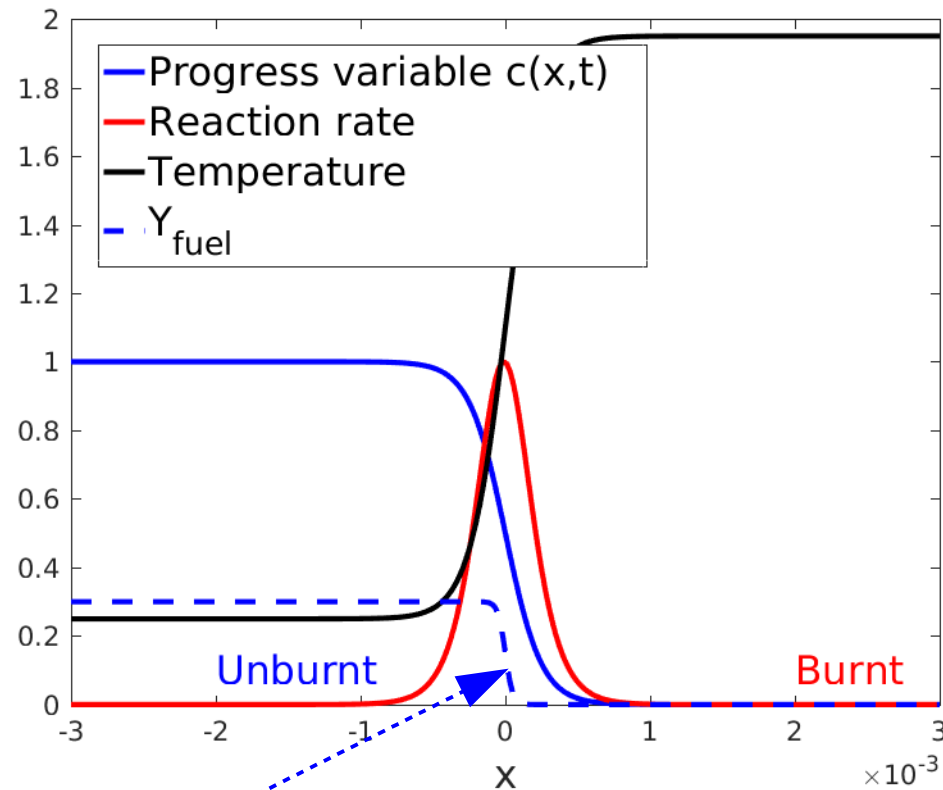
Curvature

Strain

$$\kappa = \nabla \cdot \mathbf{n}$$

$$\mathbf{n} = \frac{\nabla c}{|\nabla c|}$$

C-equation says: “We look at an averaged flame on scales much larger than flame thickness. To describe flame propagation we need model for 1) reaction rate, 2) flame speed, and 3) burnt/unburnt thermodynamics.”



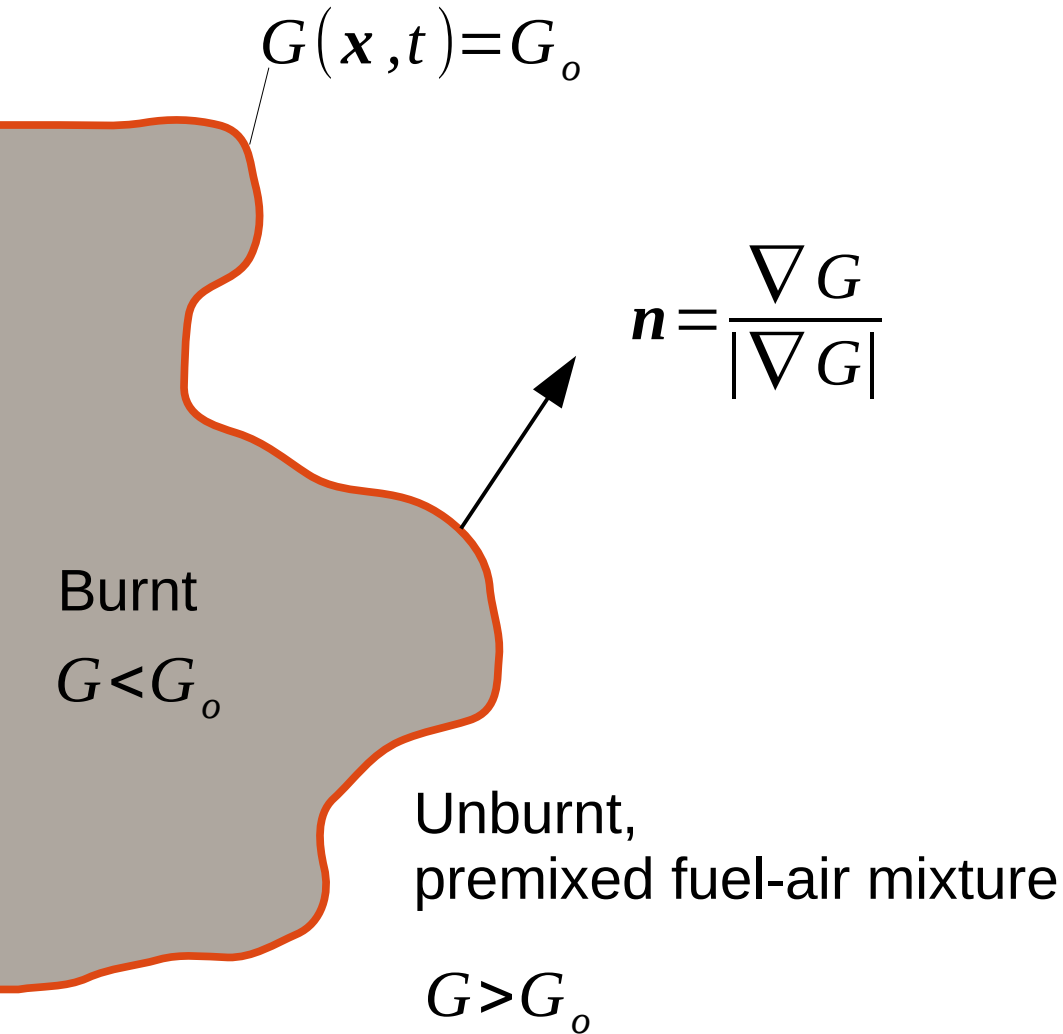
The real fuel mass fraction profiles are not captured.

$$\delta \ll \Delta x$$

$\Delta x = \text{grid spacing}$

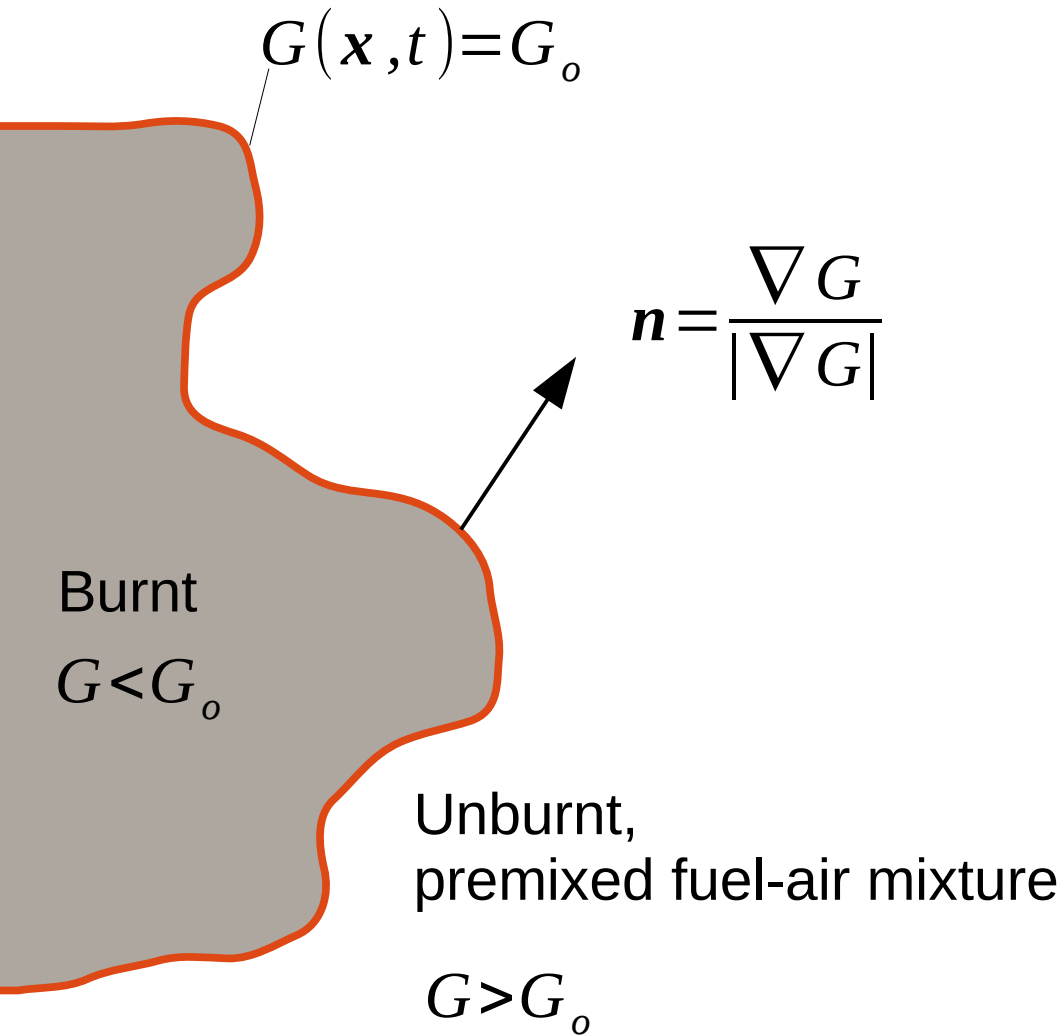
Premixed Combustion as Flame Propagation Phenomenon

G-equation (Markstein 1964, Williams 1985)



Premixed Combustion as Flame Propagation Phenomenon

G-equation (Markstein 1964, Williams 1985)



$$\frac{dG(\mathbf{x}, t)}{dt} = \frac{\partial G}{\partial t} + \frac{d\mathbf{x}_f}{dt} \cdot \nabla G = 0$$

$$\frac{d\mathbf{x}_f}{dt} = \mathbf{u} + S_f \mathbf{n}$$

$$\frac{\partial G}{\partial t} + \mathbf{u} \cdot \nabla G = -S_f |\nabla G|$$

$$-S_f |\nabla G| \quad \text{Reaction source term}$$

$$\mathbf{u} \cdot \nabla G \quad \text{Convection term}$$

$$\frac{\partial G}{\partial t} \quad \text{Time derivative term}$$

Some Available Options as Premixed Combustion CFD Model (May Apply to Non-Premixed as Well)

Model family/concept	Some assumptions	What the model typically needs?	Benefits	Some Drawbacks
G-equation (Markstein 1964, Williams 1985)	<ul style="list-style-type: none"> - physical flame thickness $\delta \ll \Delta x$ - flame at $G = \text{const.}$ i.e. level-set approach - separation to burnt and unburnt regions 	<ul style="list-style-type: none"> - Correlation S_L - an algorithm to find the flame position 	<ul style="list-style-type: none"> - single equation to describe premixed combustion 	<ul style="list-style-type: none"> - $G=G(x,y,z,t)$ has no physical meaning elsewhere than at flame - level set approach so the flame really needs to be tracked \rightarrow complications for implementation
Flame surface density (c-equation)	<ul style="list-style-type: none"> - Thin flame $\delta \ll \Delta x$ - c is defined everywhere in contrast to level-set - 	<ul style="list-style-type: none"> - Correlation S_L - Correlation for flame surface density (effect of unresolved flame deviation from planar) 	<ul style="list-style-type: none"> - single equation to describe premixed combustion - rather simple to implement 	<ul style="list-style-type: none"> - assumption of single step chemistry - a particular link between emissions and c needed - possibly even extra eqn for surface density needed
Flamelet method	<ul style="list-style-type: none"> - flame=ensemble of 1d flames 	<ul style="list-style-type: none"> - pre-calculated chemistry look-up tables 	<ul style="list-style-type: none"> - fast in runtime with accurate description of species from tables 	<ul style="list-style-type: none"> - pre-tabulation can be a tedious task
Direct chemistry	<ul style="list-style-type: none"> - full Navier-Stokes + species eqs solved - flame is resolved DNS 	<ul style="list-style-type: none"> - low Reynolds number - accurate diffusion model 	<ul style="list-style-type: none"> - computational 'experiment' with all possible data available 	<ul style="list-style-type: none"> - very heavy and limited to small mechanisms
Thickened flame	<ul style="list-style-type: none"> - flame artificially thickened to numerically resolve the flame - reaction rate scaled by L and thermal diffusivity by $1/L$ while S_L is const. 	<ul style="list-style-type: none"> - reduced or accurate chemical mechanism which gives correct flame speed and IDT 	<ul style="list-style-type: none"> - flame front is really resolved with important species 	<ul style="list-style-type: none"> - is the physics still the same ?

Assumptions of this eqn?

$$\rho U \sin(\alpha) = \rho_u S_L$$

Bunsen Flame – Background

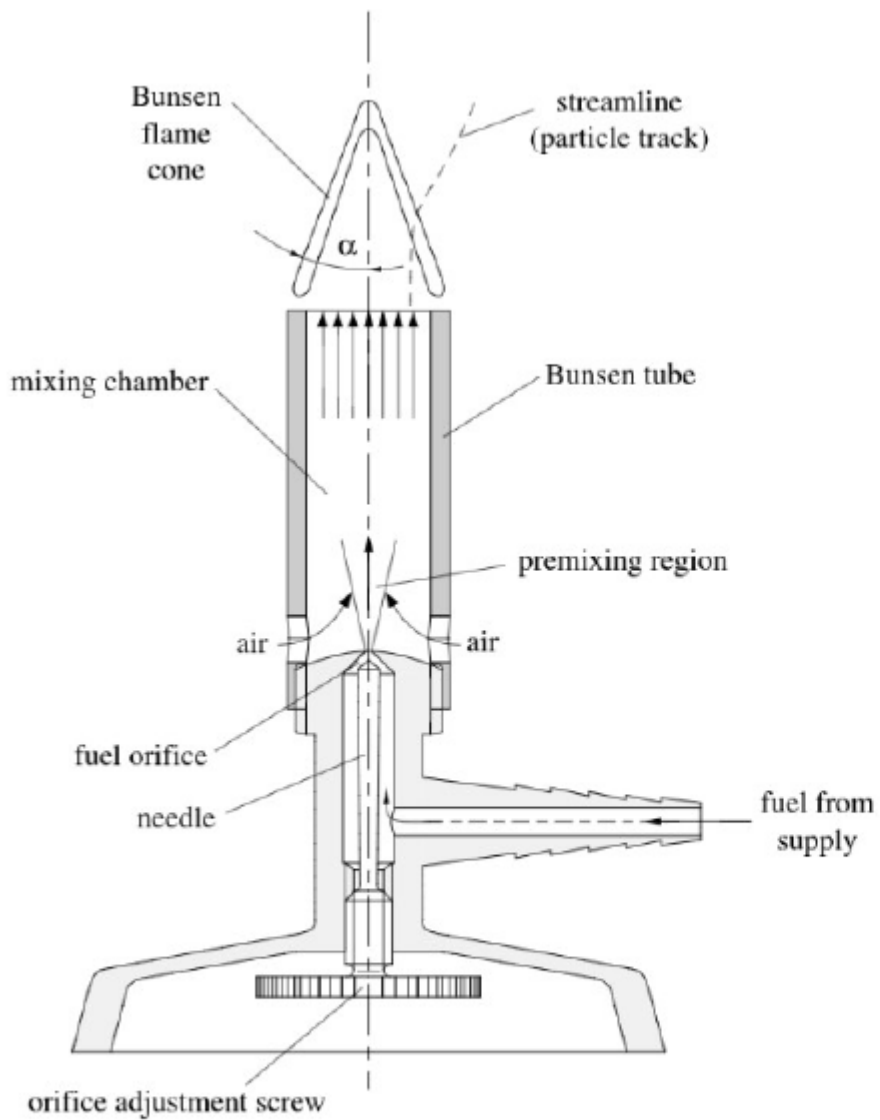


Figure 1 : Typical Bunsen burner. (Peters. Turbulent combustion)

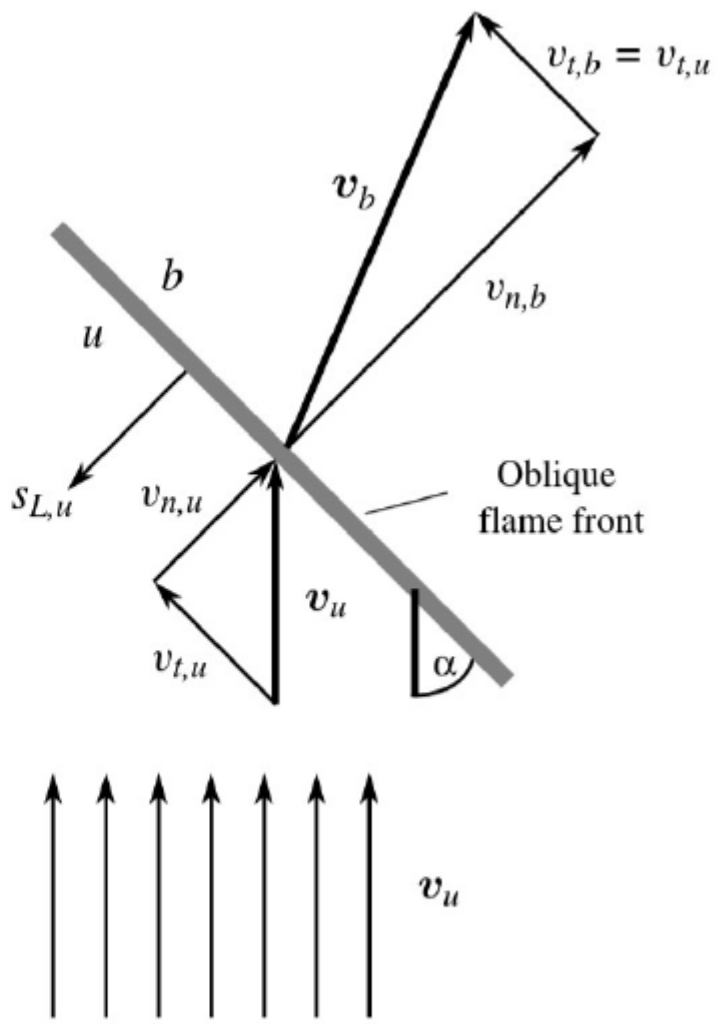


Figure 2 : Kinematic balance for a steady oblique Bunsen flame. (Peters. Turbulent combustion)

Compressible fluid flows: Full Navier-Stokes Equations

$$\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_j}{\partial x_j} = 0$$

Mass conservation

Viscous stress tensor

$$\sigma_{ij} = \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) - \frac{2}{3} \mu \frac{\partial u_i}{\partial x_j} \delta_{ij}$$

$$\frac{\partial \rho u_i}{\partial t} + \frac{\partial \rho u_i u_j}{\partial x_j} = - \frac{\partial p}{\partial x_i} + \frac{\partial \sigma_{ij}}{\partial x_i}$$

Momentum conservation

Internal energy

$$e = c_v T + \frac{1}{2} u_i^2$$

$$\frac{\partial \rho e}{\partial t} + \frac{\partial (\rho e + p) u_j}{\partial x_j} = \frac{\partial u_i \sigma_{ij}}{\partial x_i} + \frac{\partial}{\partial x_i} \lambda \frac{\partial T}{\partial x_i}$$

Energy conservation

$$p = \rho R T$$

Note: 1 + 3 + 1 equations, the set is closed by the equation of state

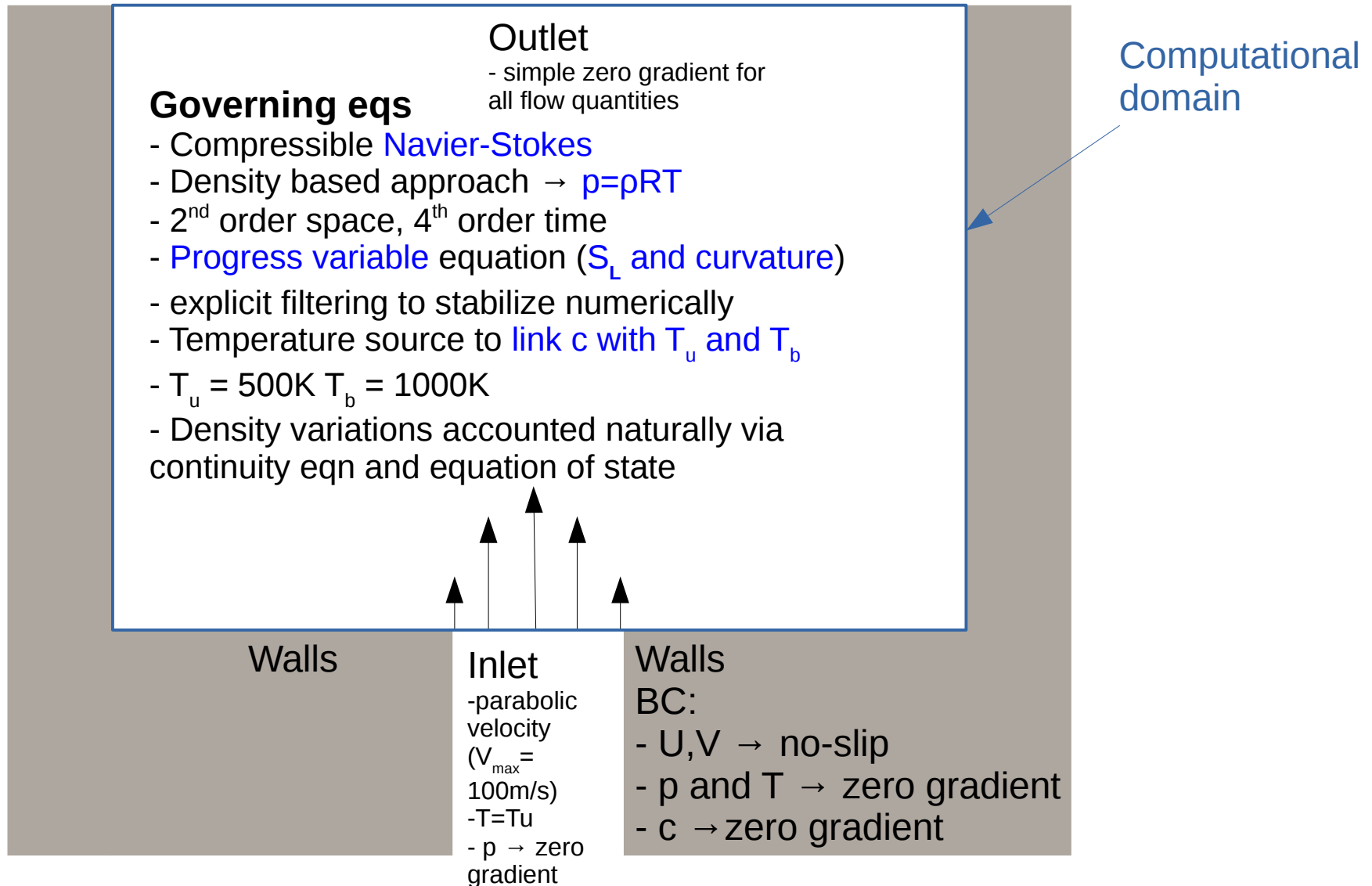
Note 1: Possible viscosity model: Sutherland

Note 2: Specific heat is in general temperature dependent

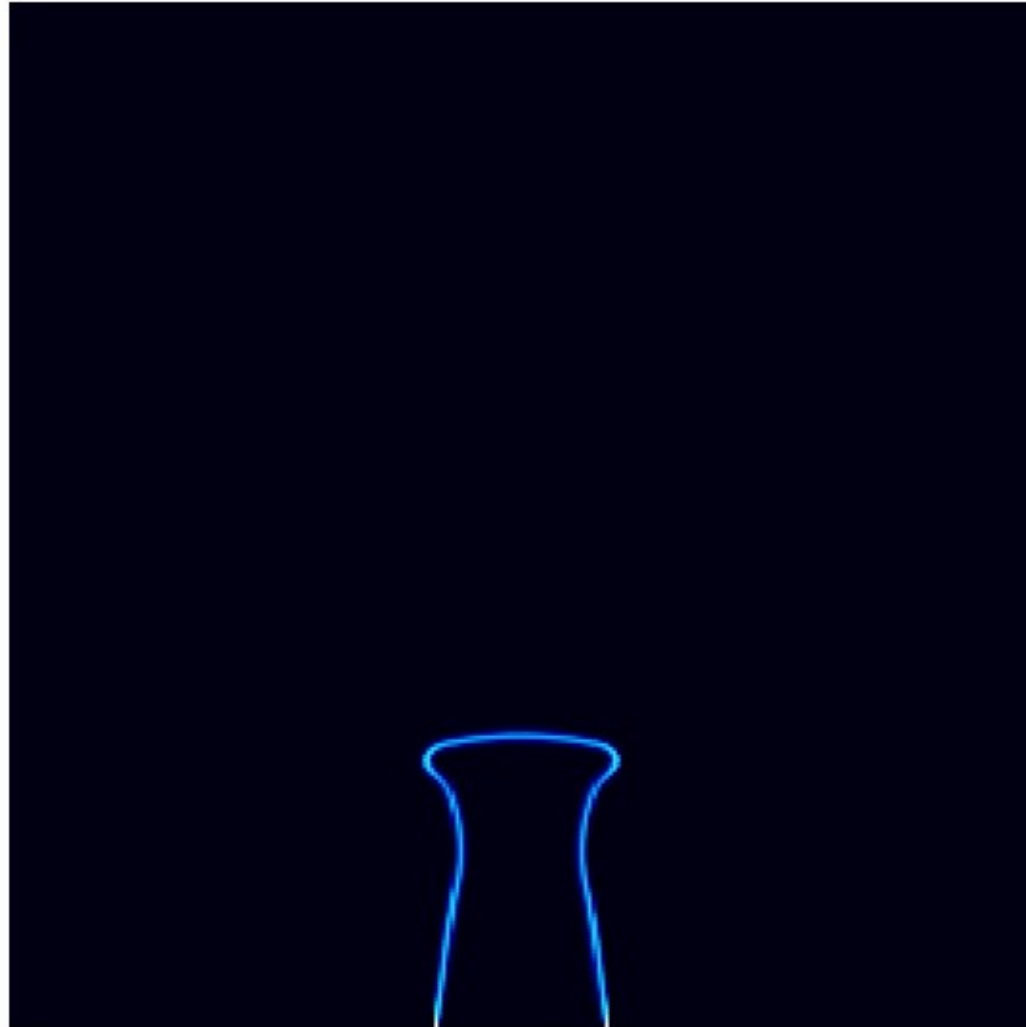
Simplified Matlab Code for Simulating Premixed Slot Burner

- **2d Navier-Stokes** equations of gas dynamics i.e. mass, momentum, and energy conservation
- **c-equation** to describe burnt/unburnt region
- Runge-Kutta 4 time integration
- Premixed combustion of a **prototype** “fuel” with $T_u = 500K$ $T_b = 1000K$
- Density effect accounted for via NS-eqs (continuity, momentum eqs)
- Ideal gas law **$p = \rho RT$**
- The code can simulate 1) Bunsen burner, 2) Flame propagation in 2d “quasi-turbulence”

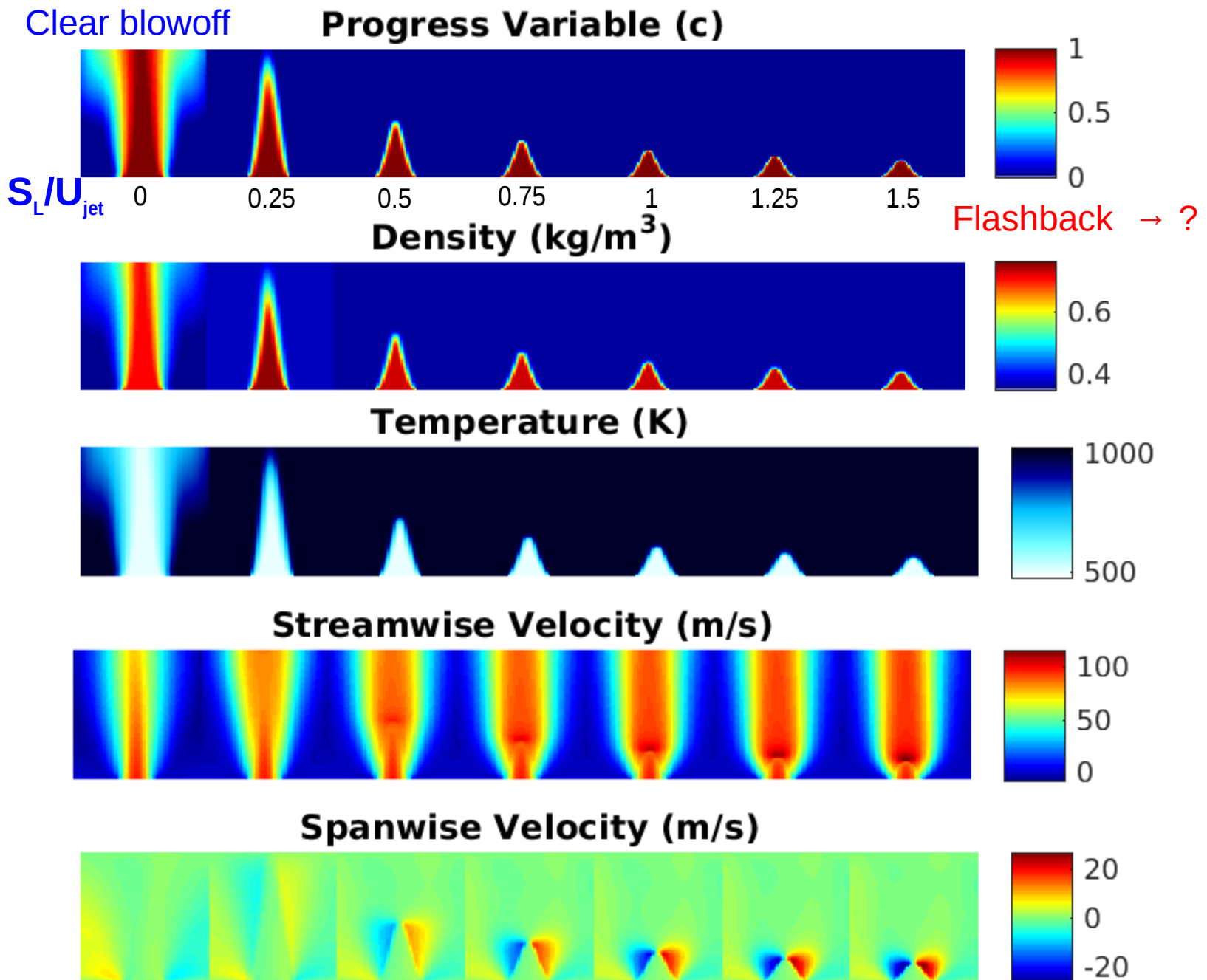
Bunsen Flame – Domain Modeled as a 2d “Slot” Burner in the Matlab Code



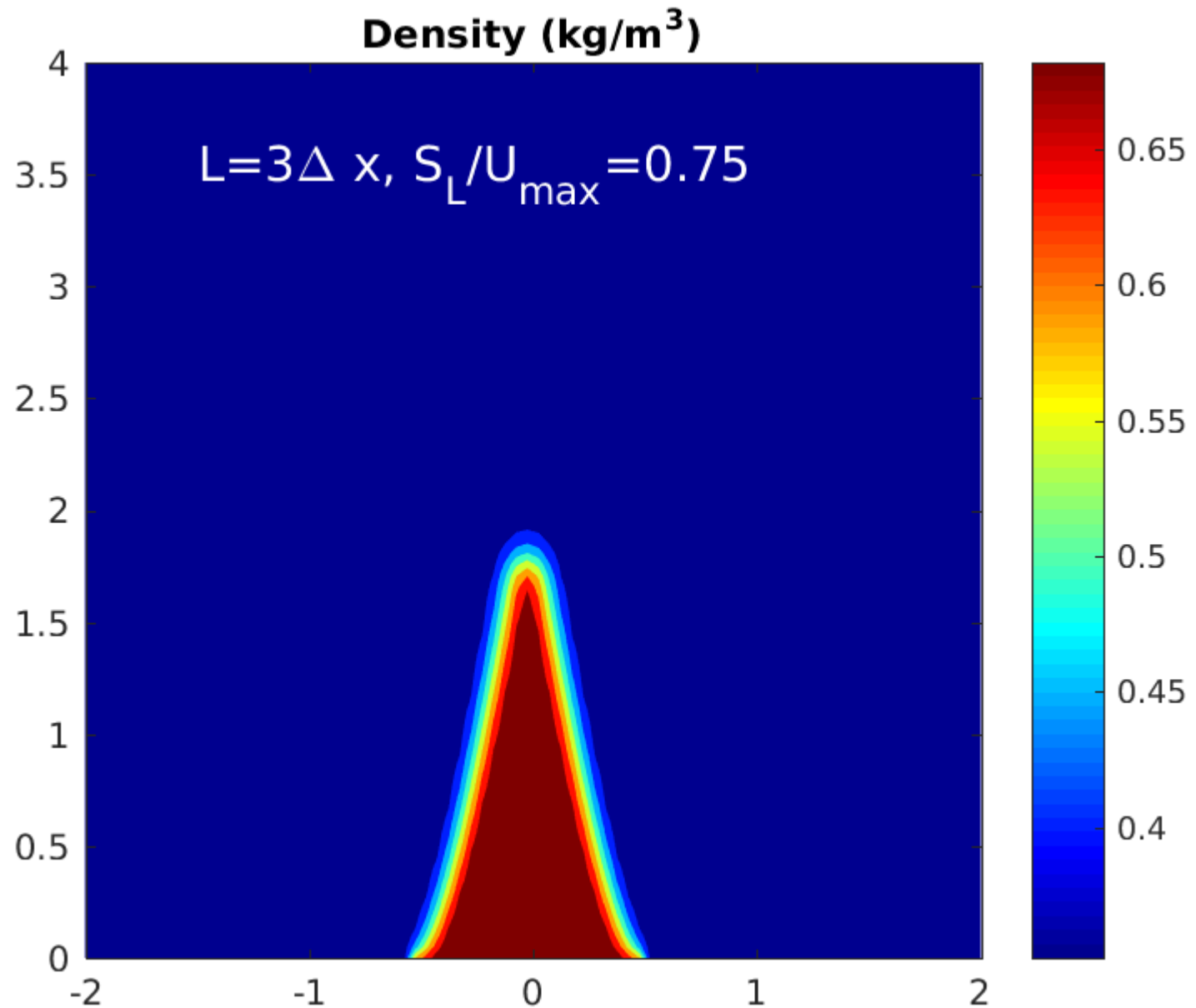
Bunsen Flame – This Case is With Top-Hat Velocity Profile Instead of Parabolic ($S_L/U_{jet}=0.75$). High Reynolds number.



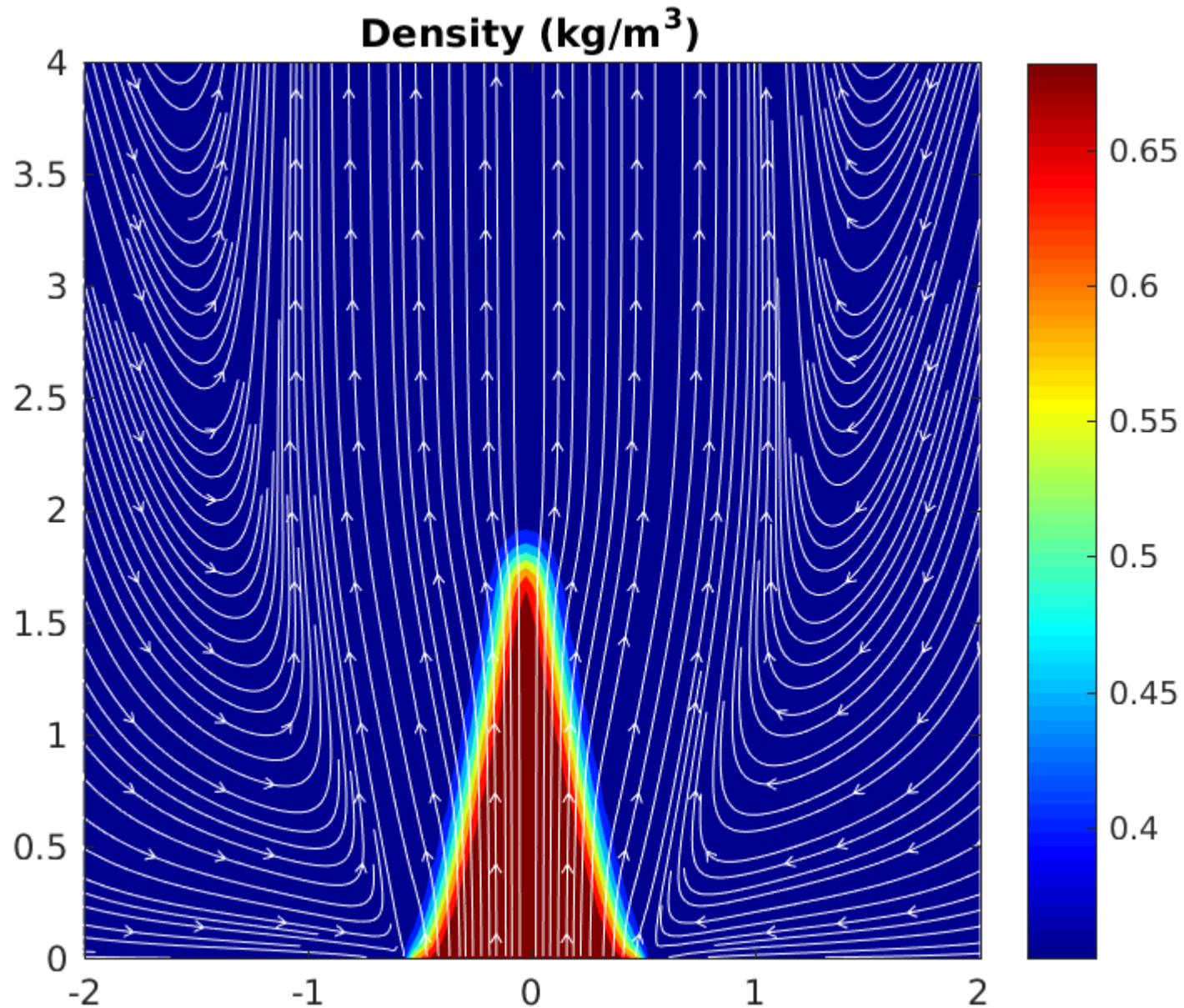
Bunsen Flame – Influence of Laminar Flame Speed (S_L/U_{jet})



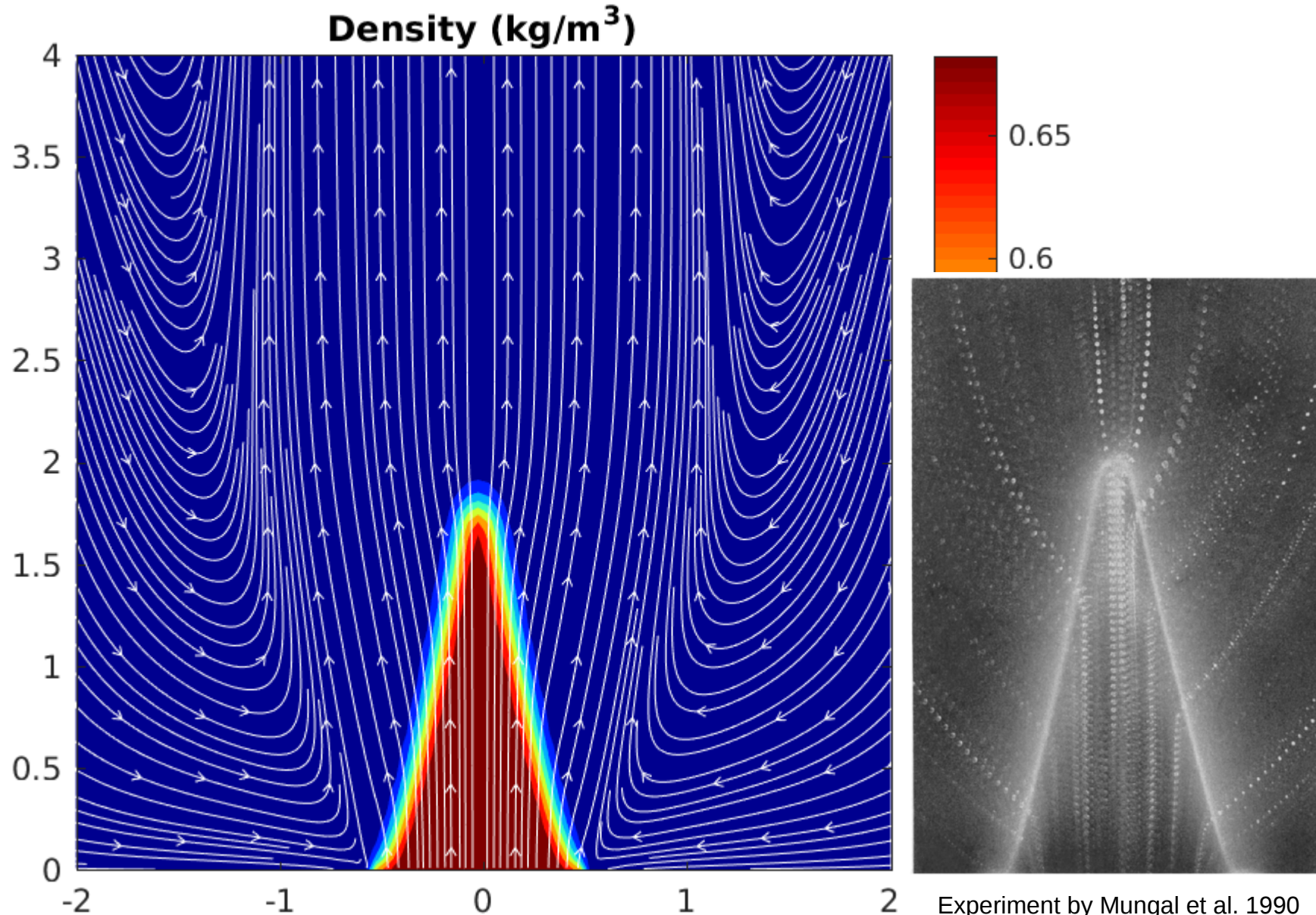
Bunsen Flame – Burnt vs Unburnt Density



Bunsen Flame – Burnt vs Unburnt Density and Streamlines

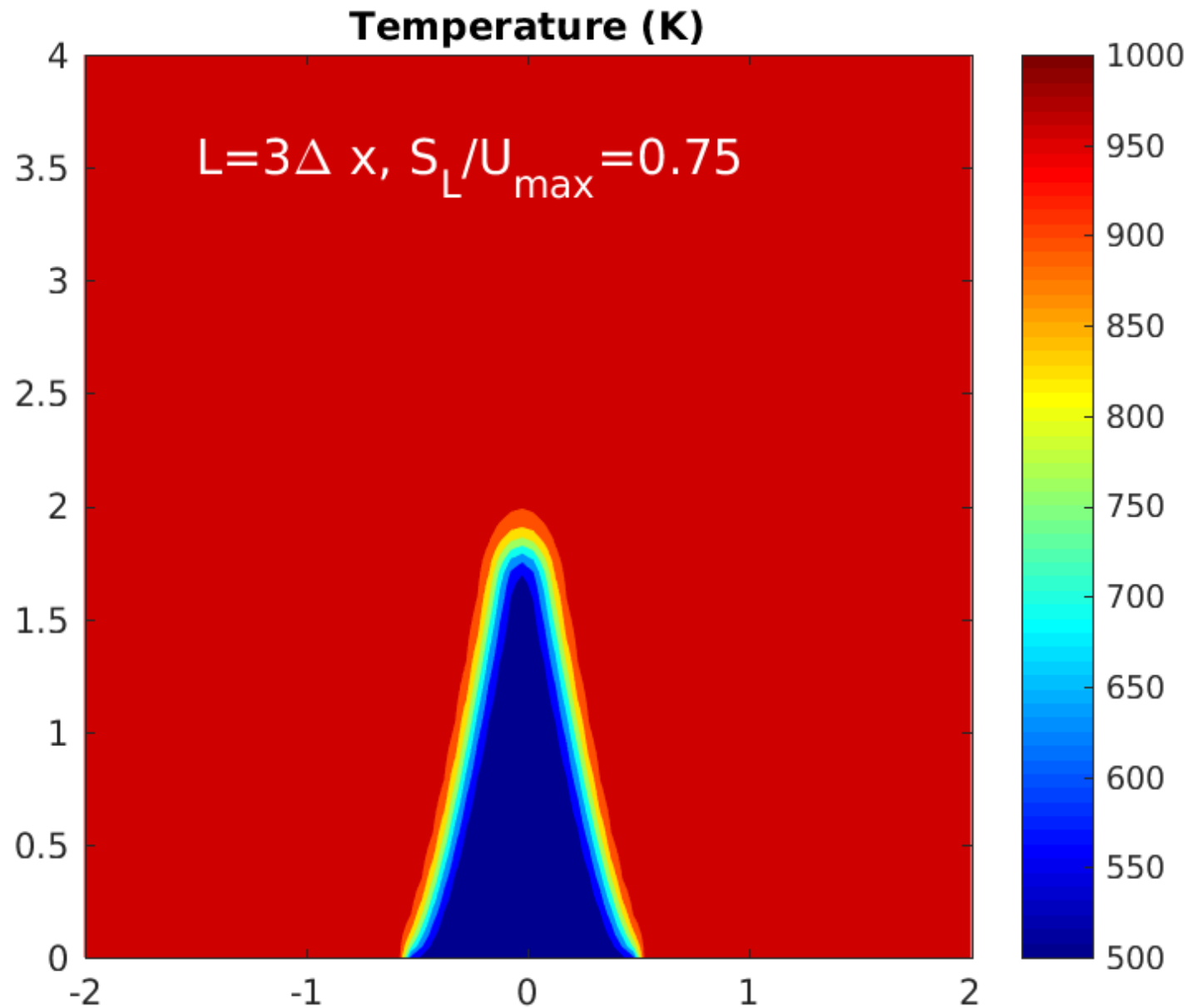


Bunsen Flame – Burnt vs Unburnt Density and Streamlines

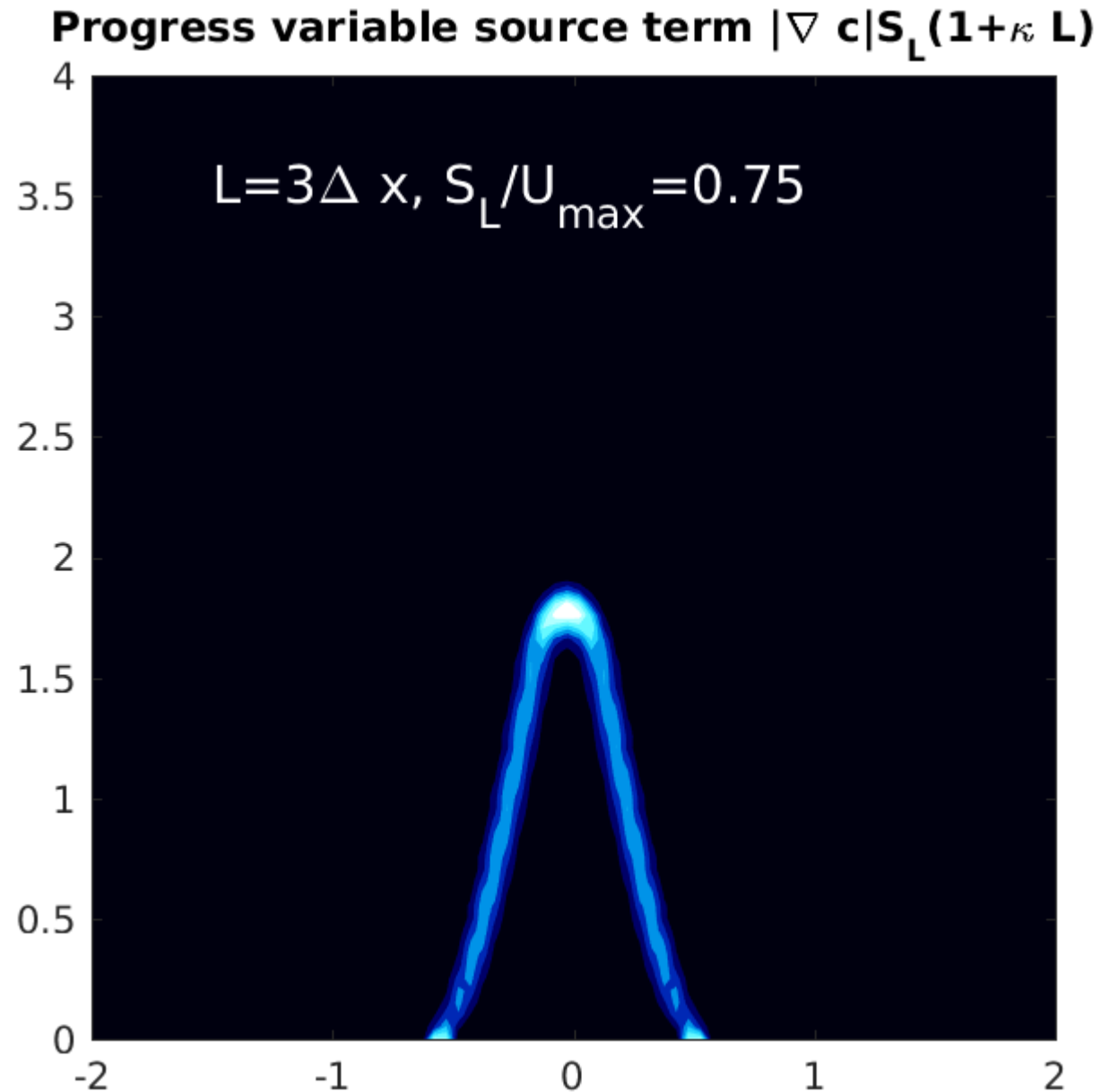


Experiment by Mungal et al. 1990
Symp. Comb. Institute

Bunsen Flame – Burnt vs Unburnt Density

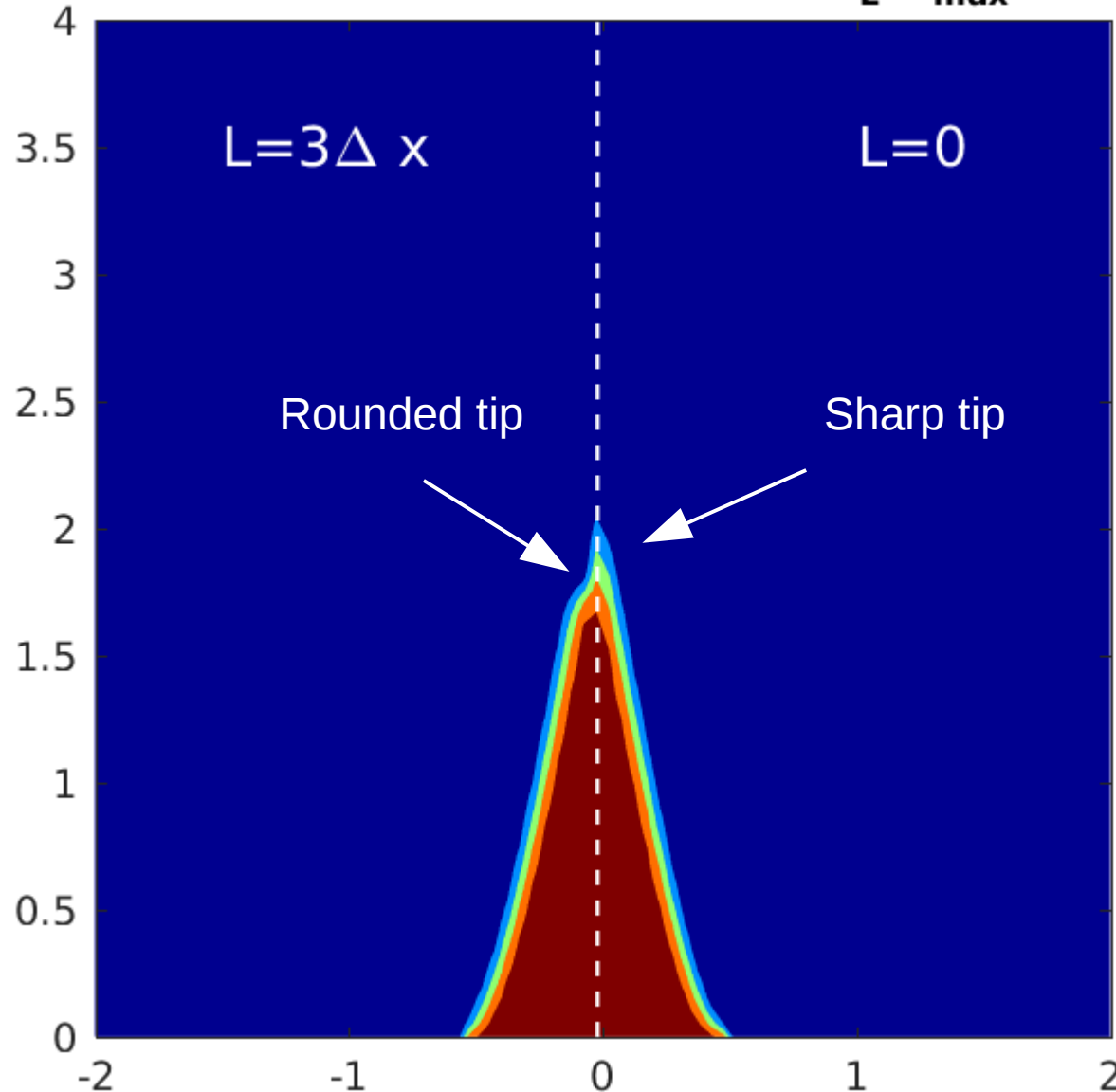


Bunsen Flame – Burnt vs Unburnt Density



Bunsen Flame – Curvature and Markstein Length Effect

Markstein length and flame tip ($S_L/U_{\max}=0.75$)



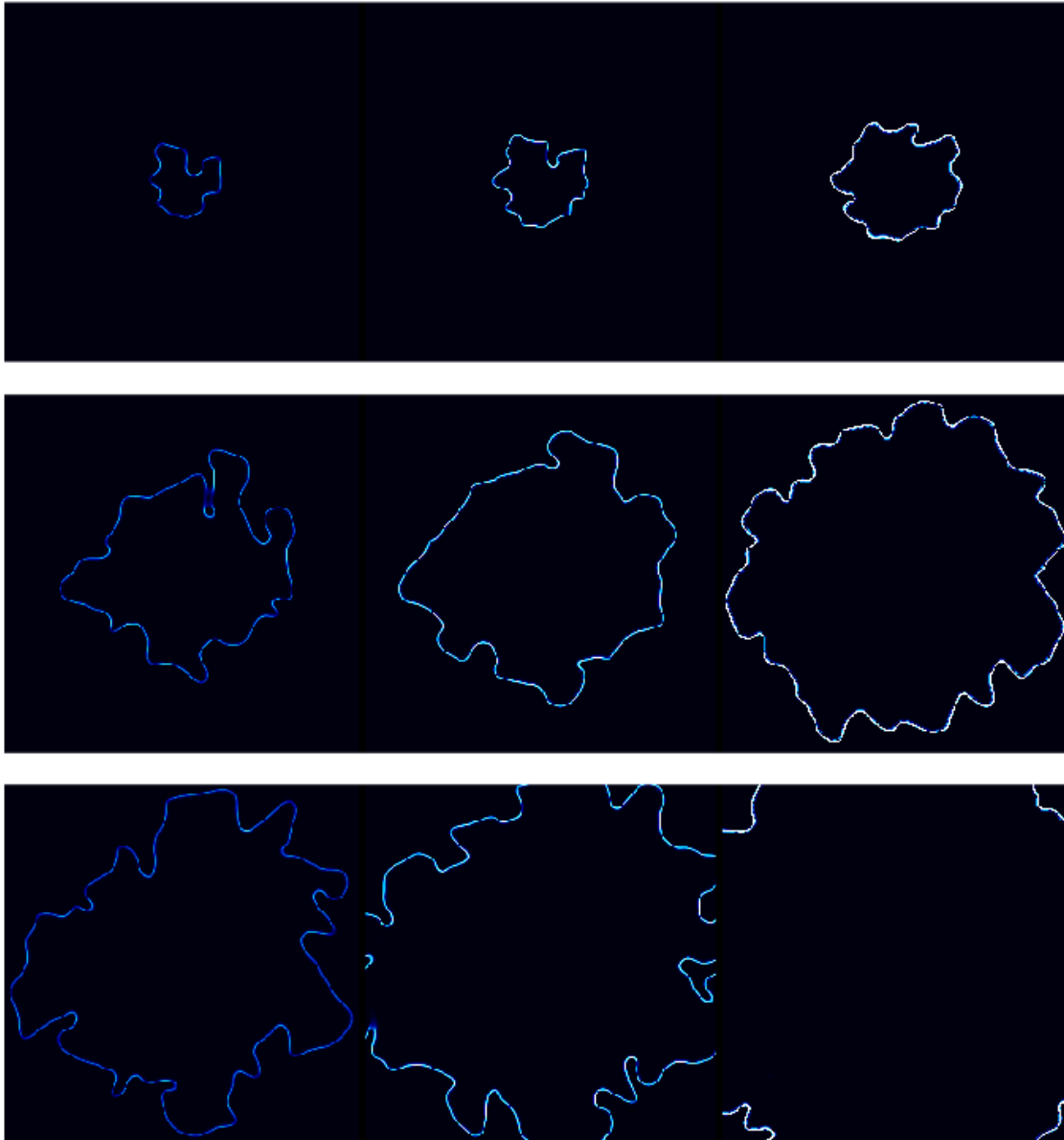
Ignition Kernel: U' is the Typical Turbulent Fluctuation "Eddy Amplitude". We keep here U' constant while changing U

S_L/U'

0.15

0.25

0.5



→ Reaction rate evolution

$$-S_d \rho_u |\nabla c|$$

→ Note how the curvature term enhances or slows down the flow speed depending on the sign (+/-) of the curvature (see the animations on kernel & Bunsen flame)

Karlovitz number
Damköhler number

Borghgi Diagram

